

Fig.1B

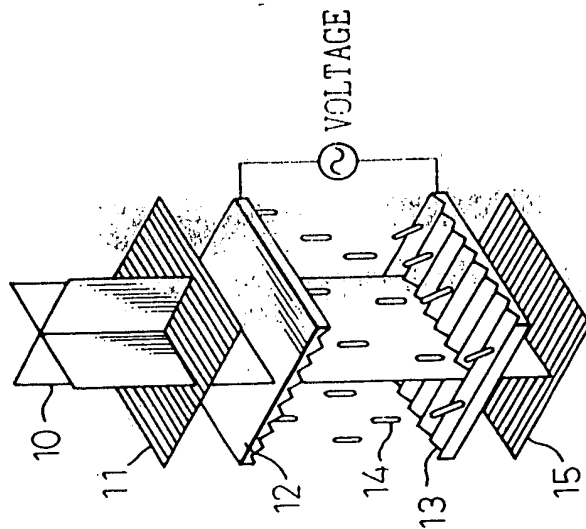


Fig.1A

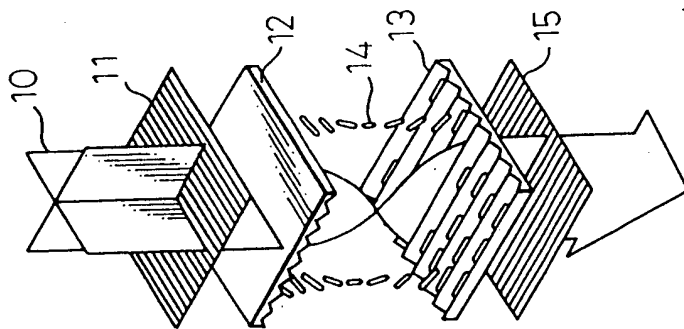


Fig.2A

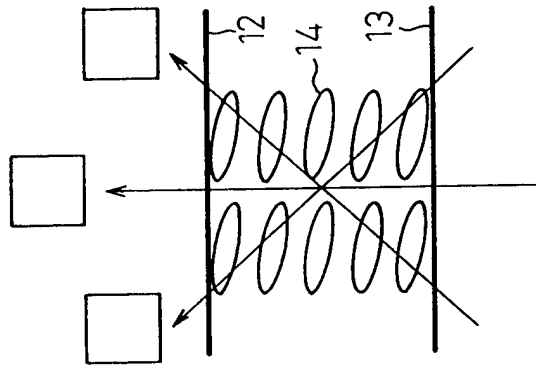


Fig.2B

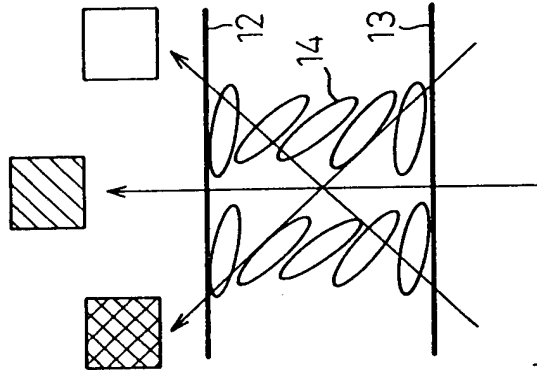


Fig.2C

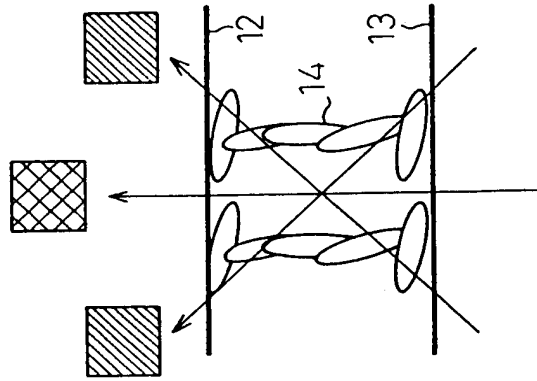


Fig.3A

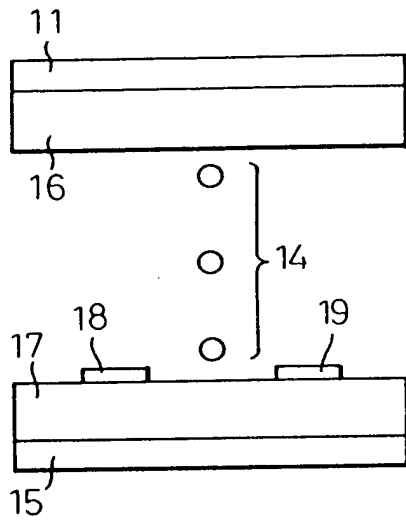


Fig.3C

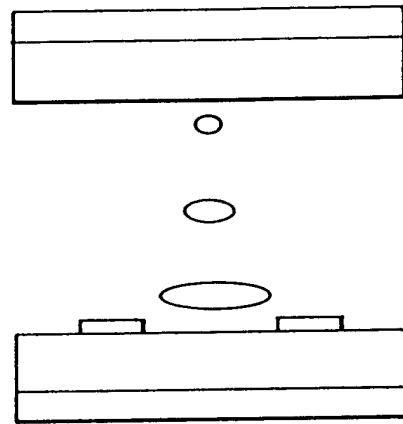


Fig.3B

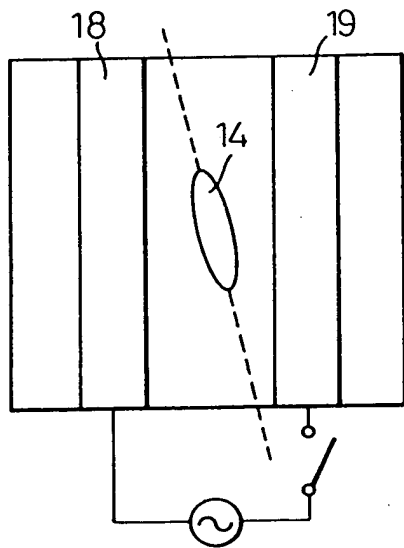


Fig.3D

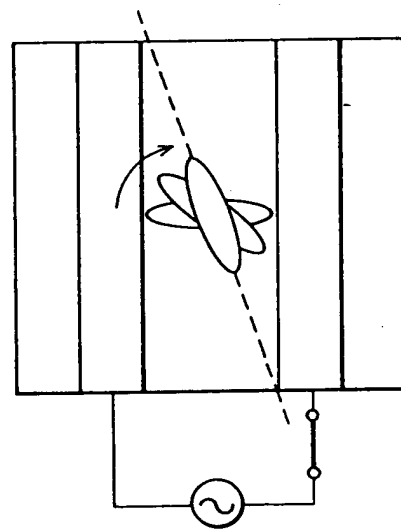
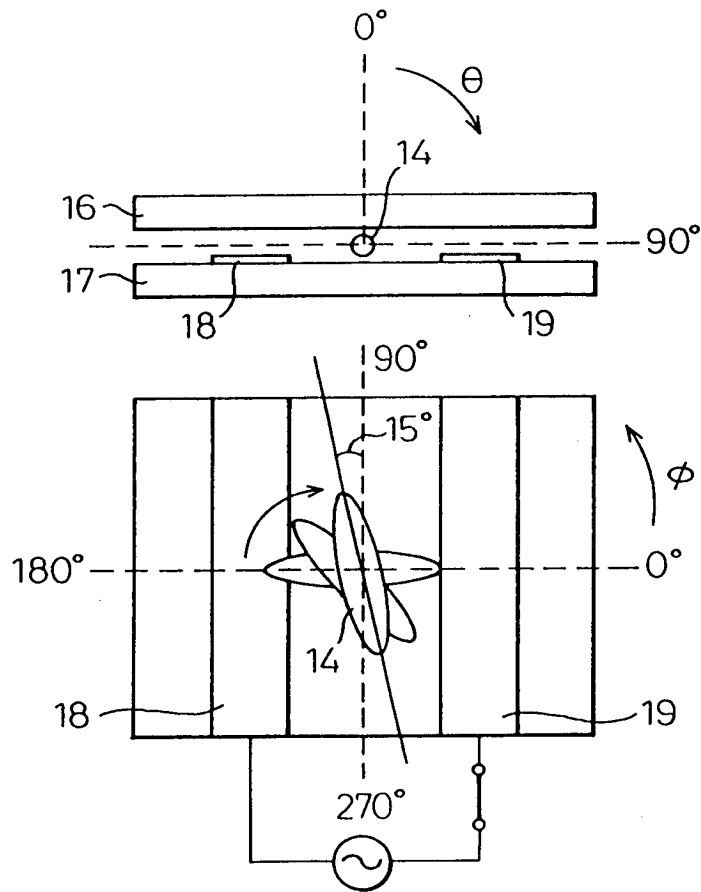
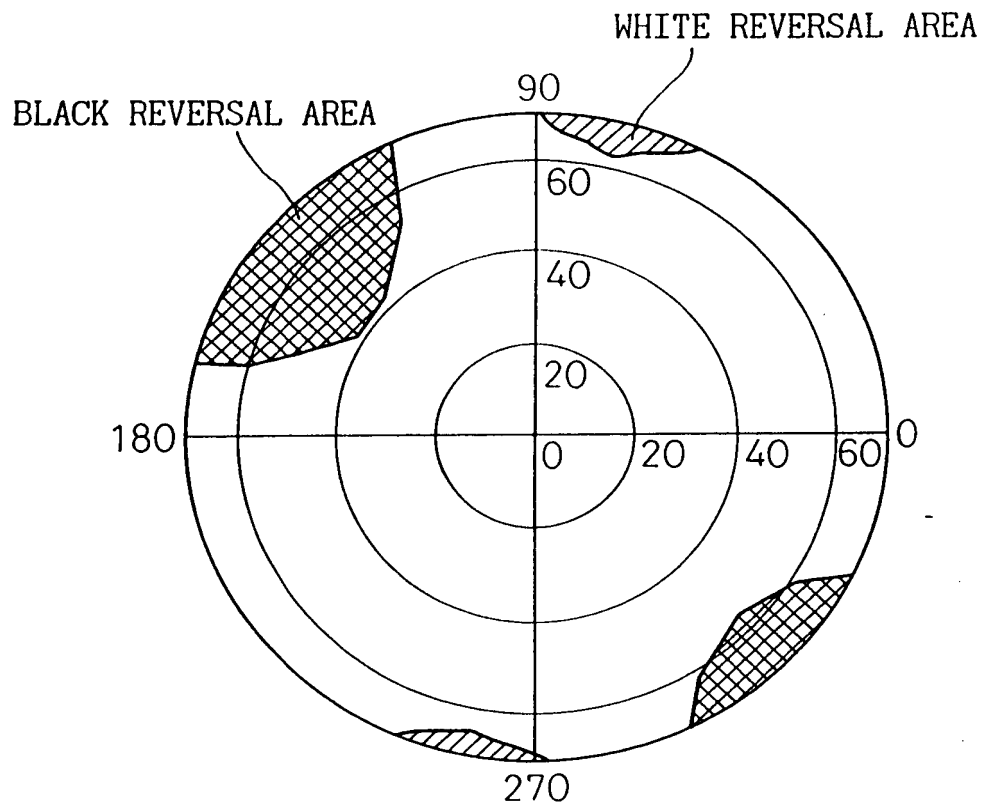


Fig.4



5/246

Fig. 5



6/246

Fig. 6A

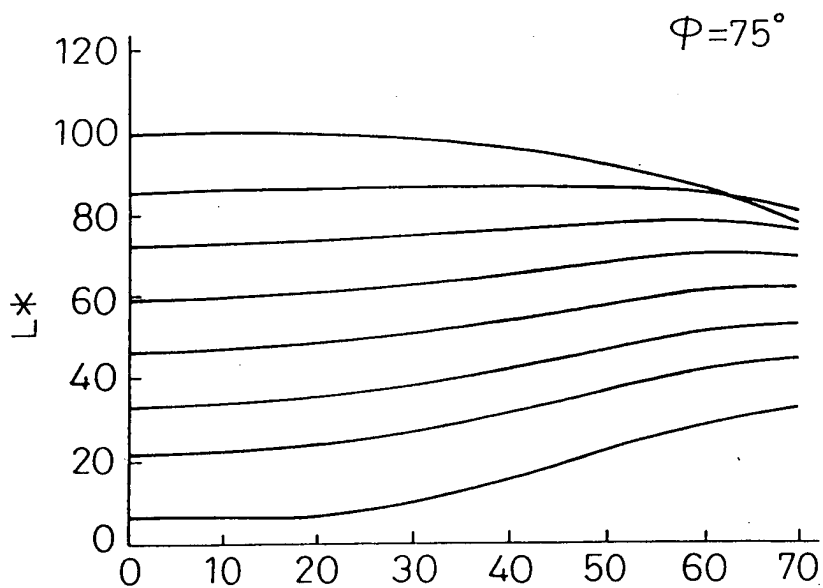


Fig. 6B

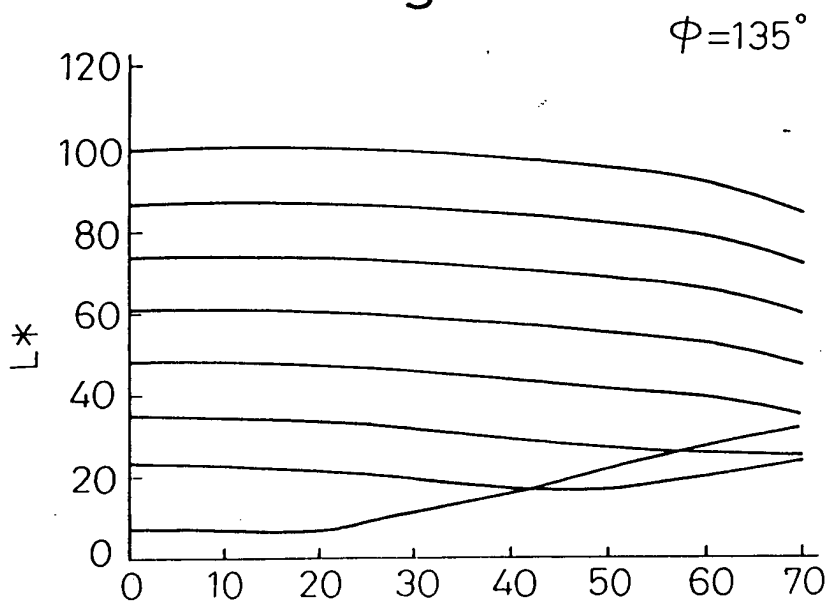


Fig.8A

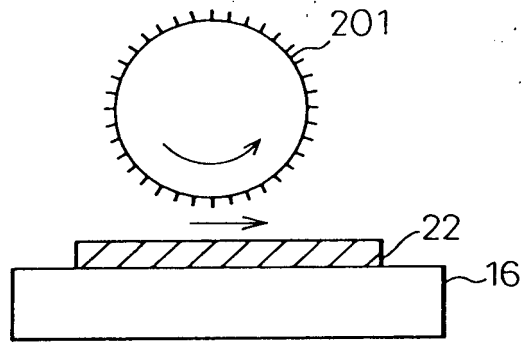


Fig.8B

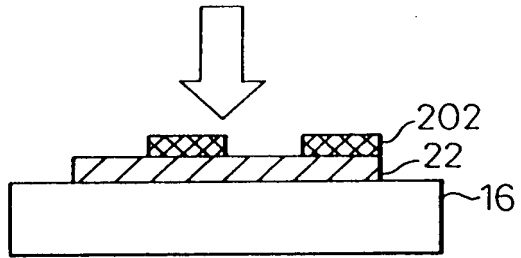


Fig.8C

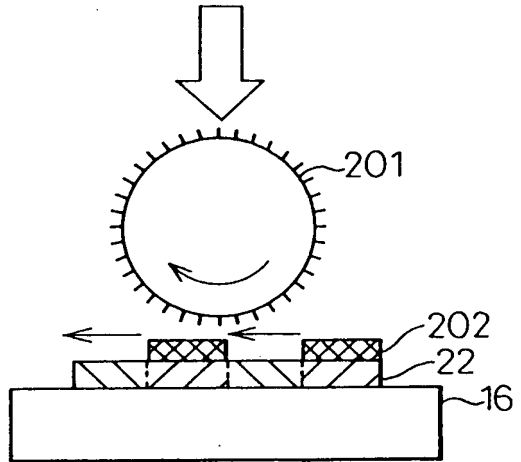


Fig.9A

Fig.9B

Fig.9C

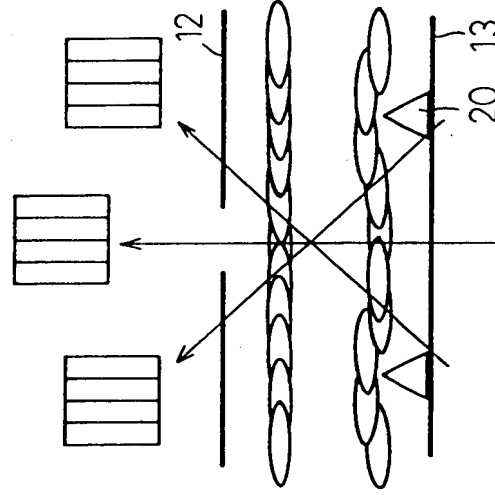
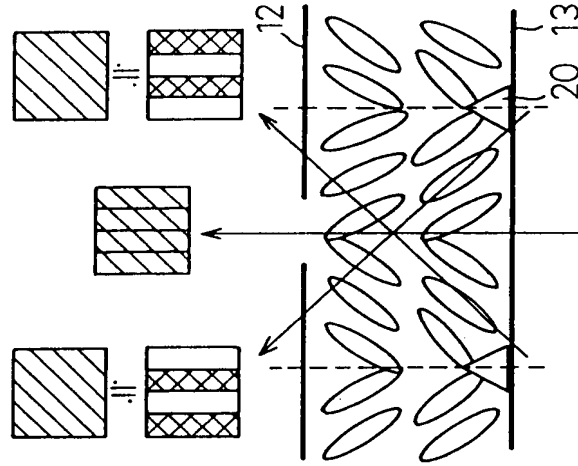
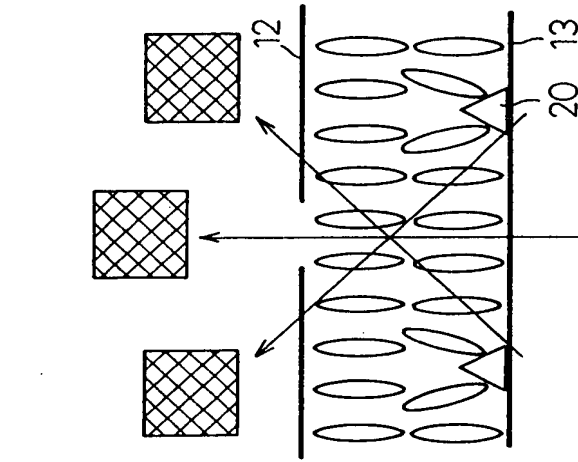


Fig.10A

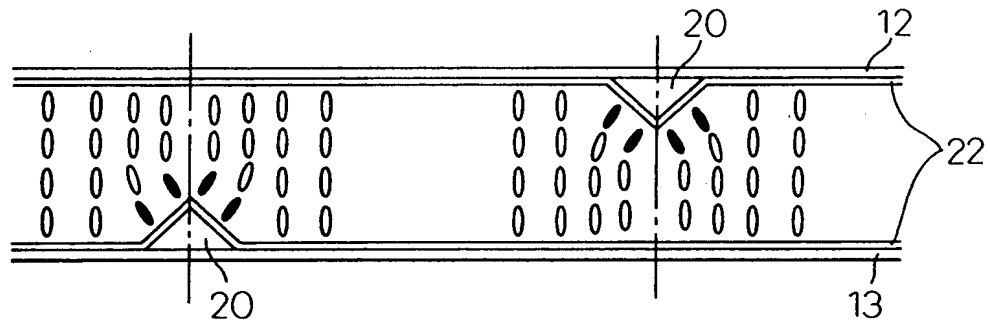


Fig.10B

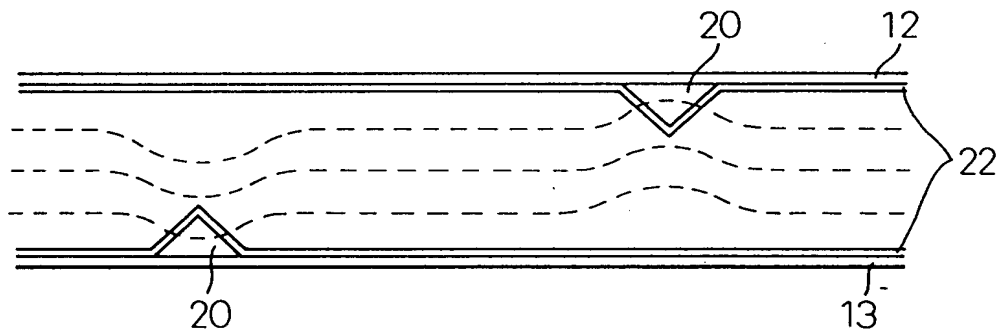


Fig.10C

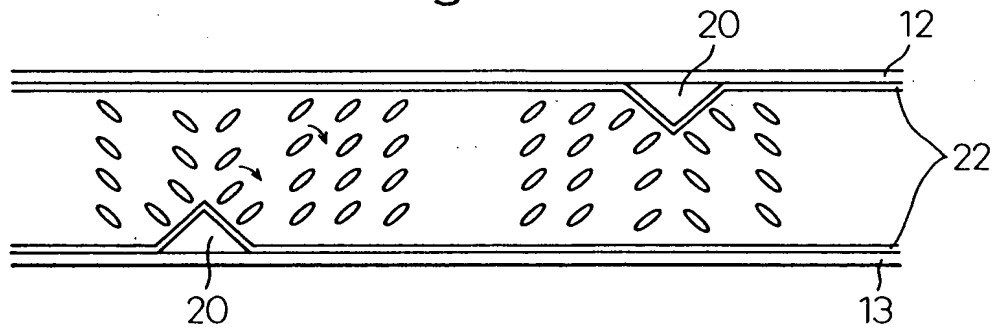


Fig.11A

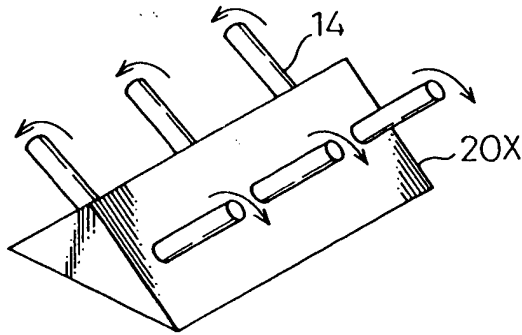
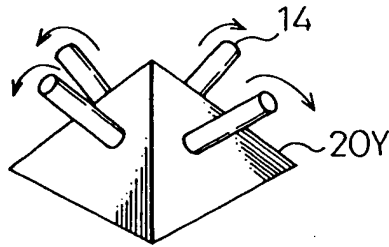


Fig.11B



F i g . 1 1 C

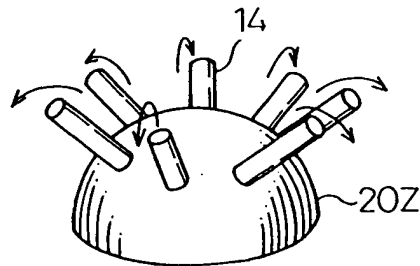


Fig.12A

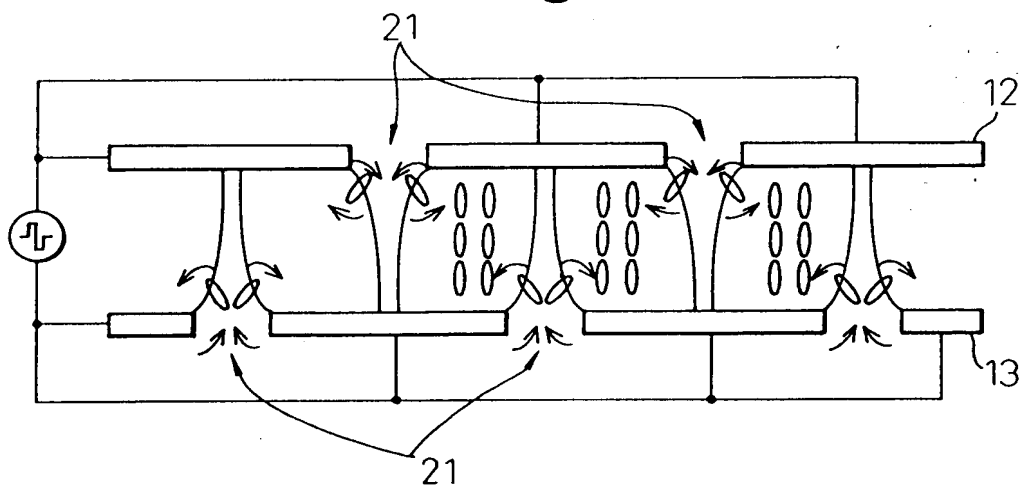


Fig.12B

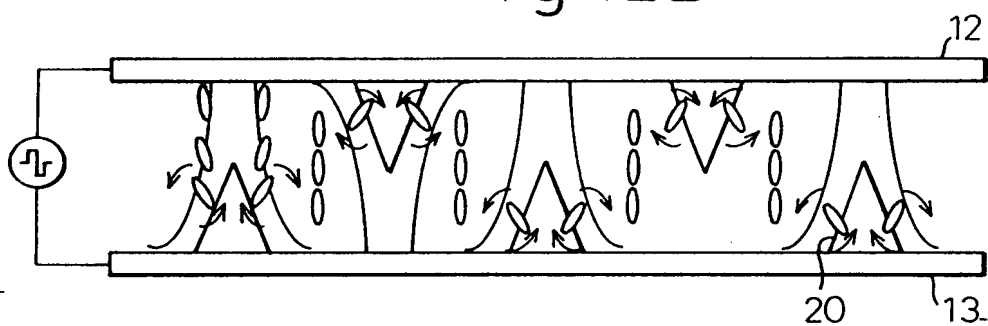
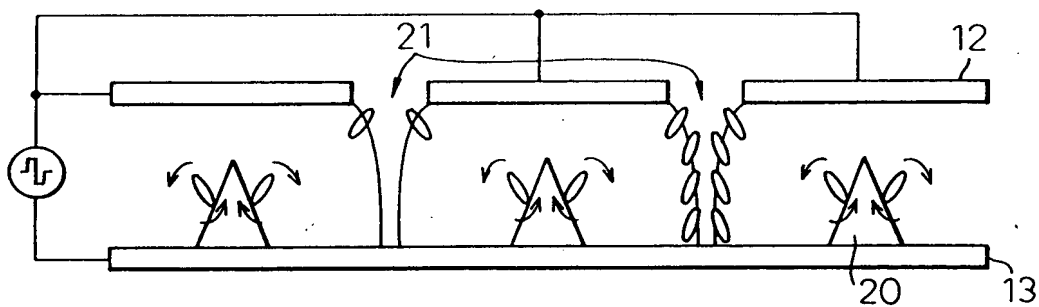


Fig.12C



13/246

Fig.13

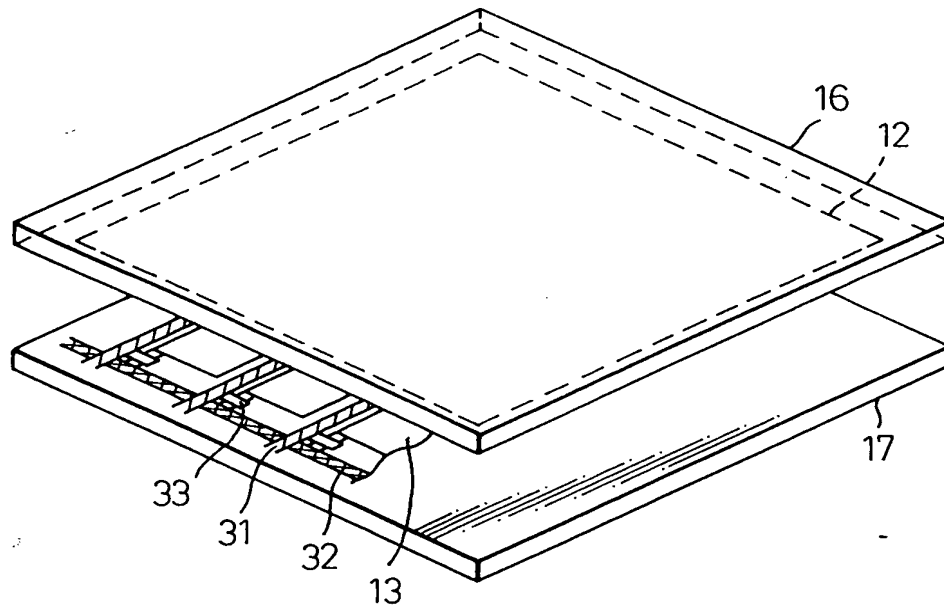


Fig.14A

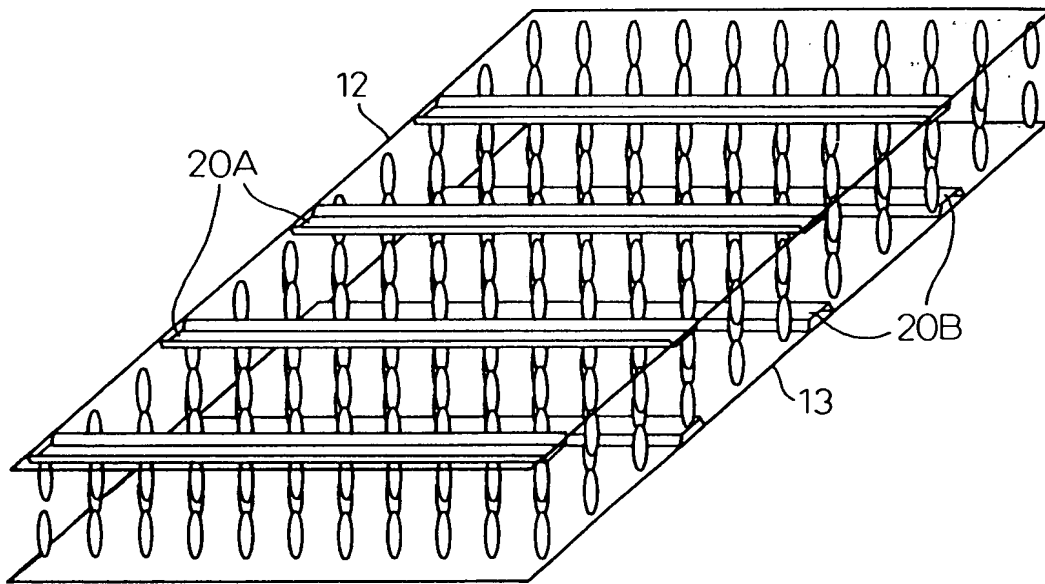


Fig.14B

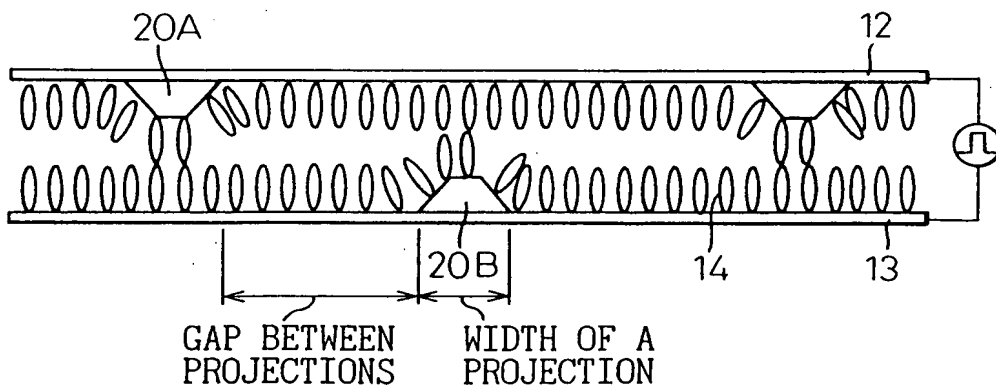


Fig.15.

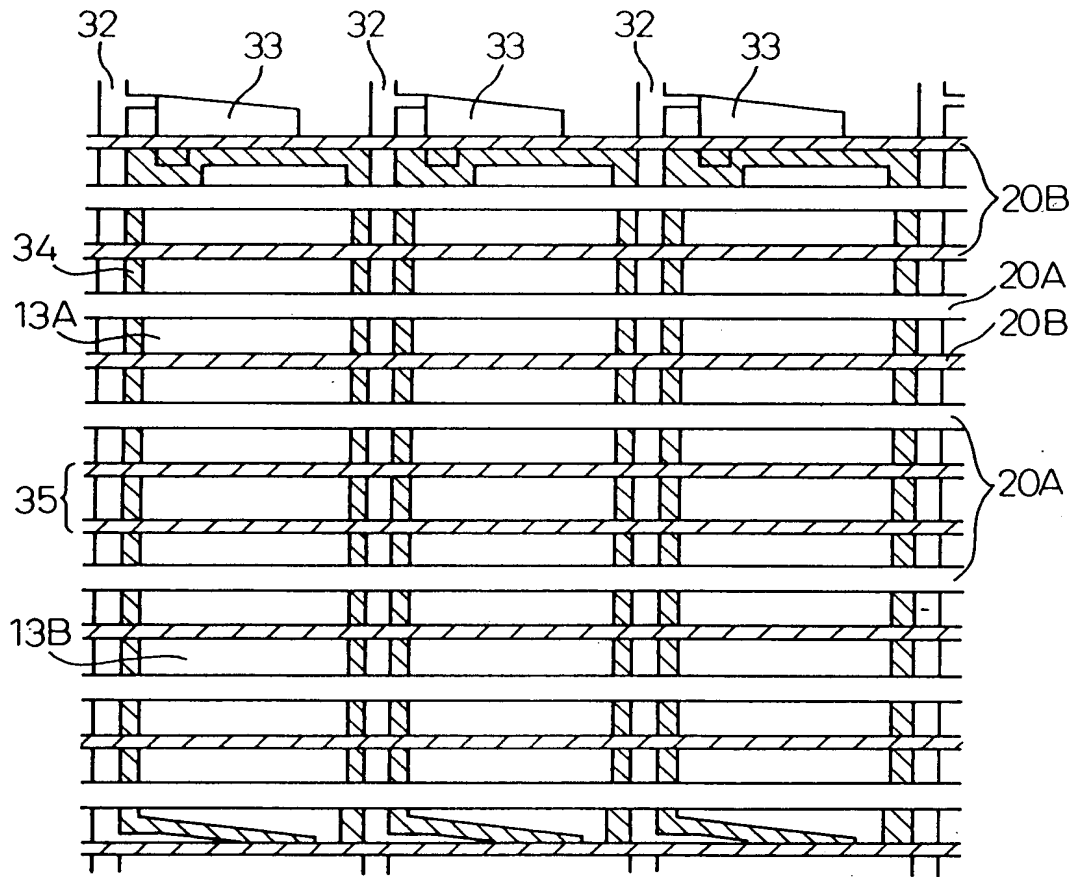


Fig.16

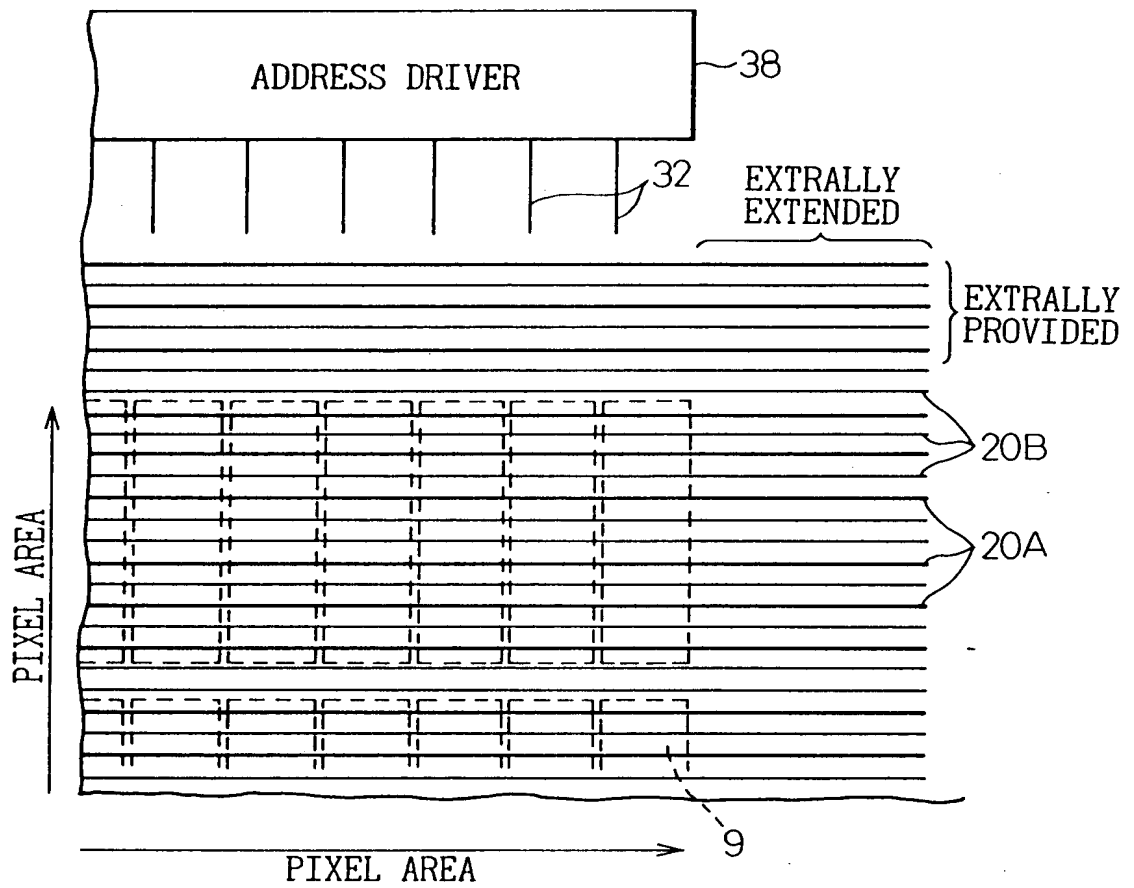


Fig.17

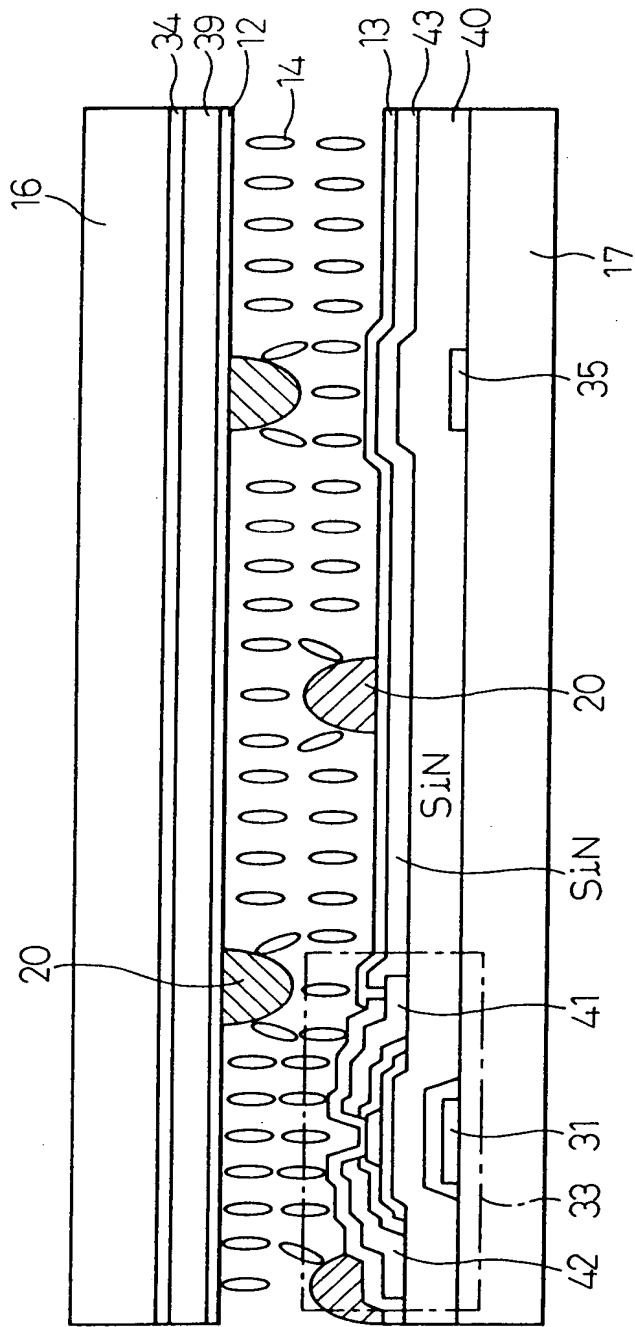


Fig.18A

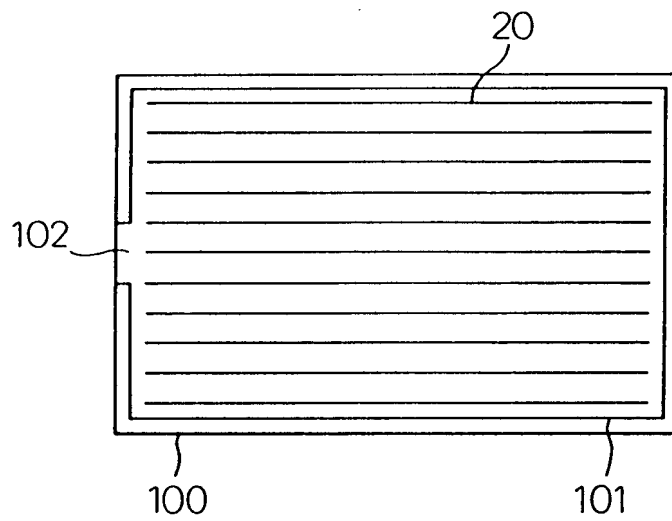


Fig.18B

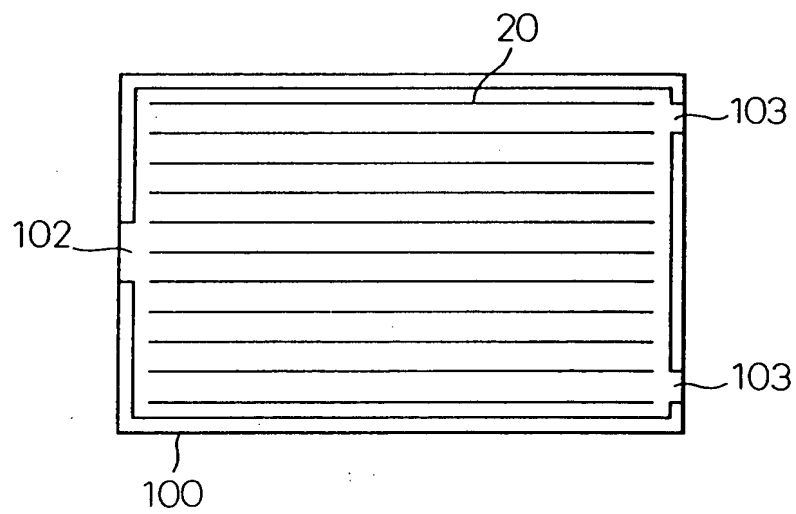
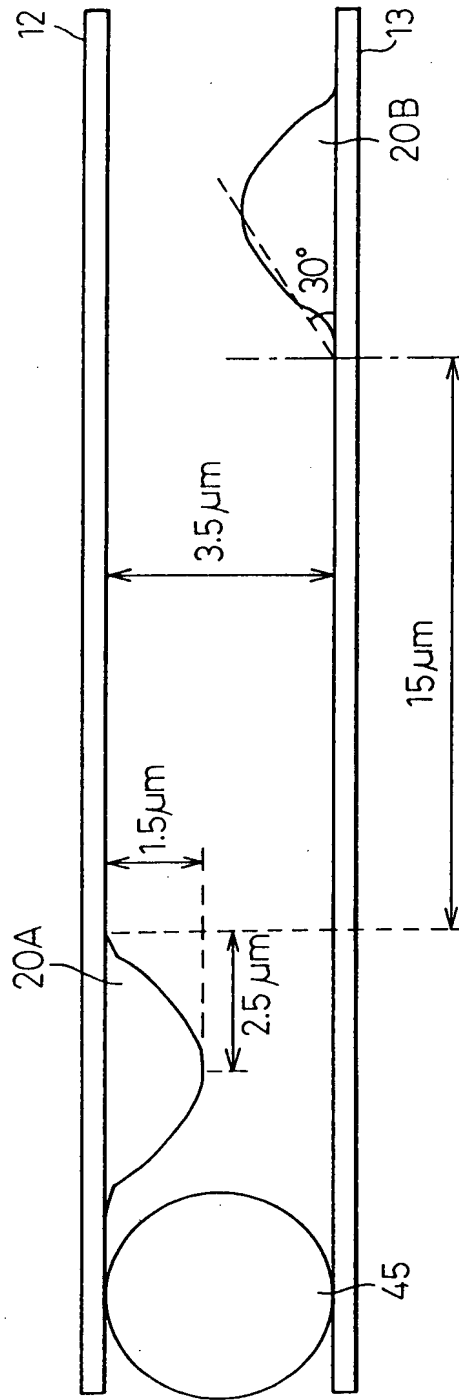


Fig. 19



20/246

Fig.20A

ON RESPONSE SPEED

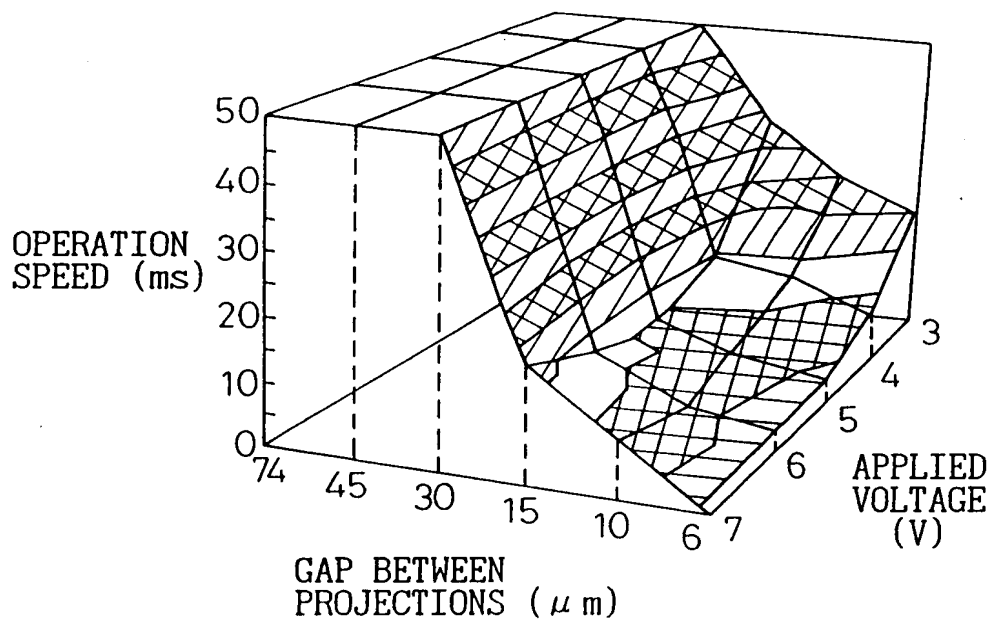
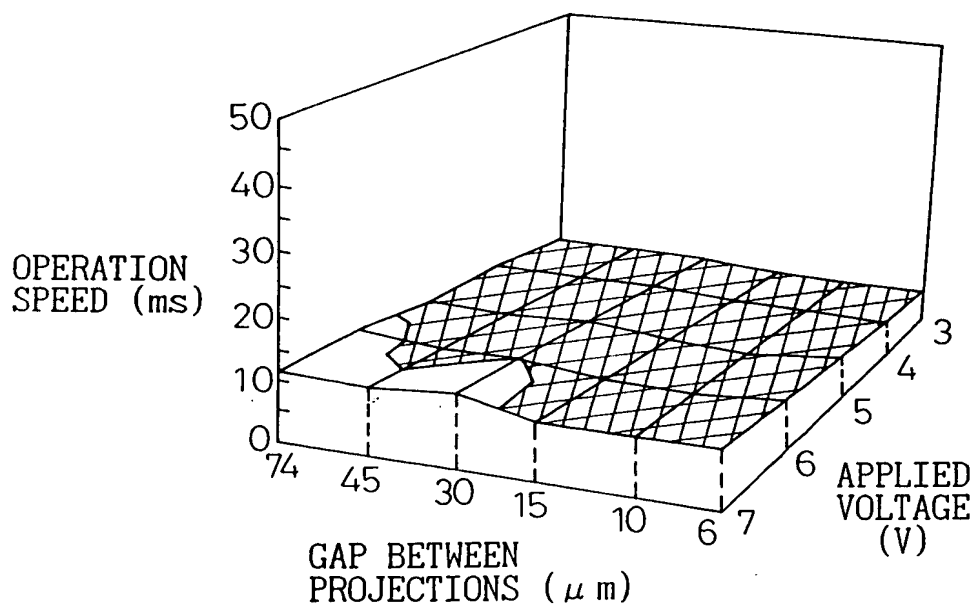


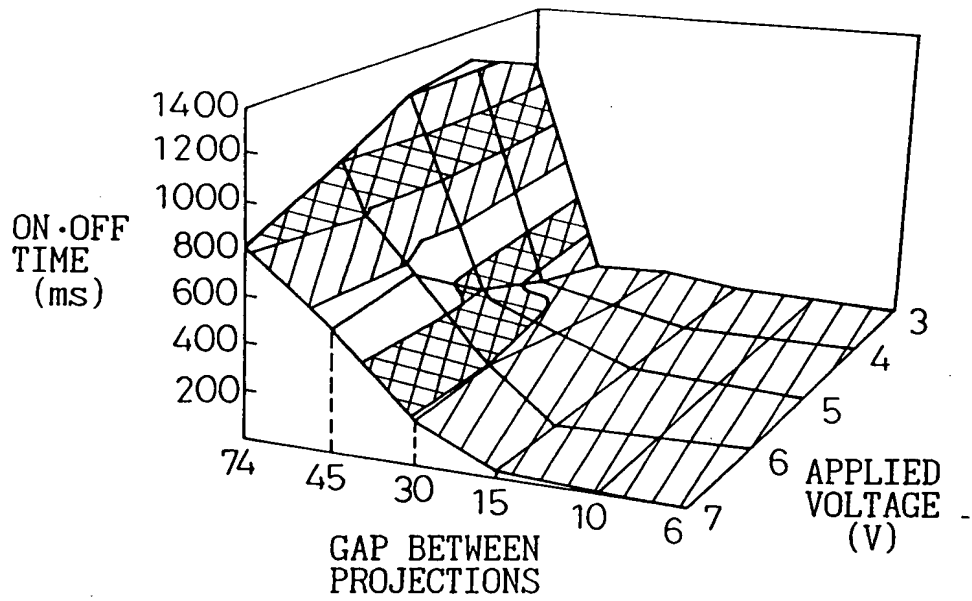
Fig.20B

OFF RESPONSE SPEED



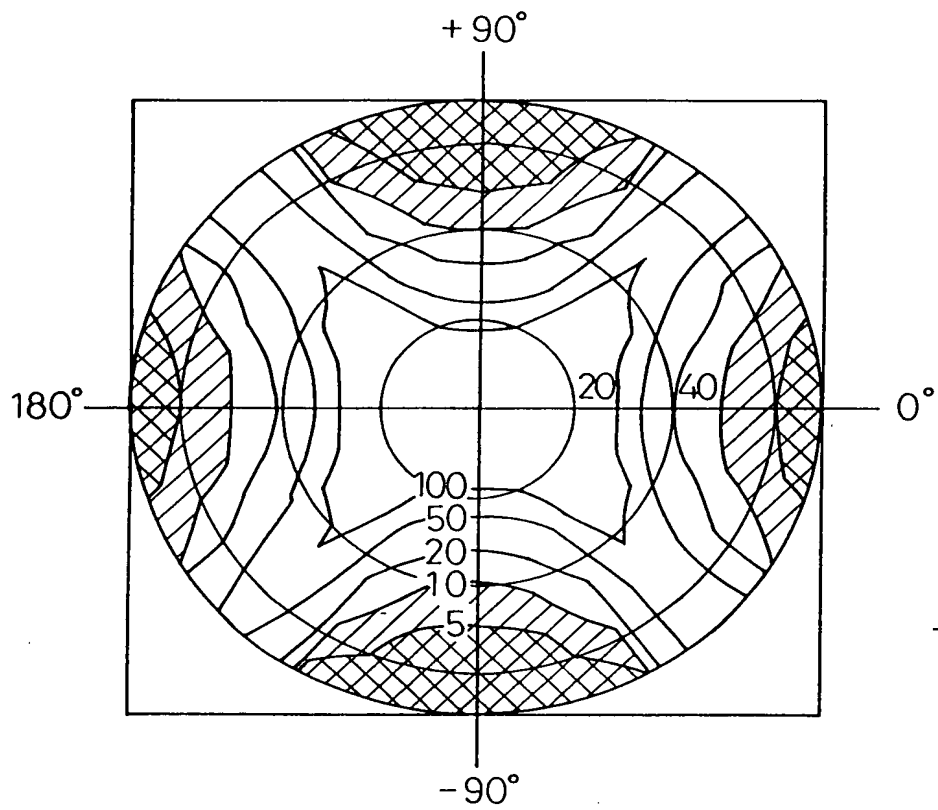
21/246

Fig. 21



22/246

Fig. 22



23/246

Fig.23A

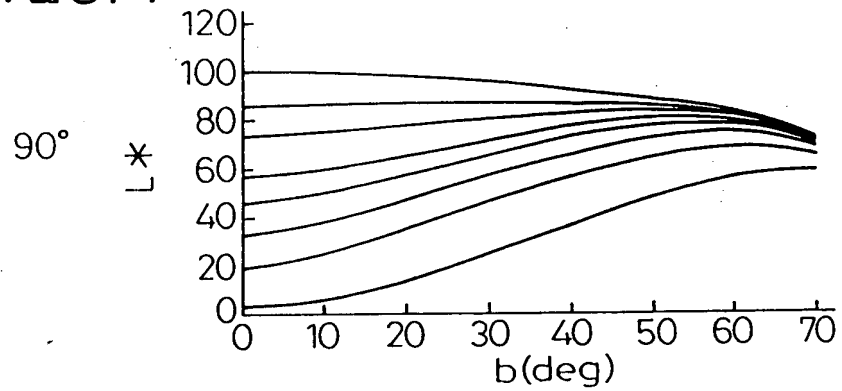


Fig.23B

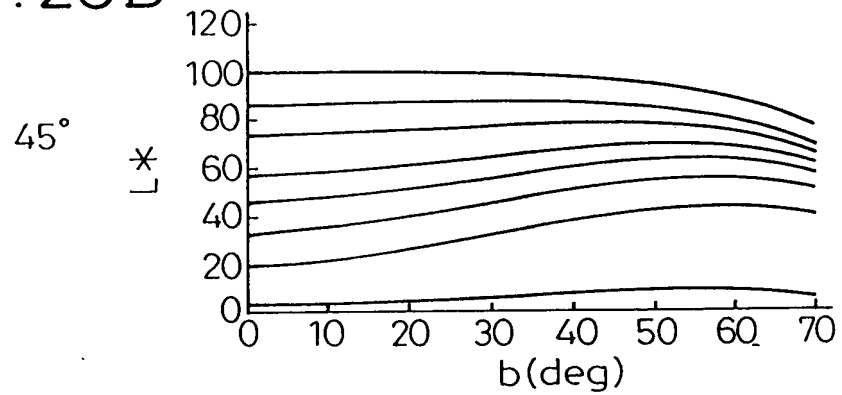
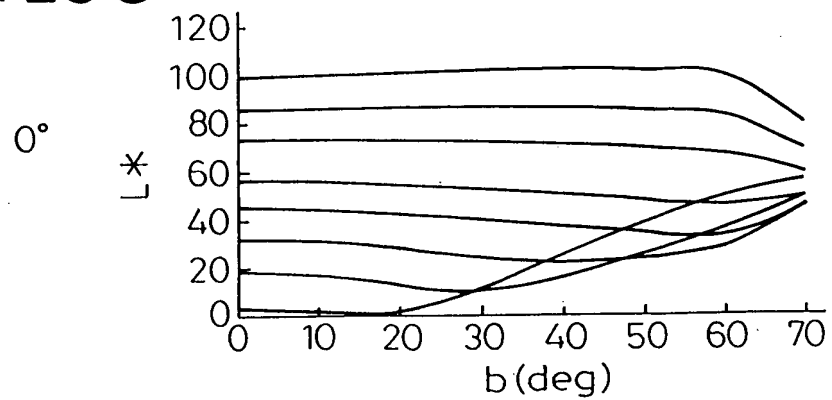


Fig.23C



24/246

Fig.24A

-45°

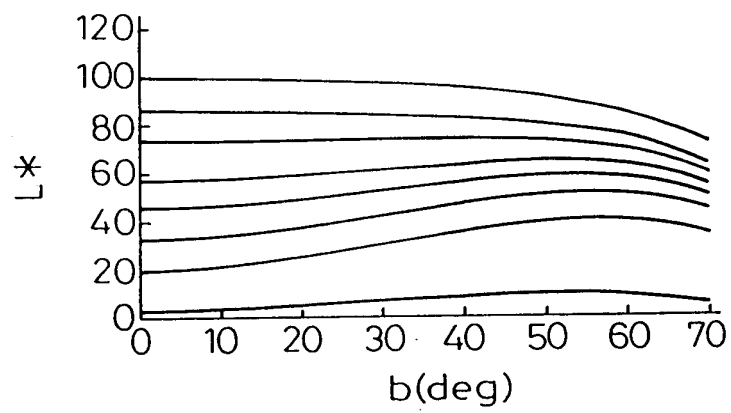
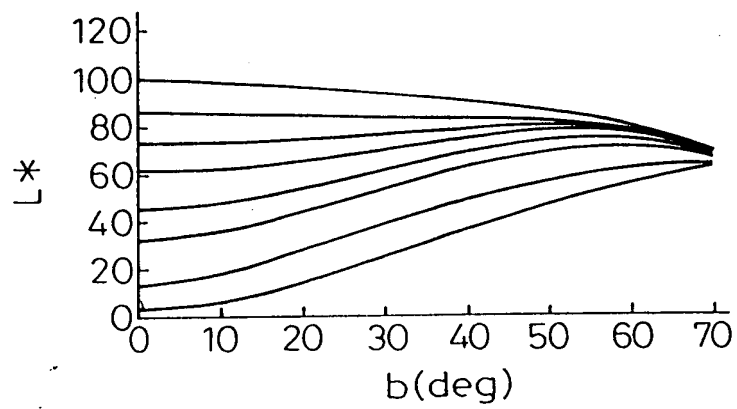


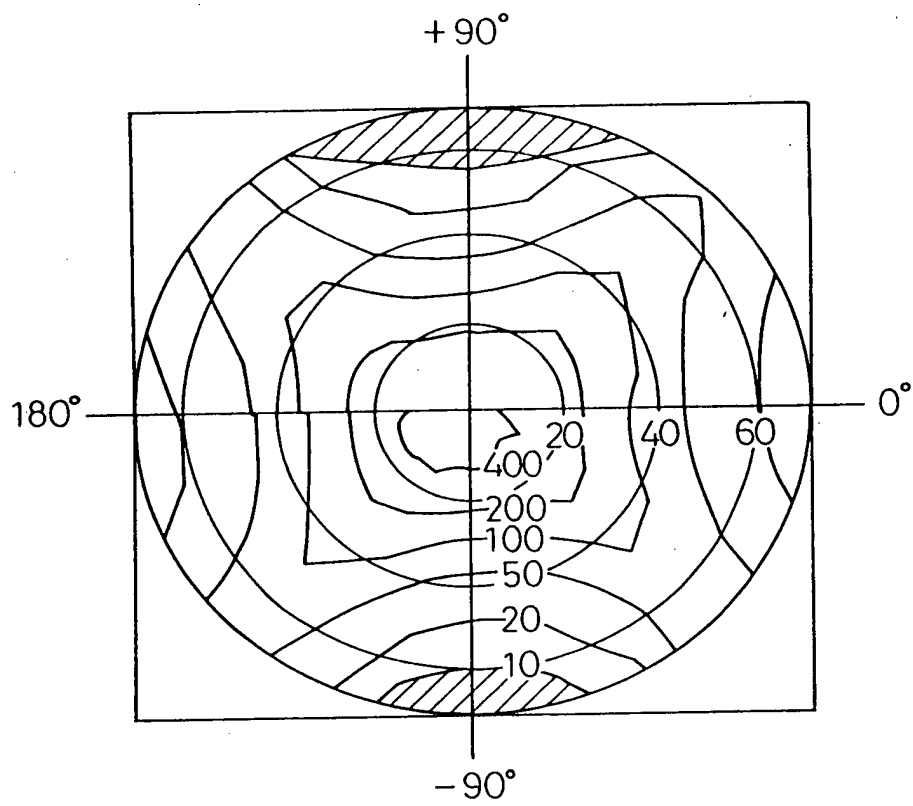
Fig.24B

-90°



25/
246

Fig.25



26/
246

Fig.26A

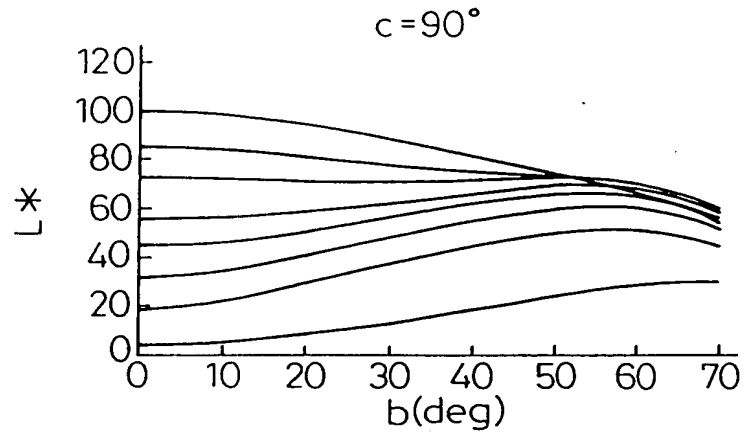


Fig.26B

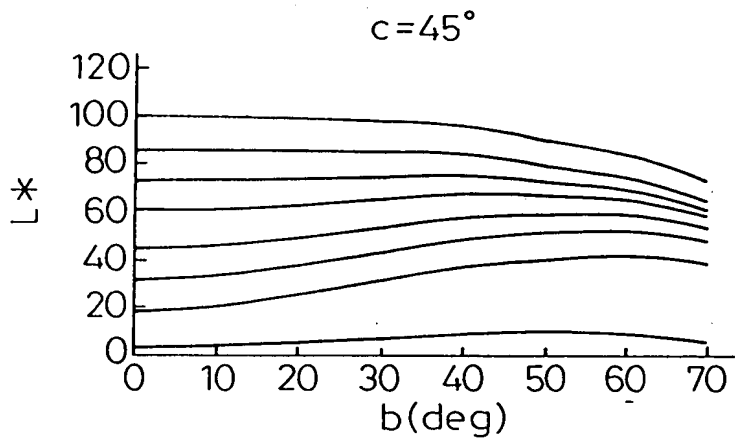
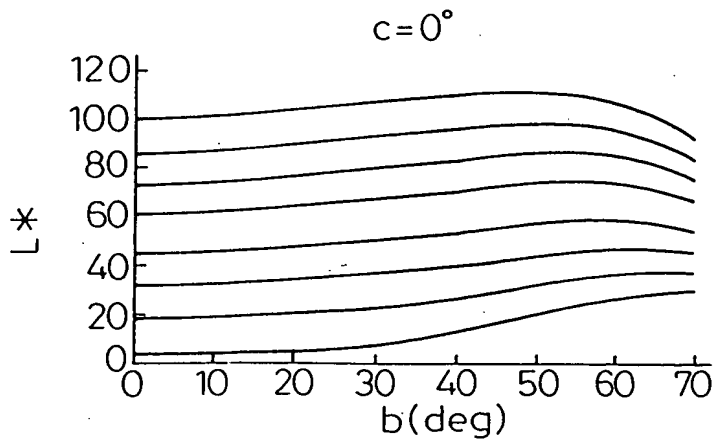


Fig.26C



27/246

Fig. 27

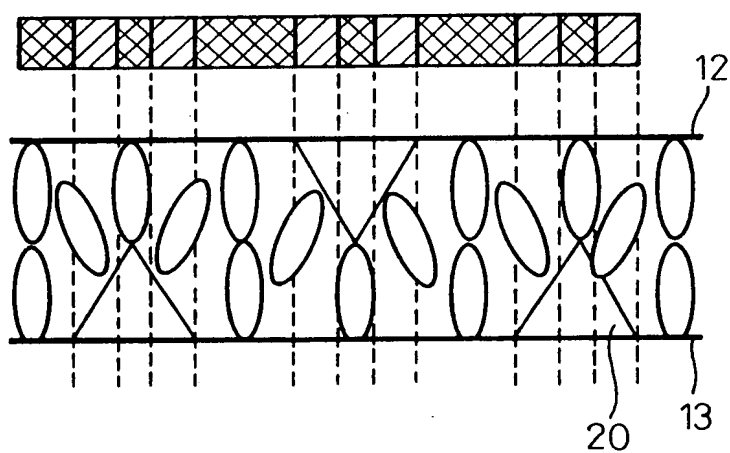


Fig. 28

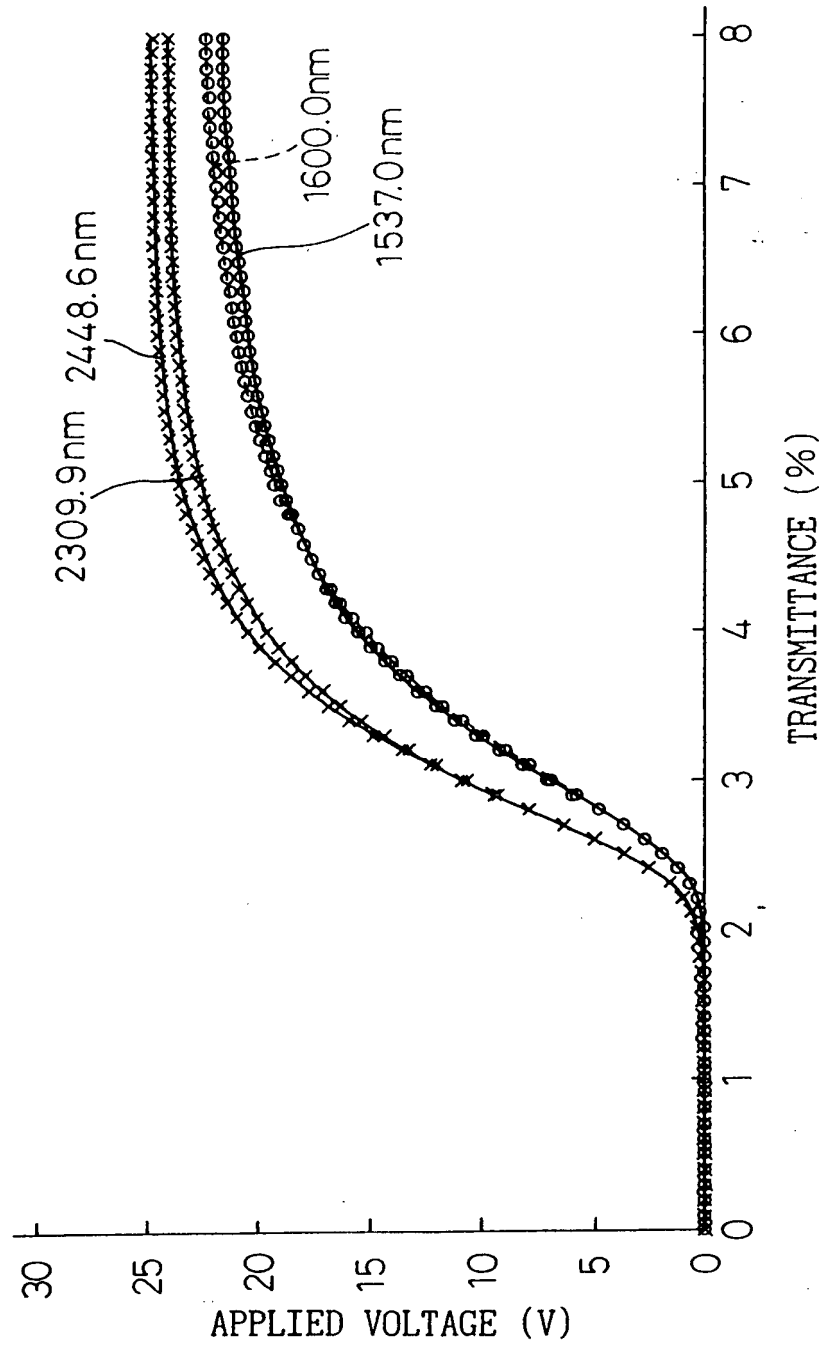
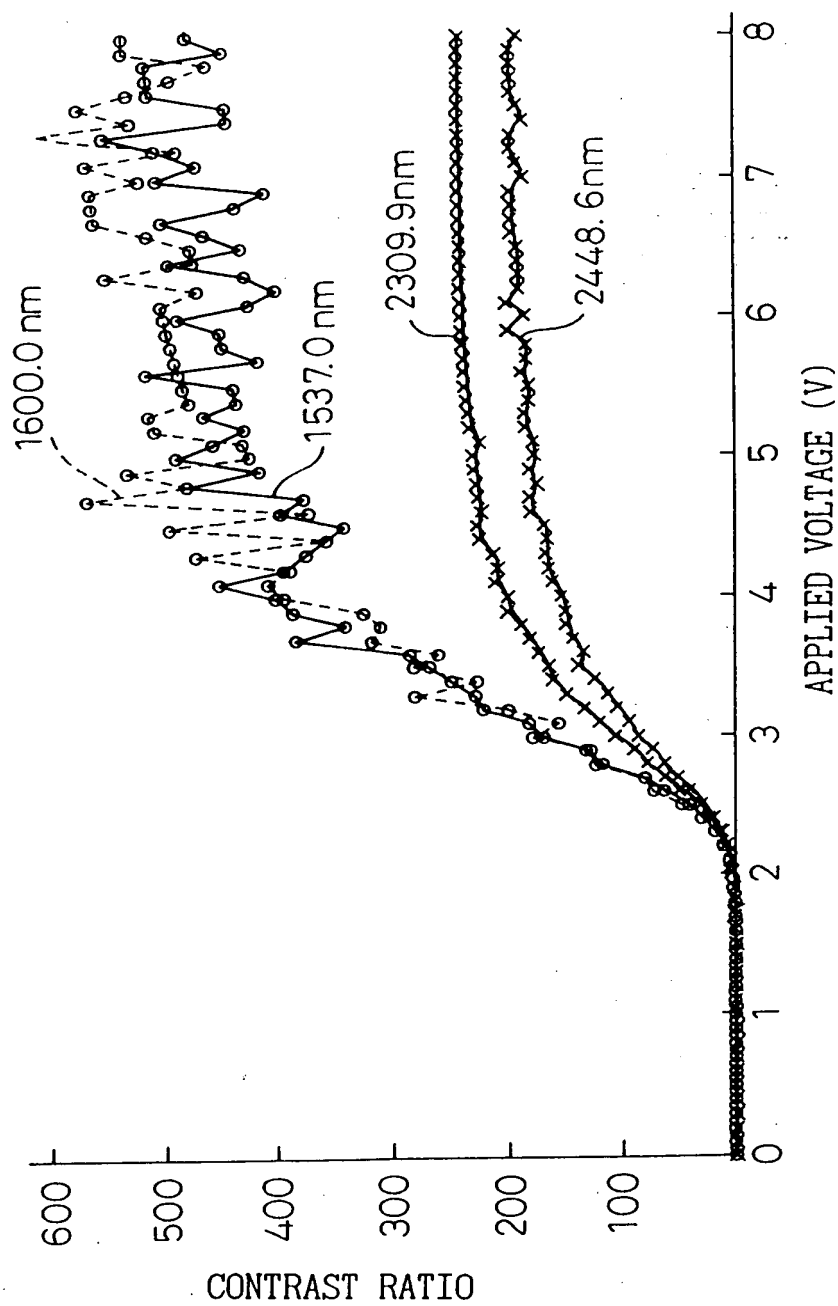


Fig. 29



WHEN 5V IS APPLIED

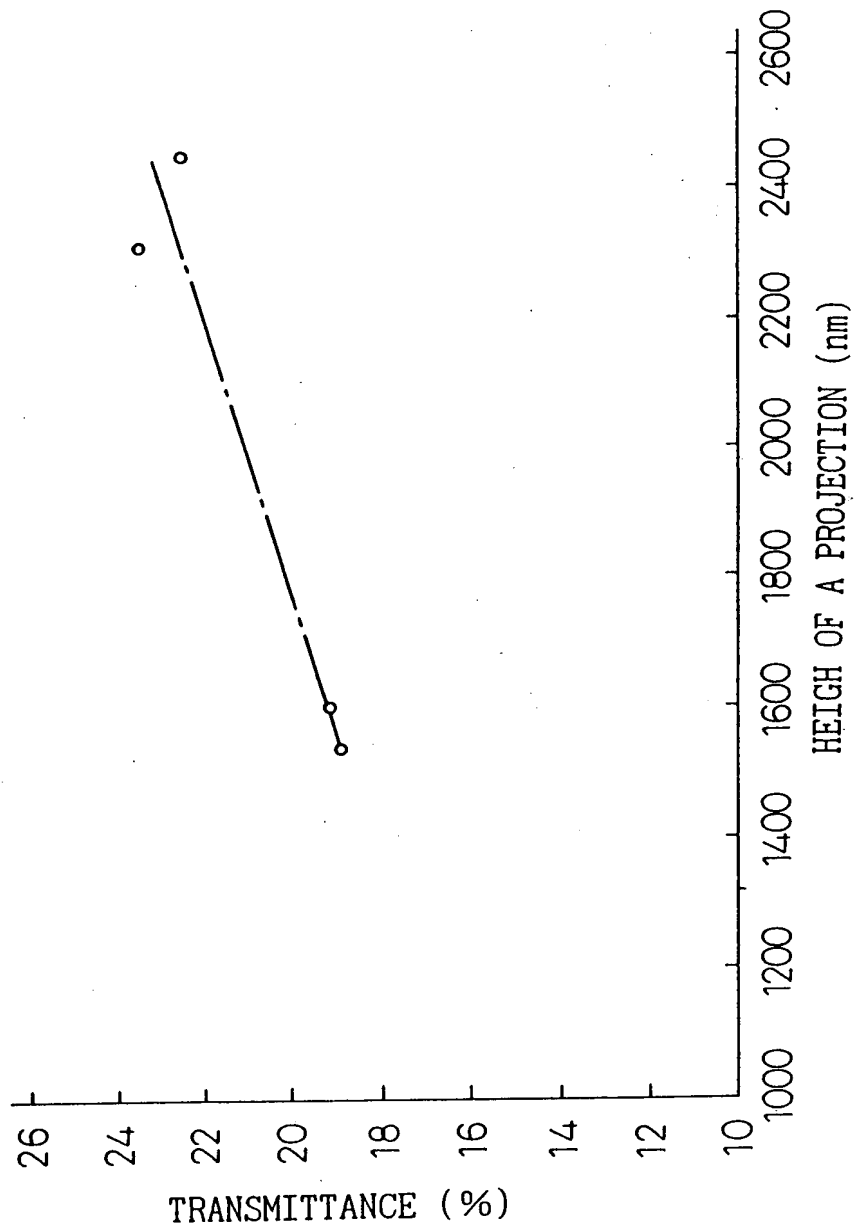
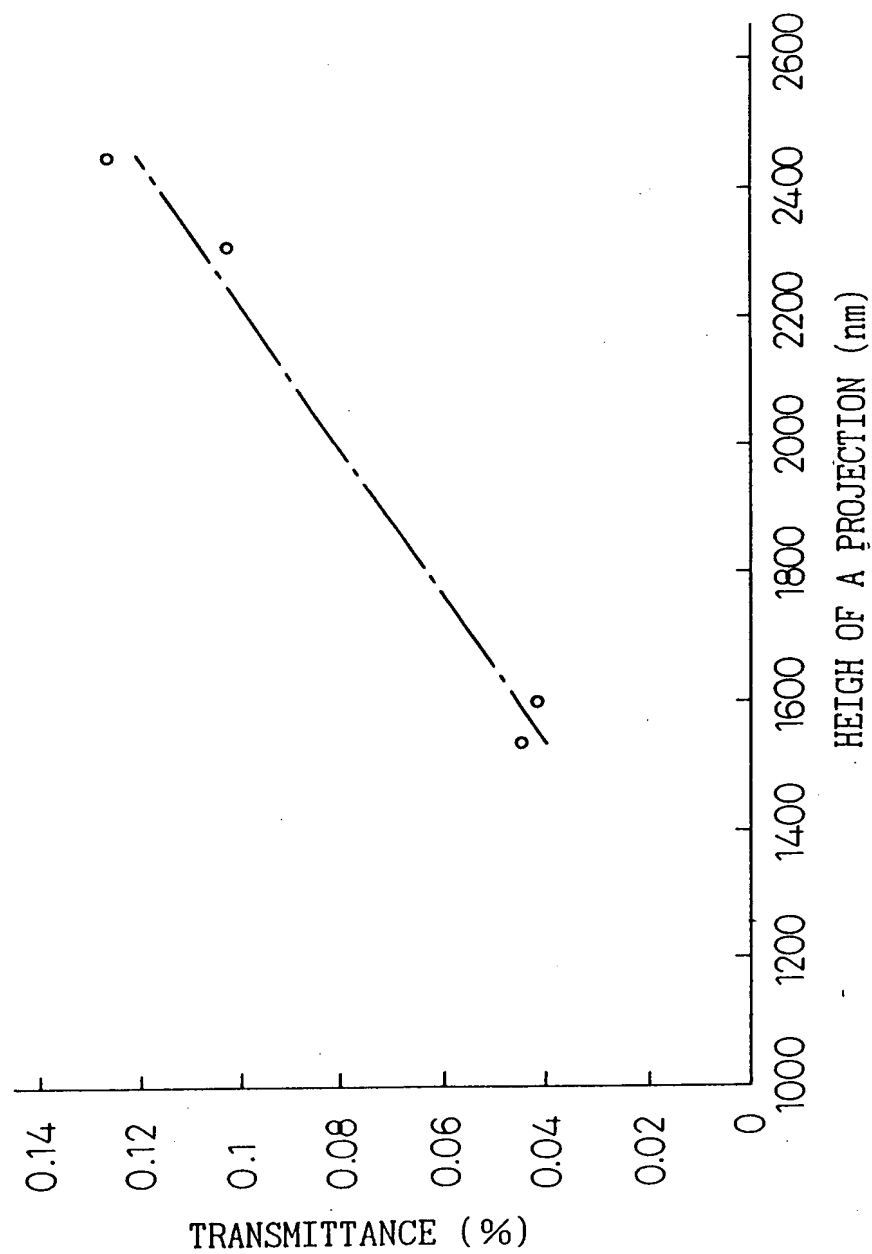


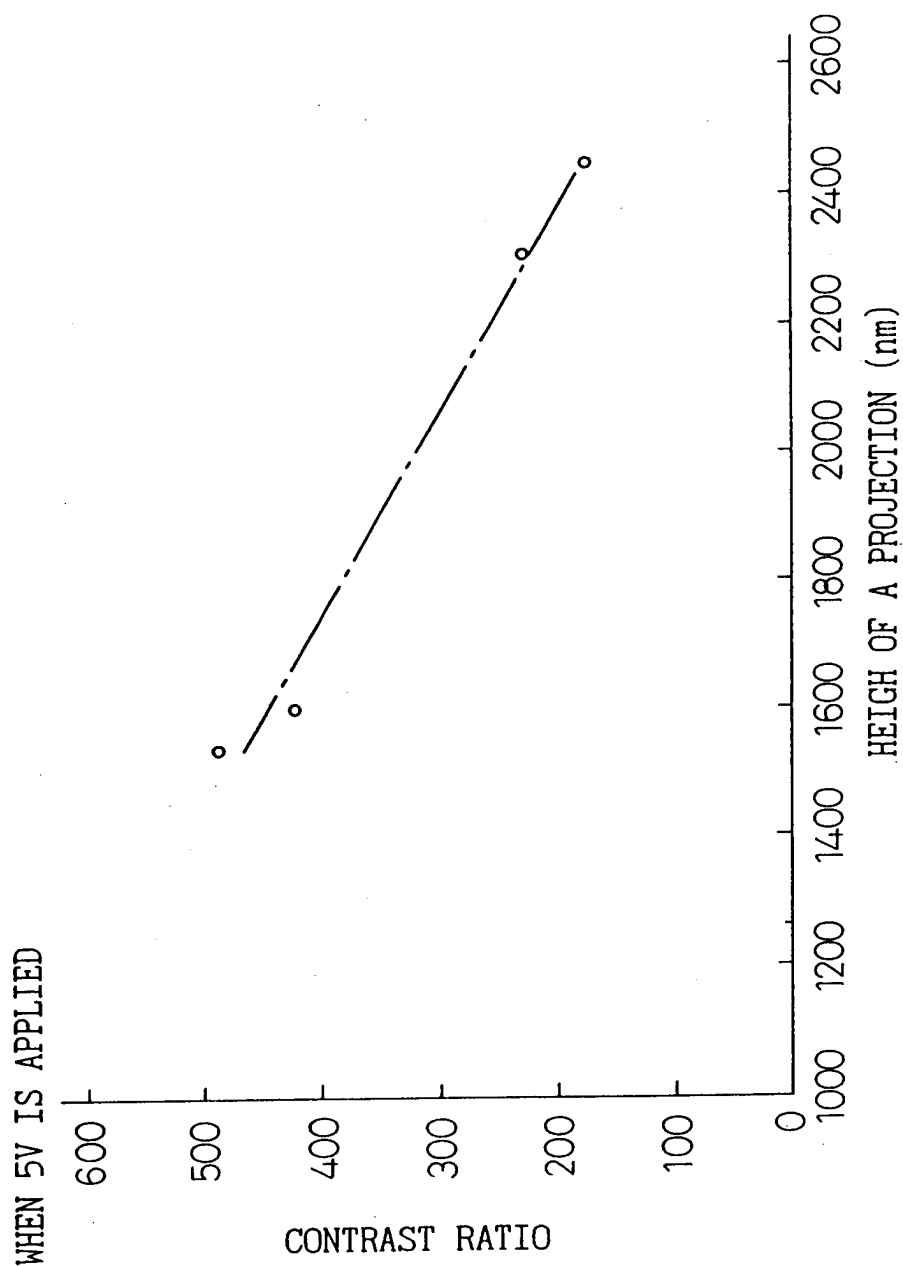
Fig.31

WHEN NO VOLTAGE IS APPLIED



31/246

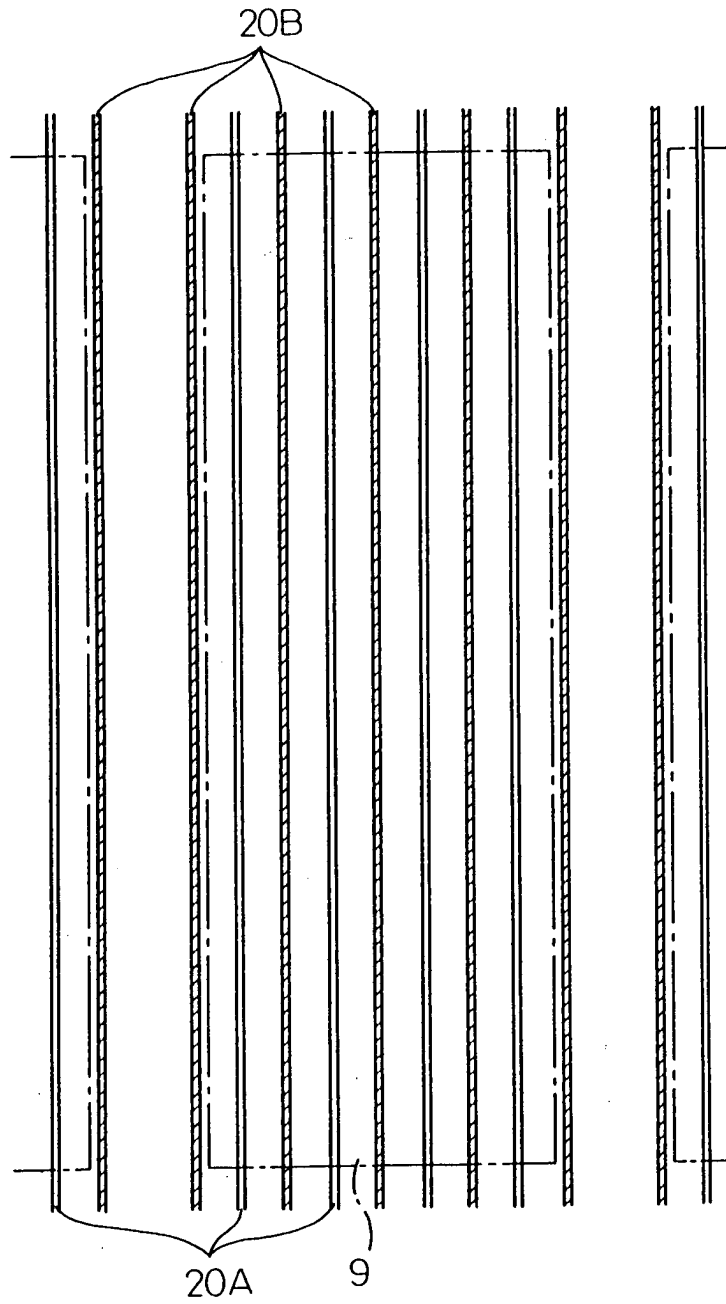
Fig.32



$\frac{32}{246}$

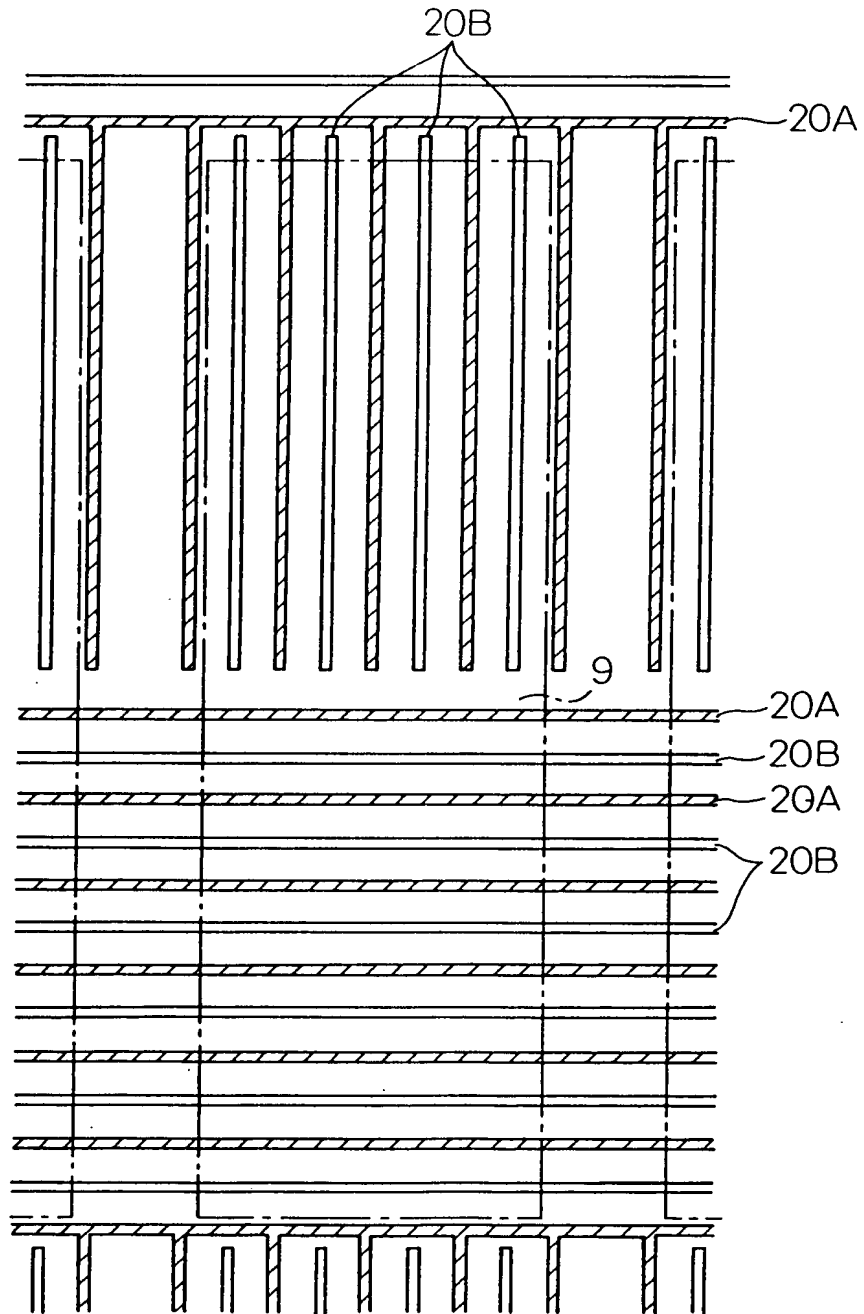
33/246

Fig. 33



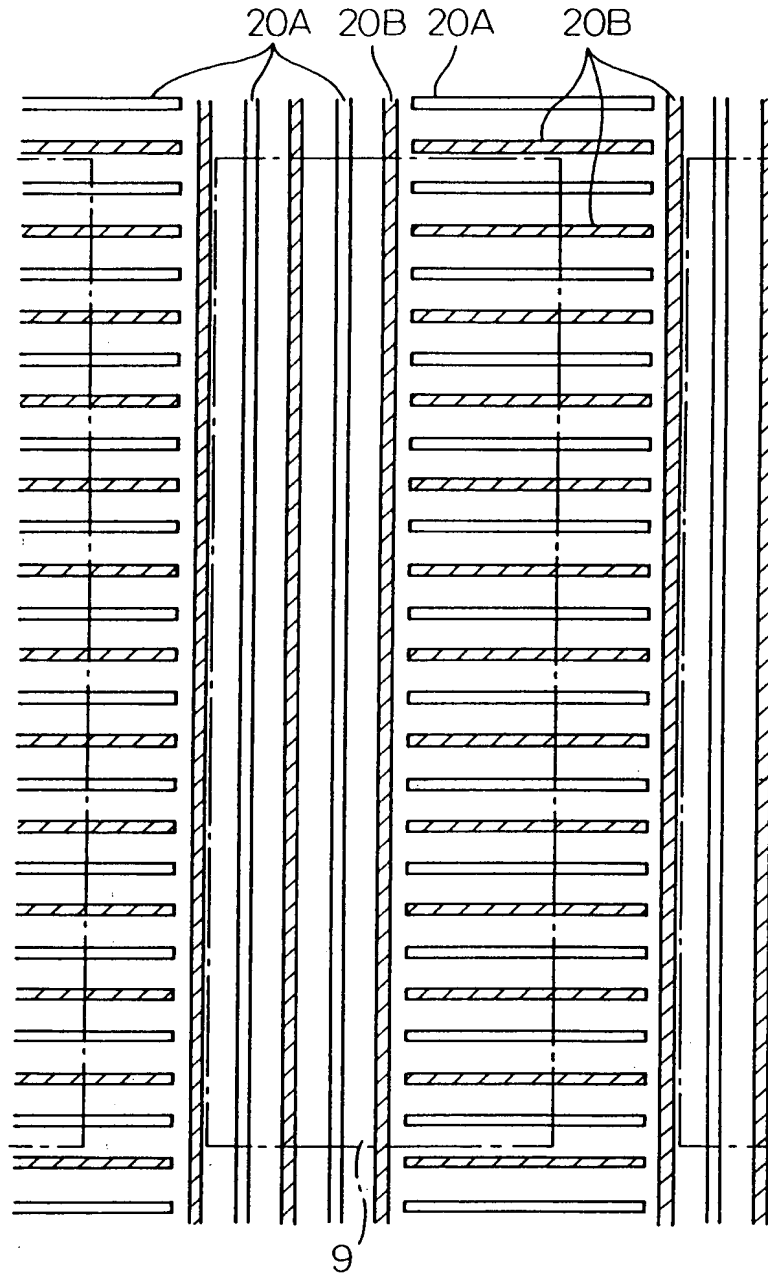
34/246

Fig. 34



35/246

Fig. 35



36/246

Fig. 36

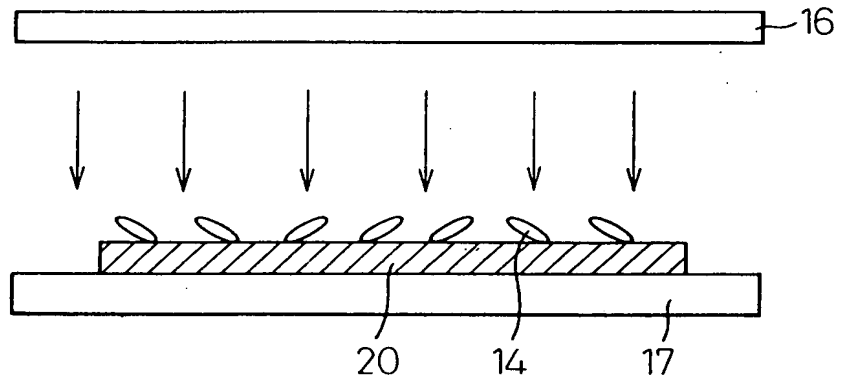


Fig. 37A

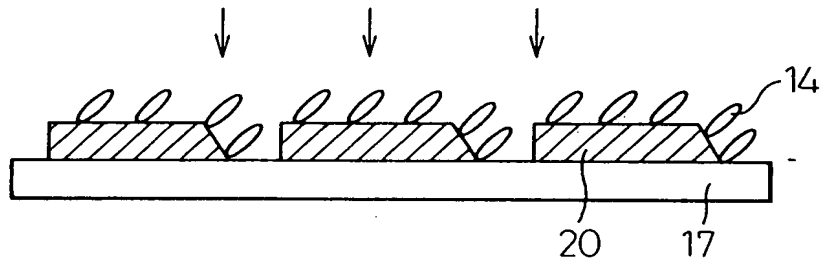


Fig. 37B

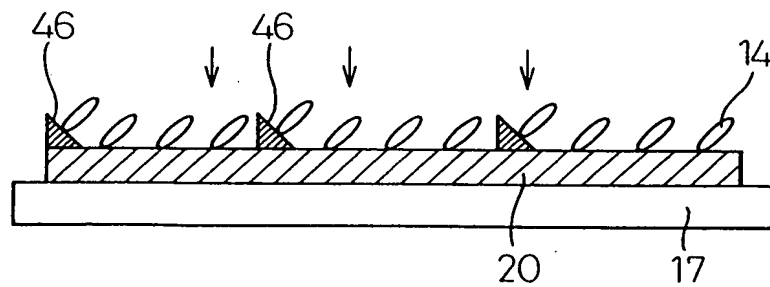


Fig.38A

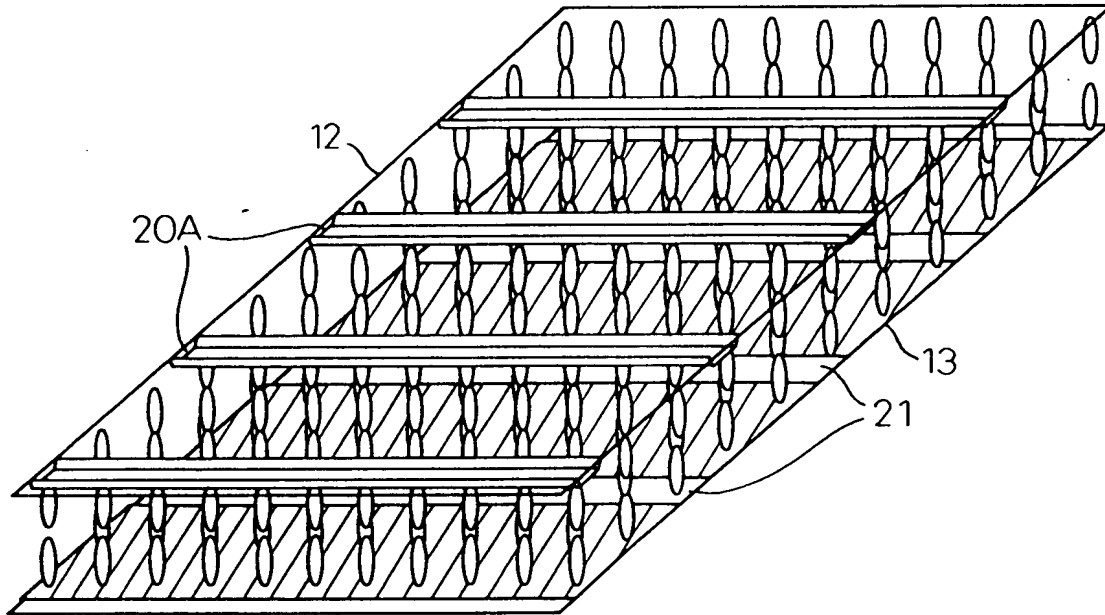


Fig.38B

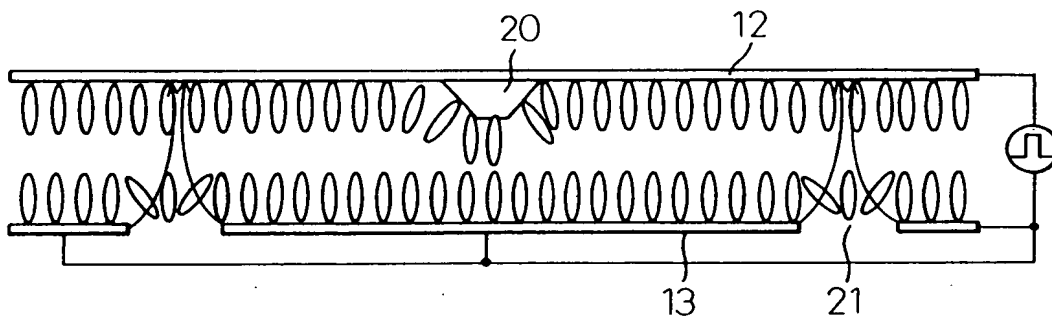


Fig. 39

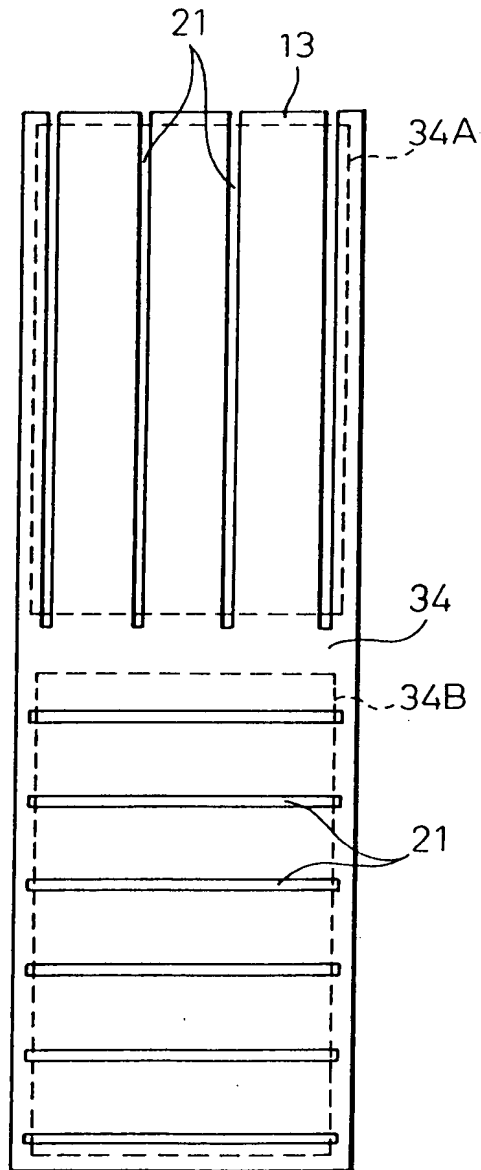


Fig.40

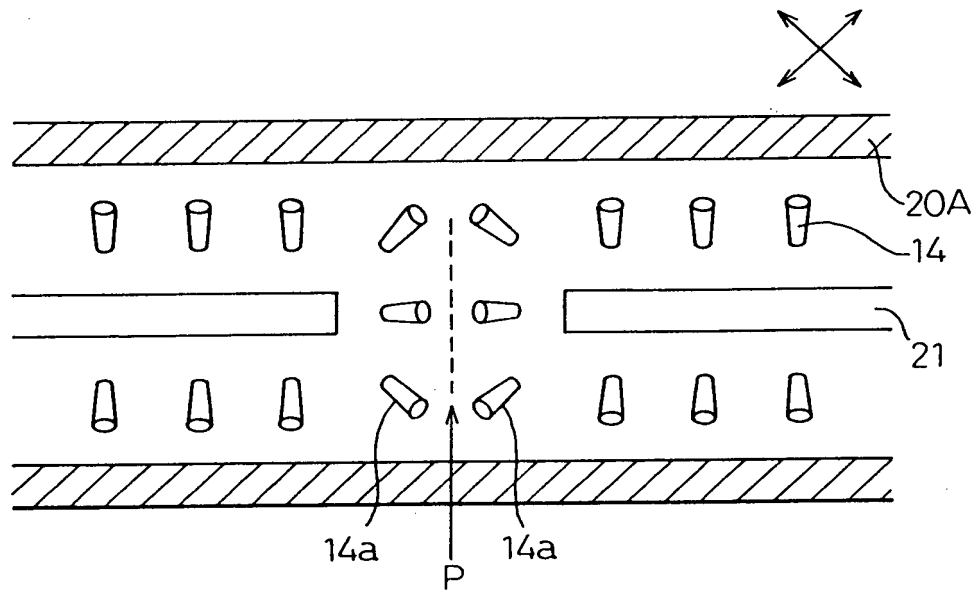
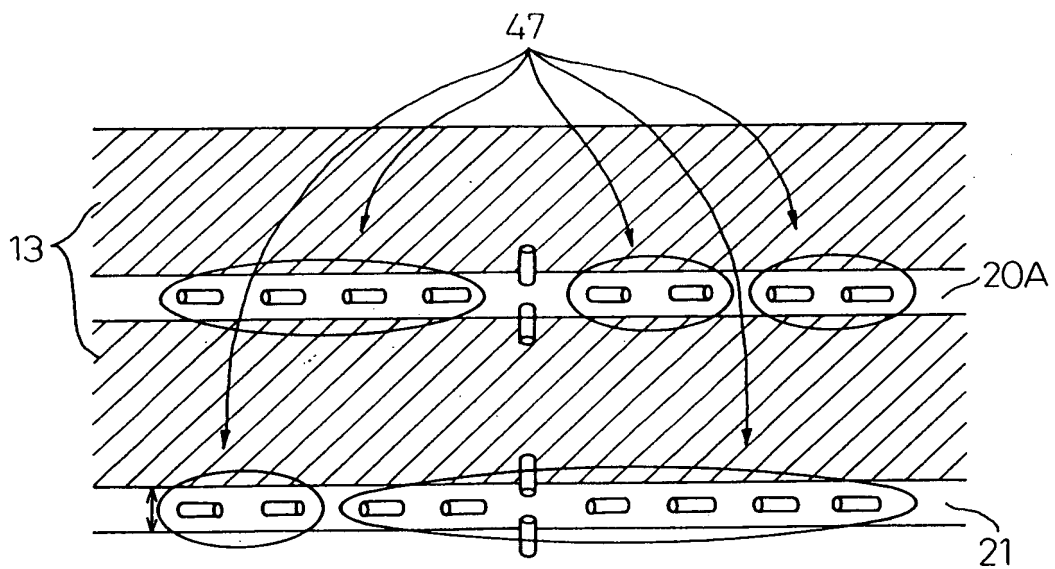


Fig.41



40/246

Fig. 42

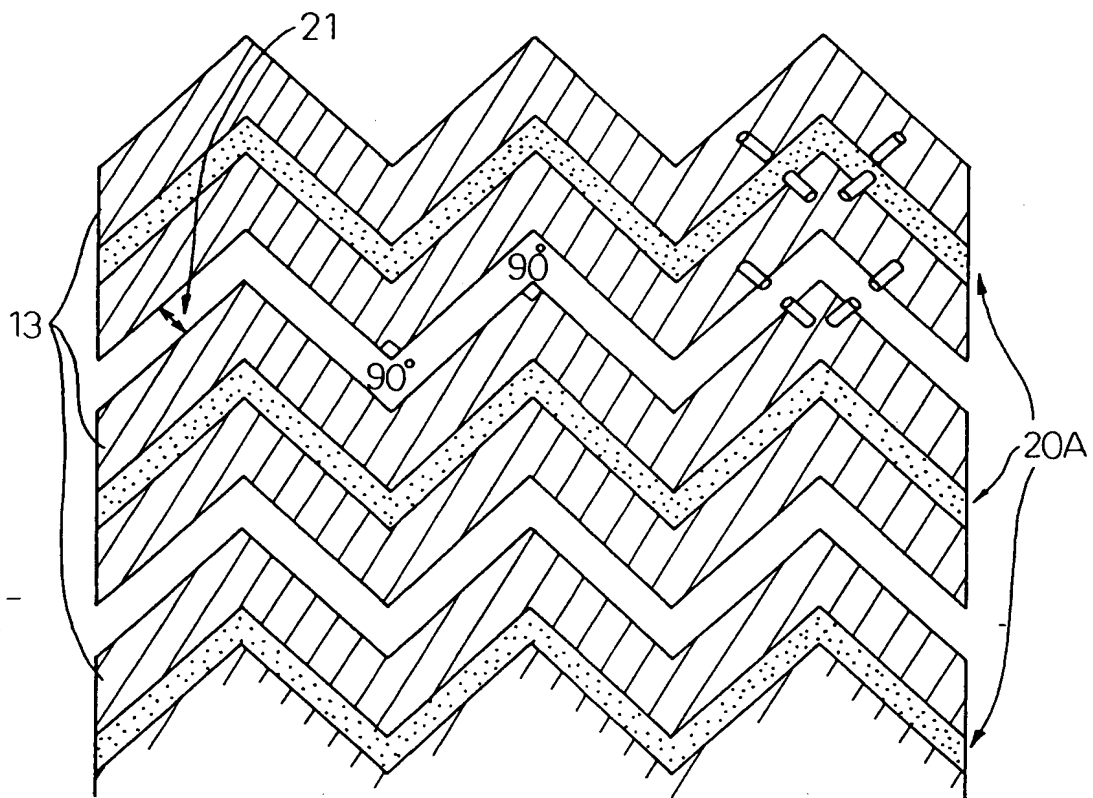
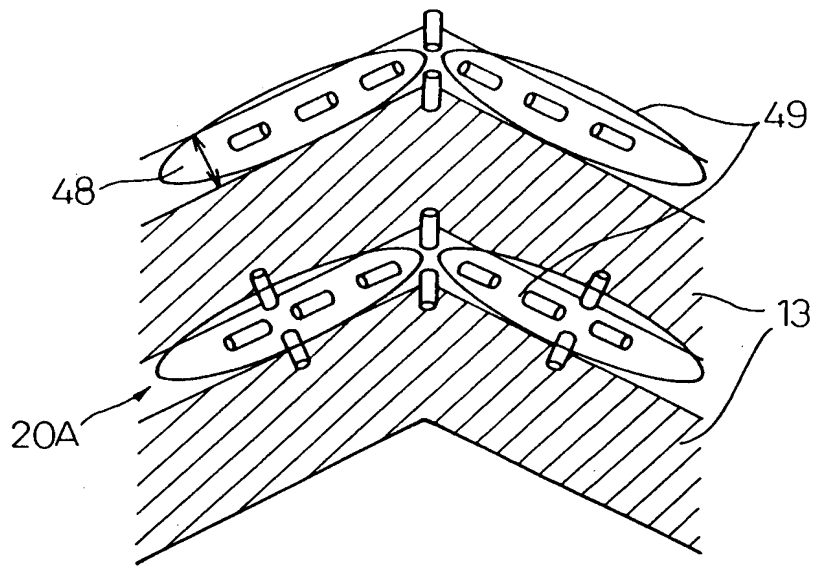


Fig. 43



42/246

Fig. 44

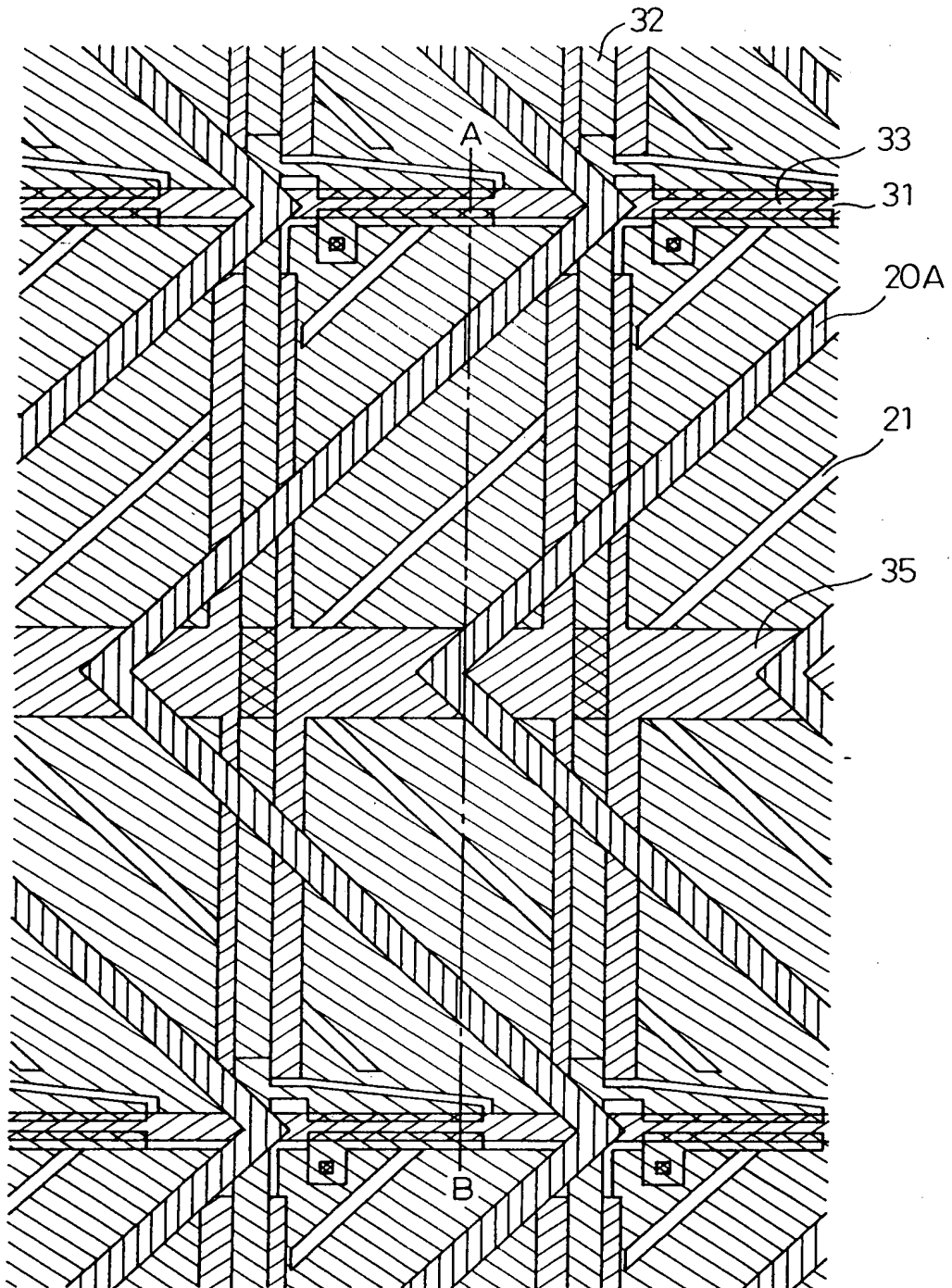


Fig. 45

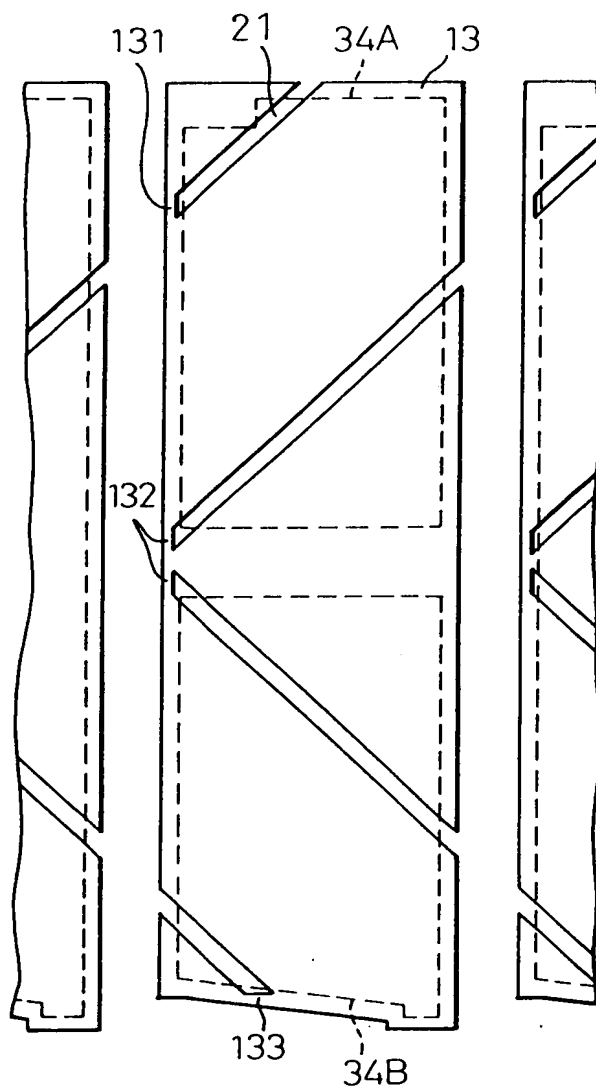
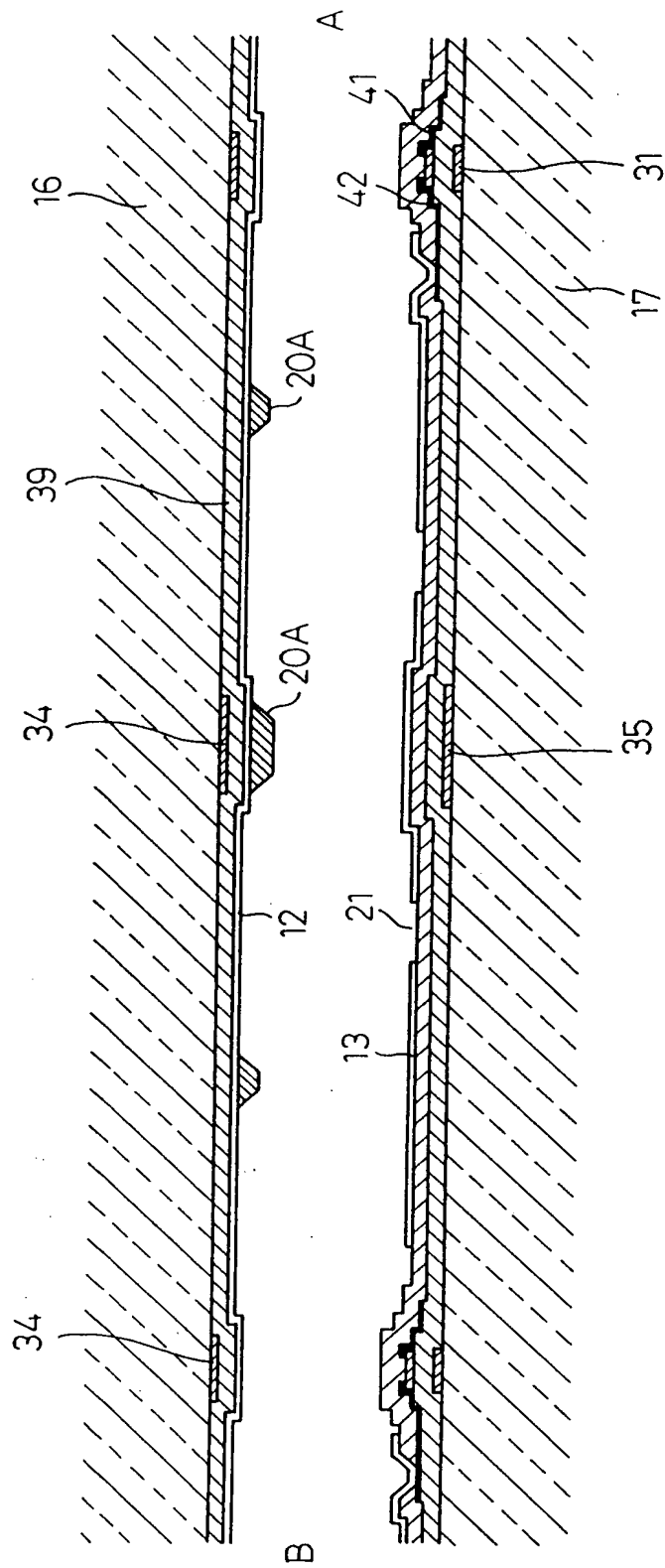
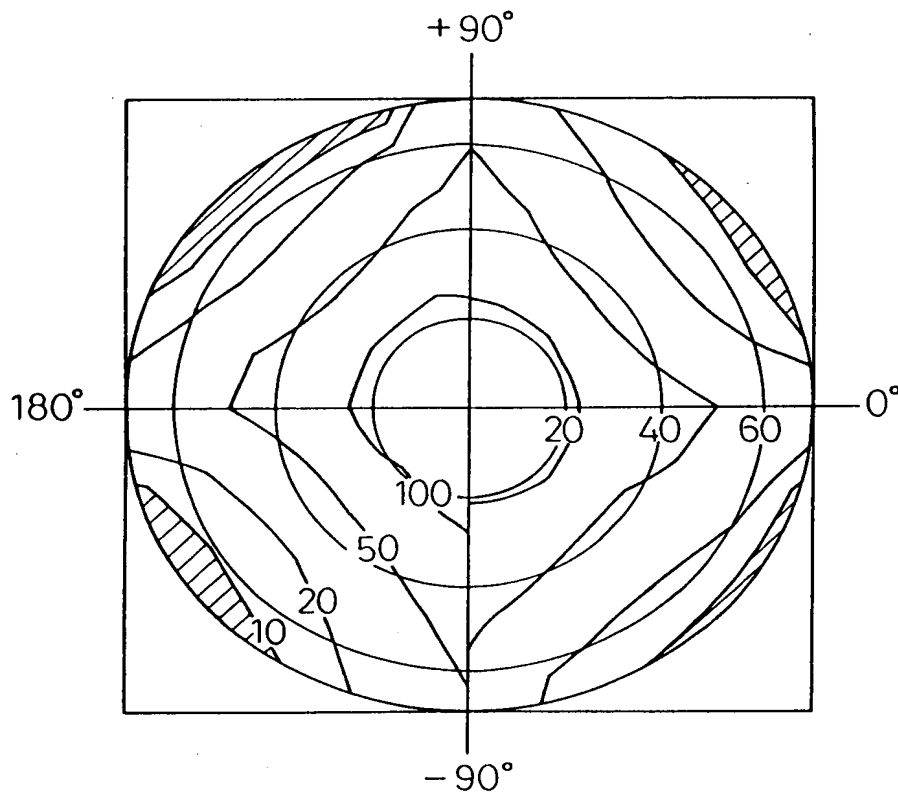


Fig. 46



45/246

Fig.47



46/
246

Fig.48A

-90°

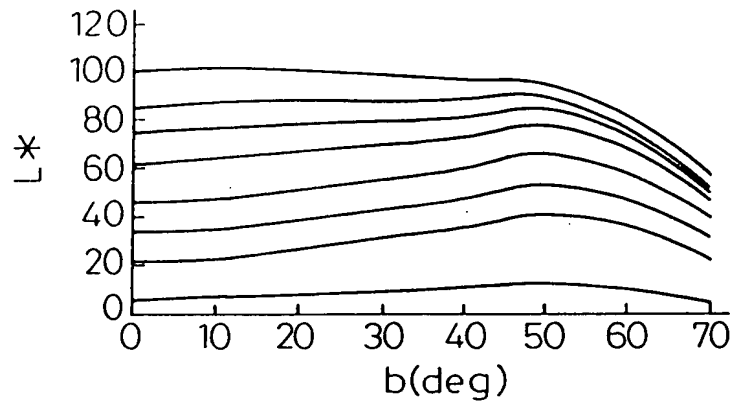


Fig.48B

-45°

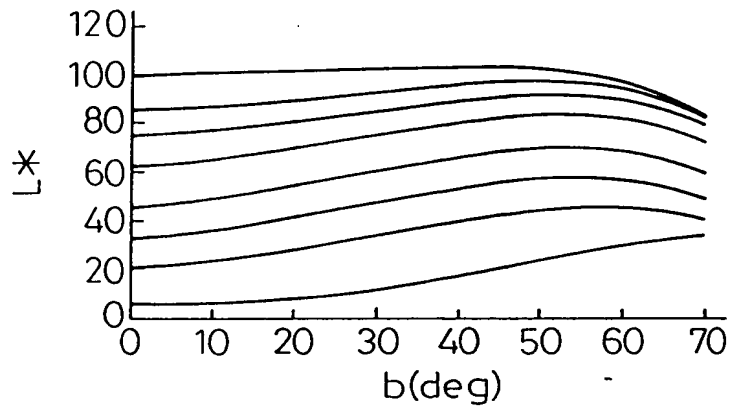


Fig.48C

0°

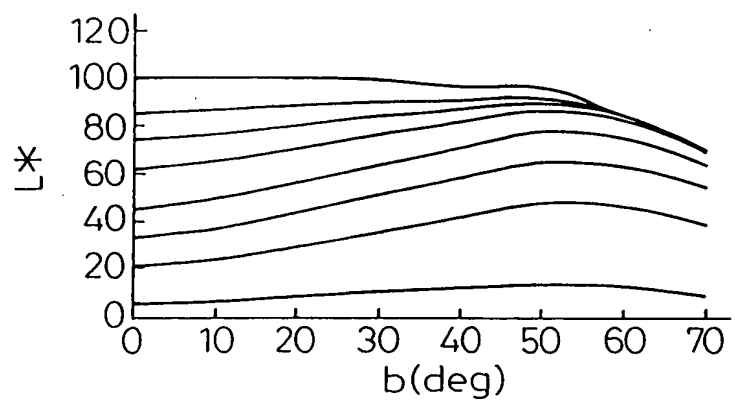


Fig.49A

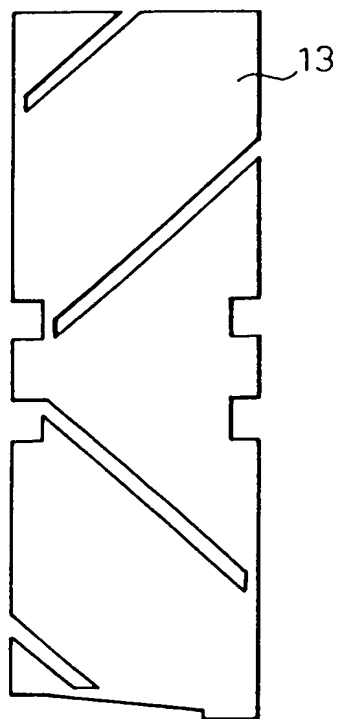


Fig.49B

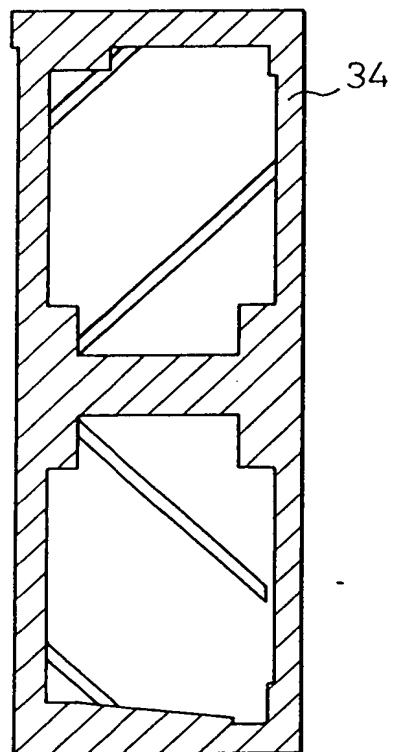


Fig.50A

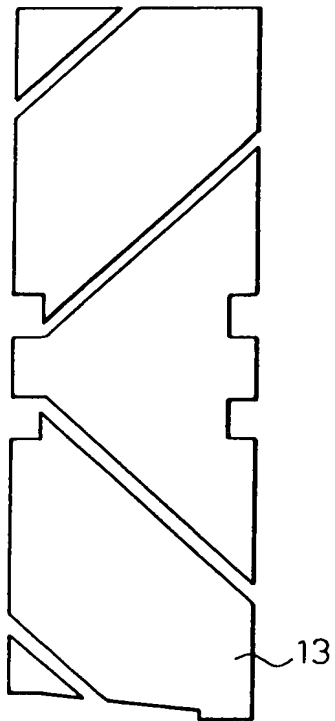
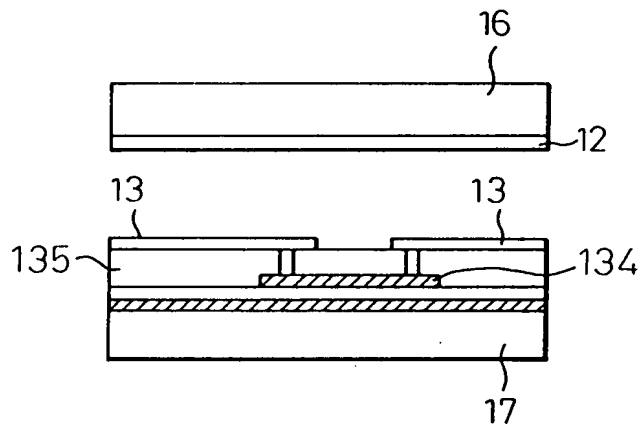
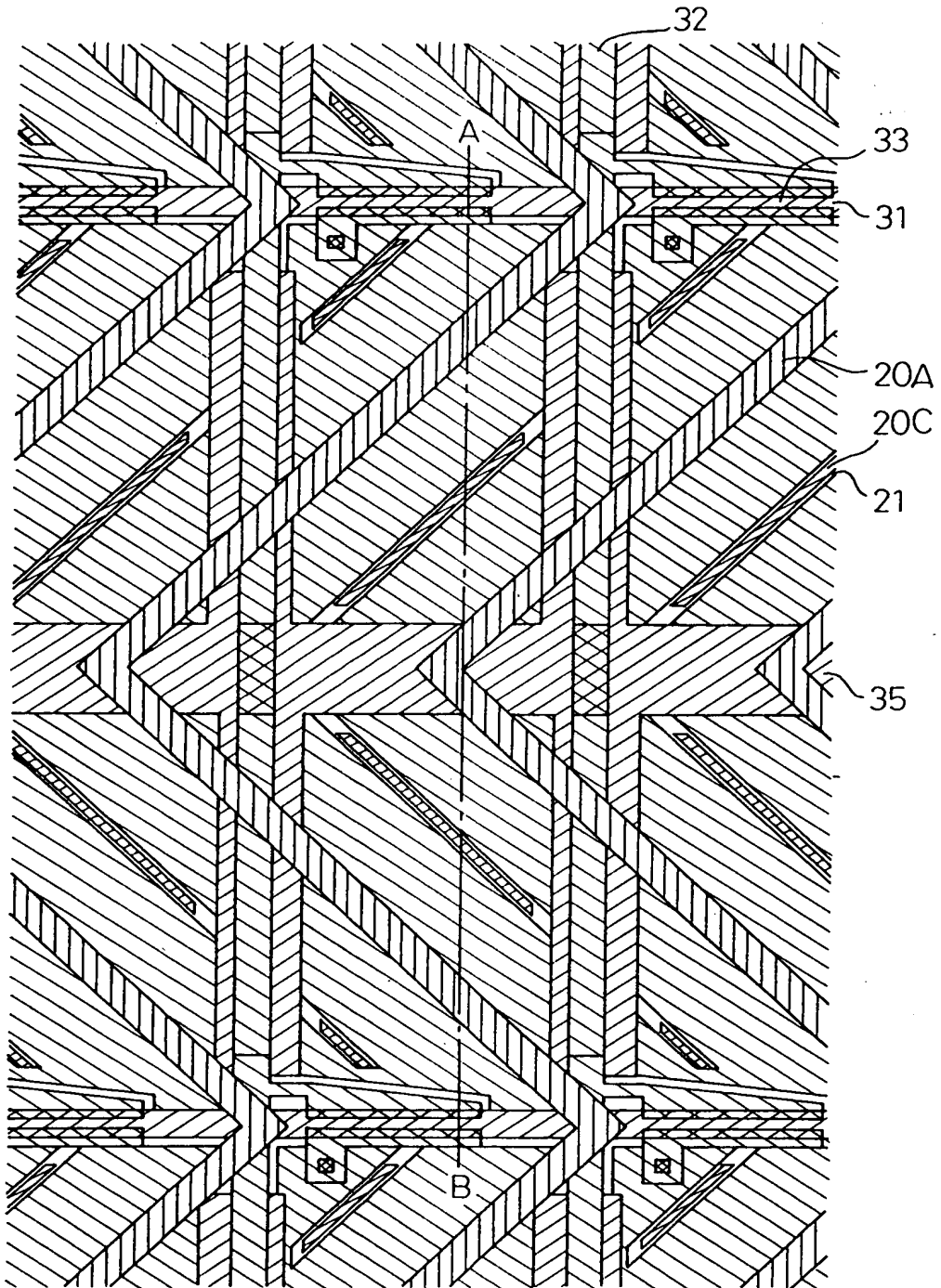


Fig.50B



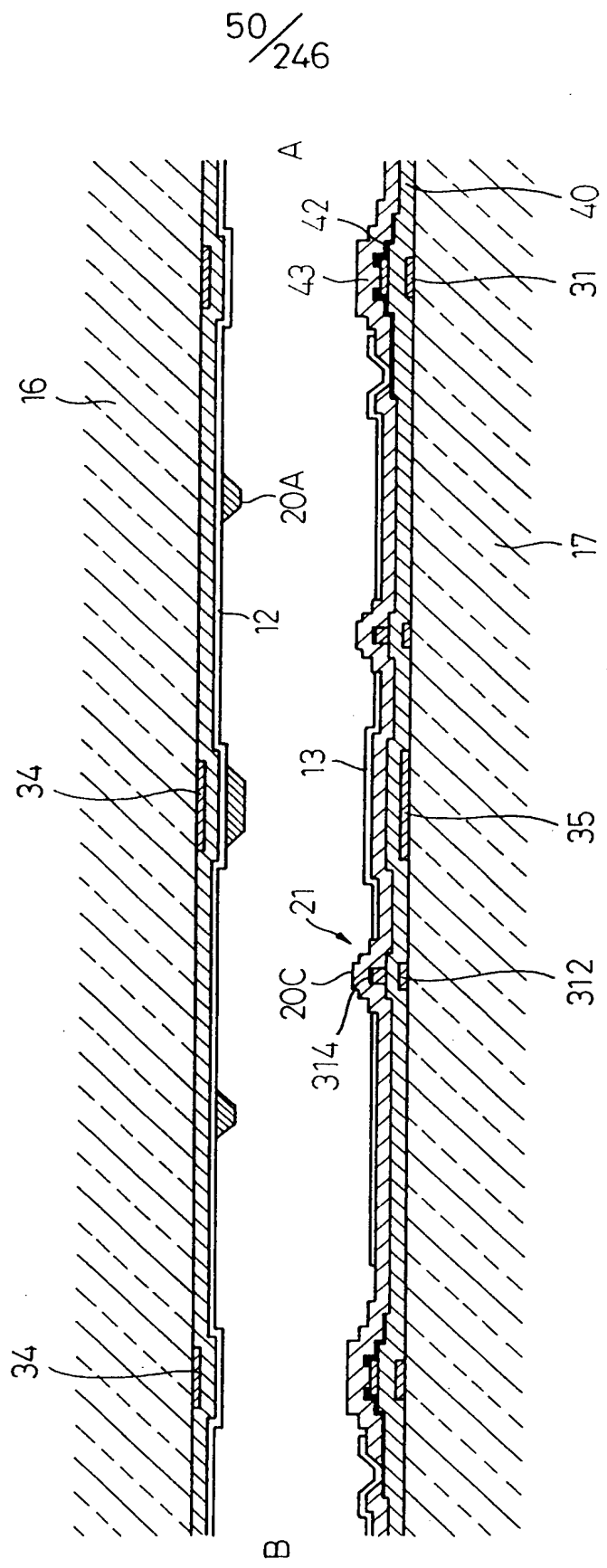
49/246

Fig. 51



50/246

Fig. 52



51/246

Fig.53A

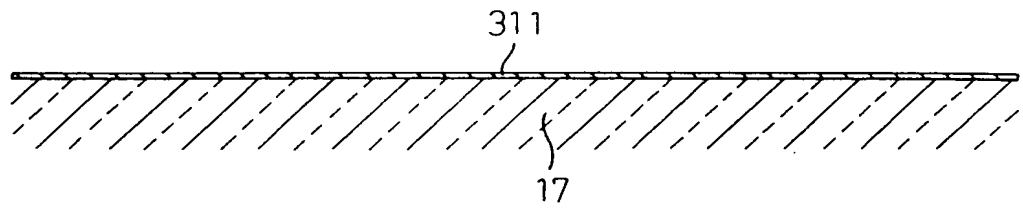


Fig.53B

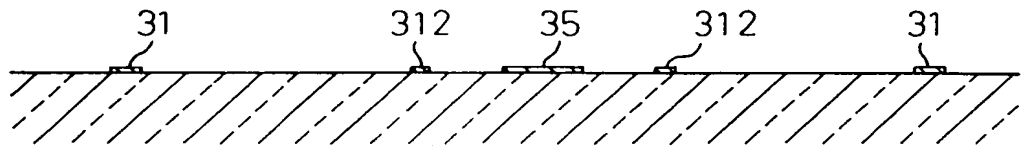


Fig.53C

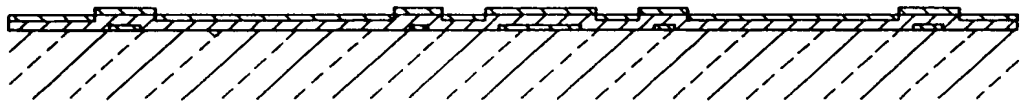


Fig.53D

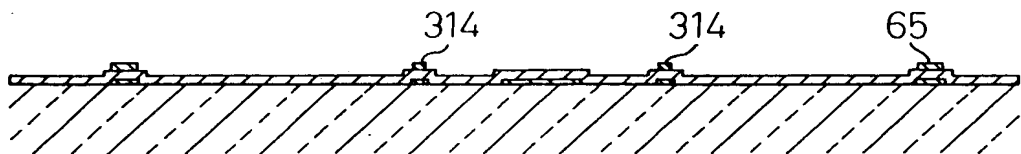


Fig.53E

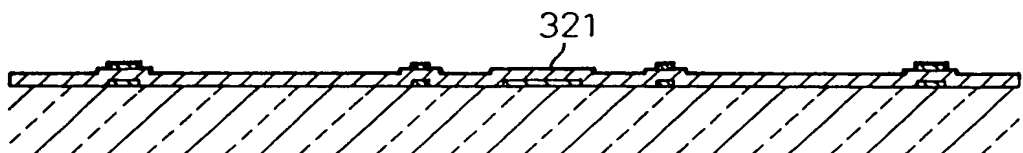


Fig. 53F

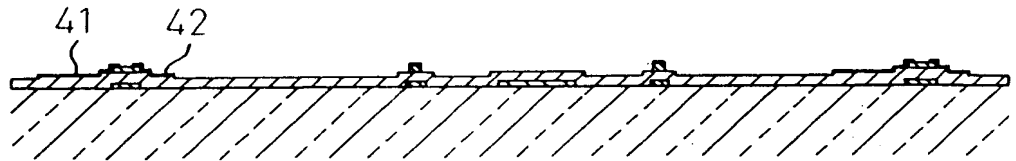


Fig. 53G

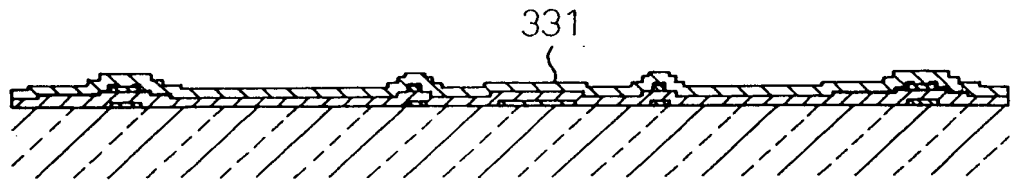


Fig. 53H

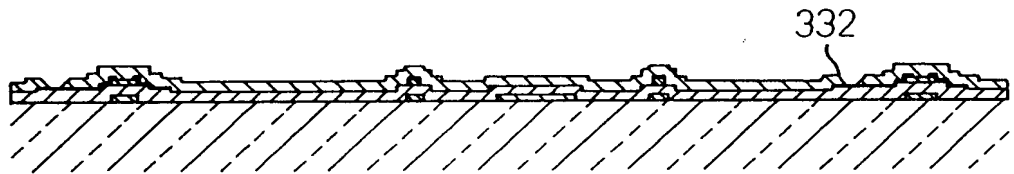


Fig. 53I

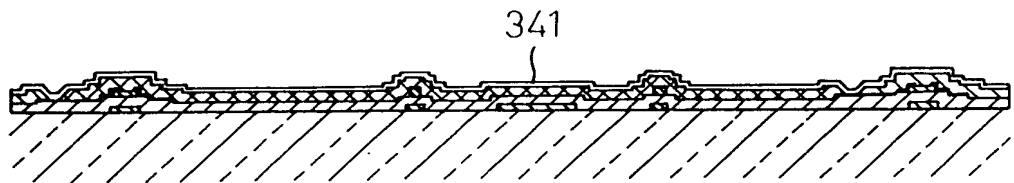


Fig. 53J

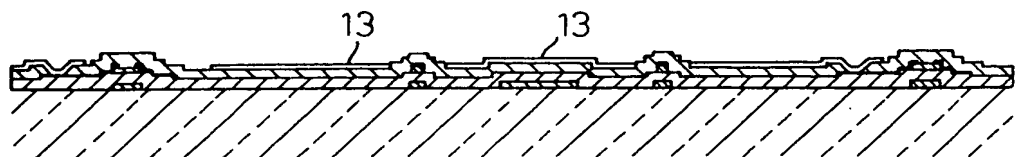
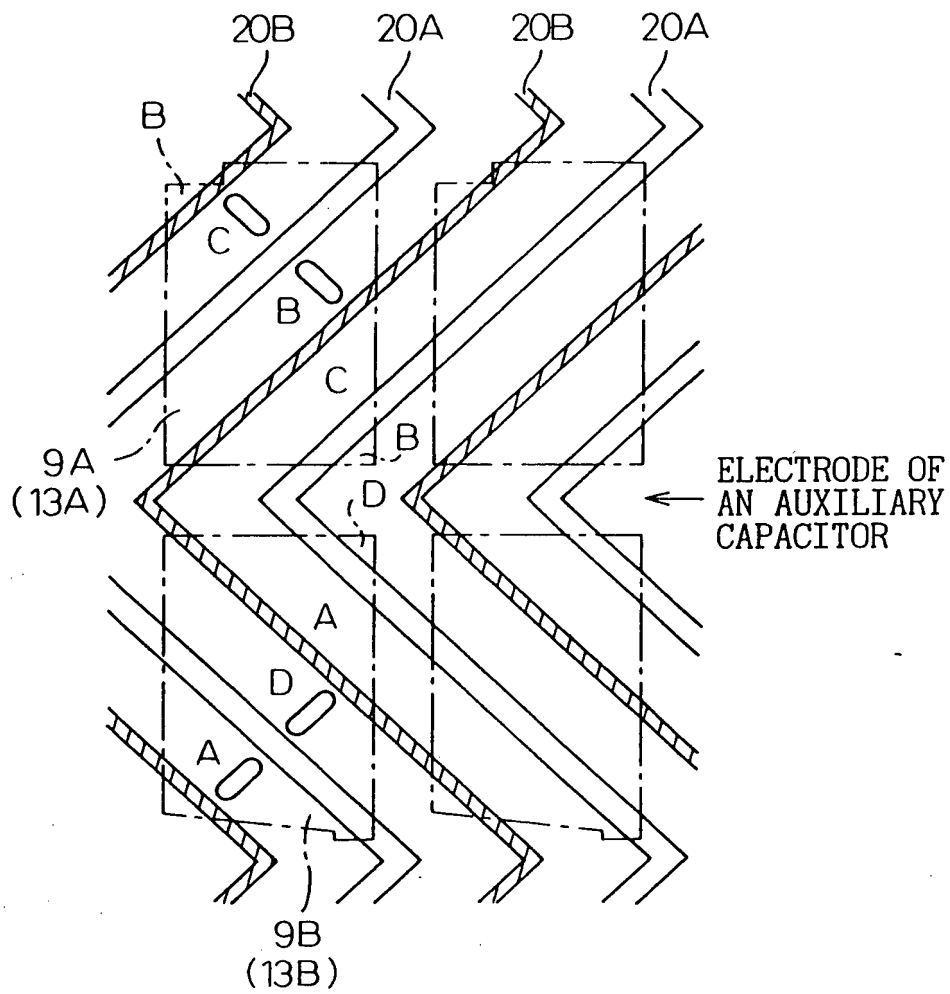


Fig. 54



54/246

Fig. 55

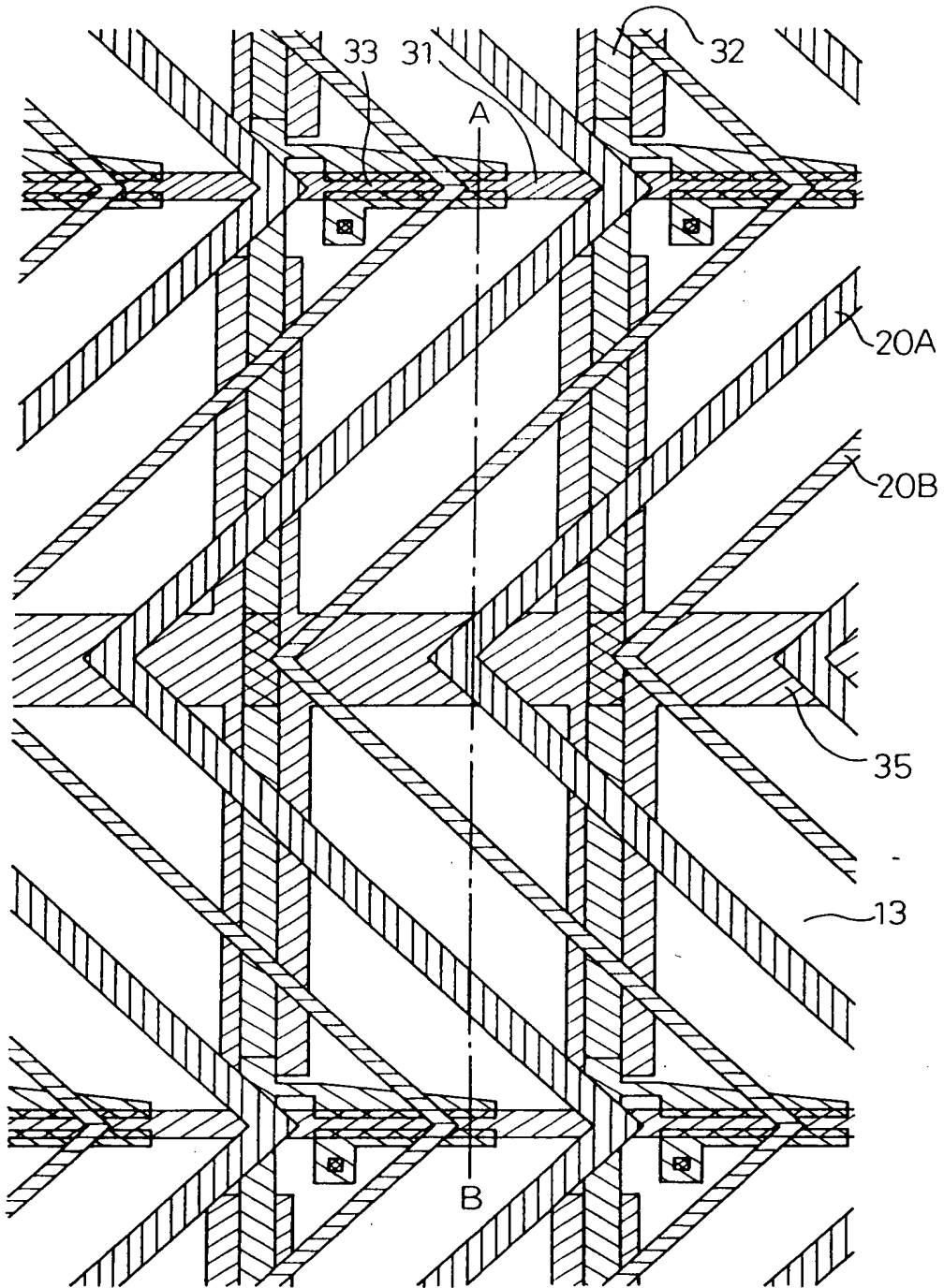




Fig. 57A

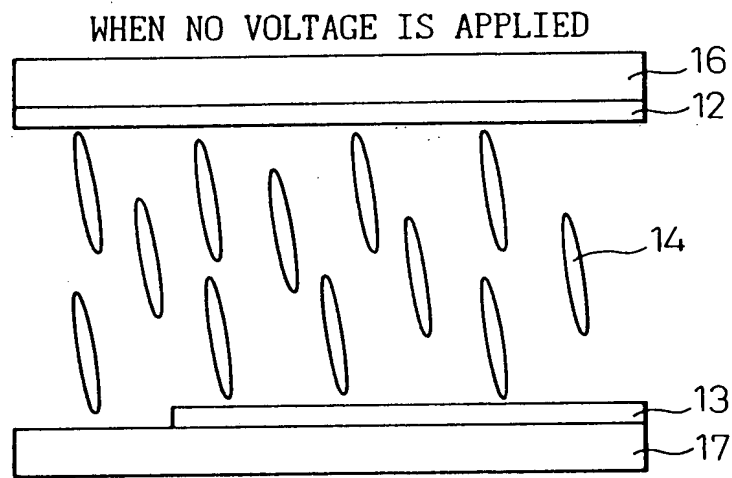
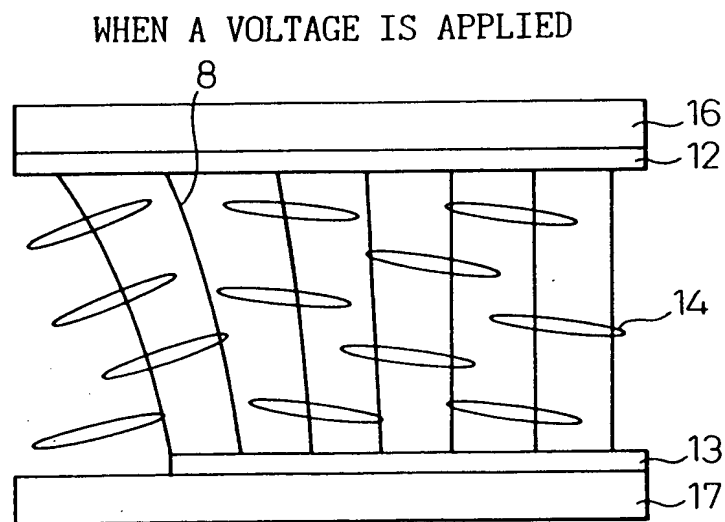


Fig. 57B



57/246

Fig. 58

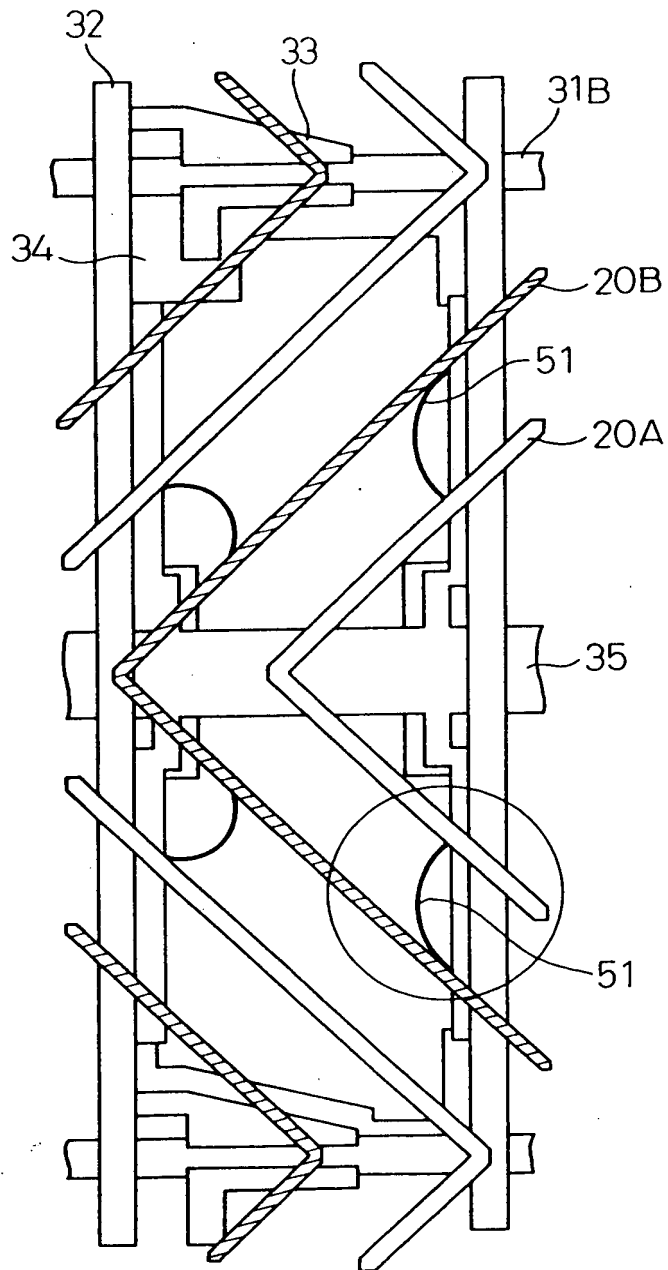


Fig. 59

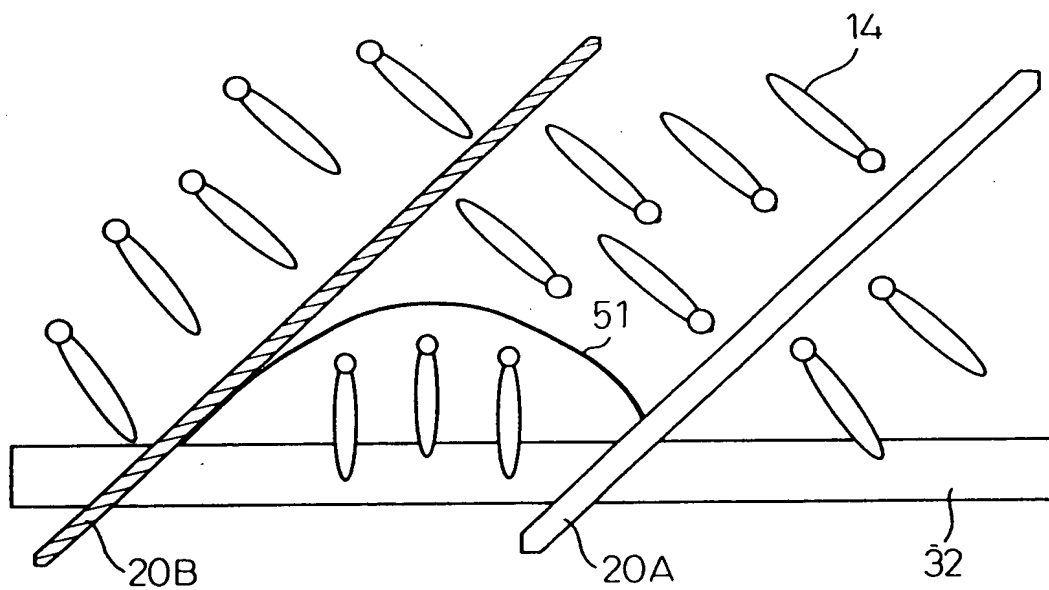
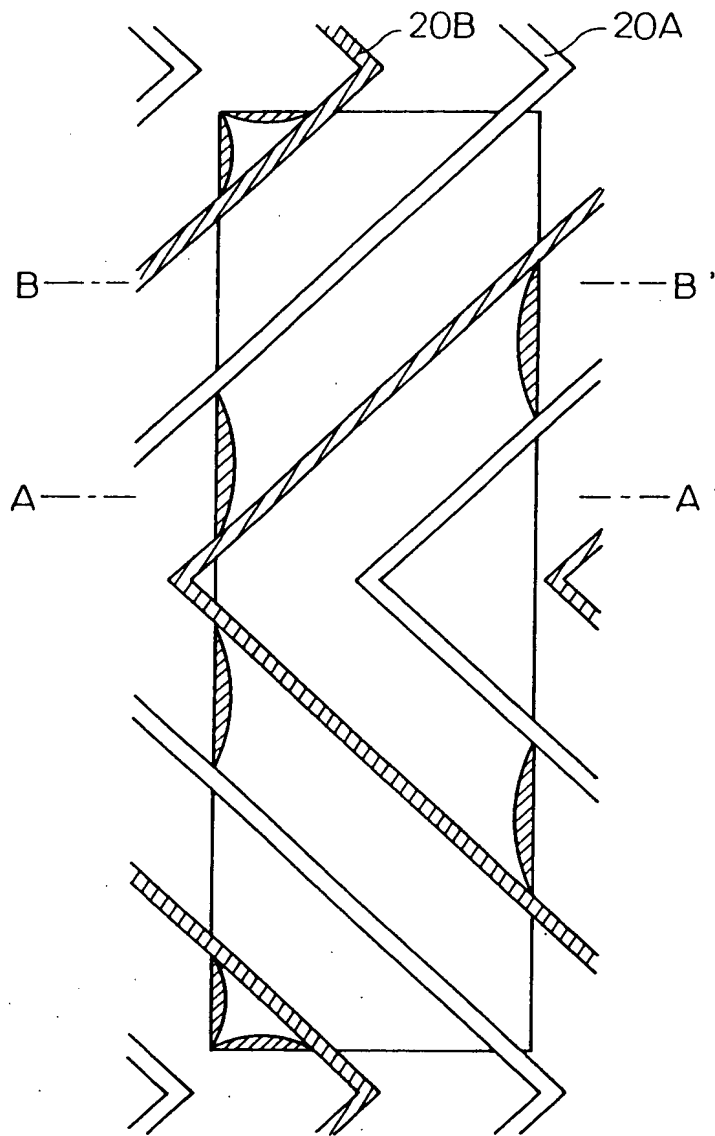


Fig. 60



60/246

Fig. 61A

A - A'

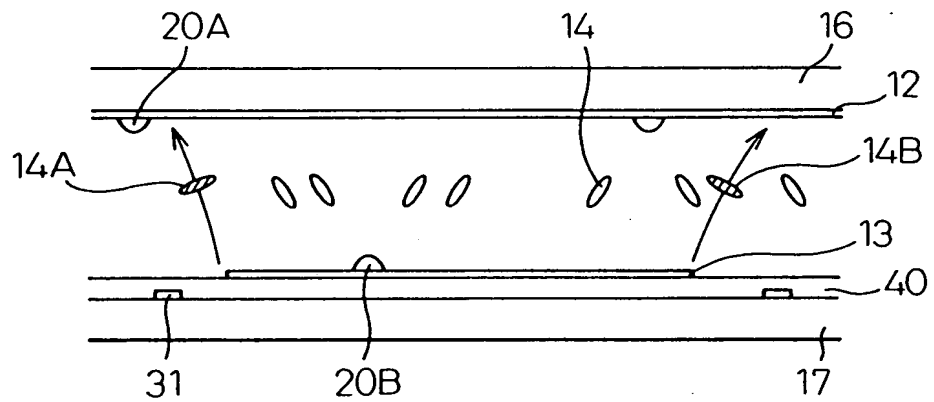


Fig. 61B

B - B'

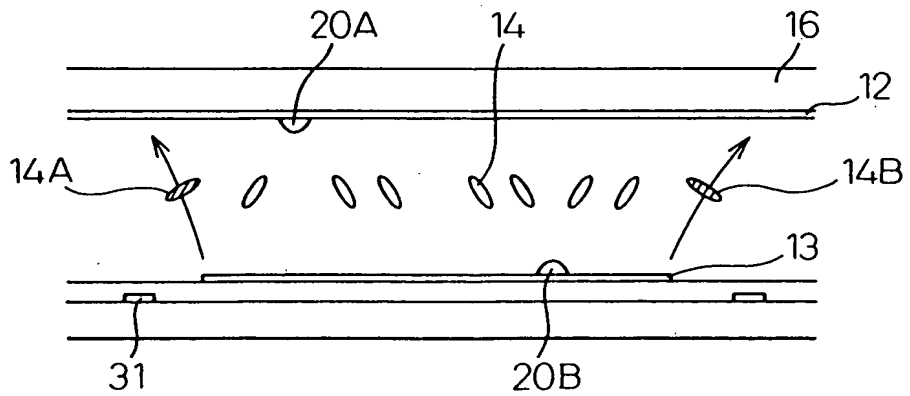


Fig.62A

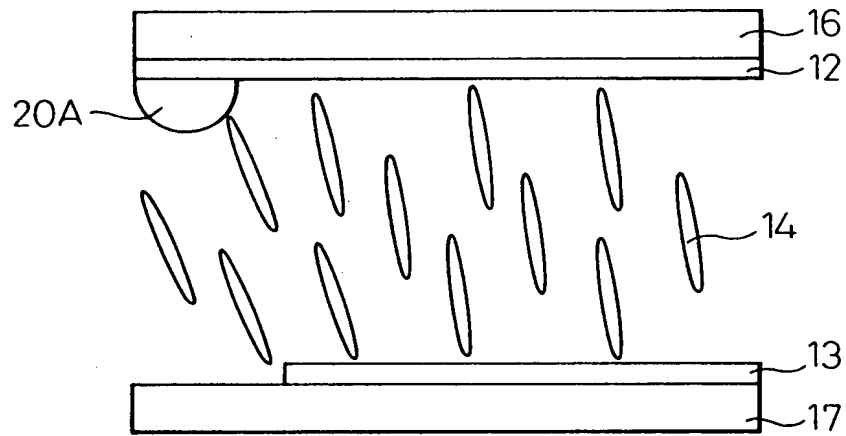


Fig.62B

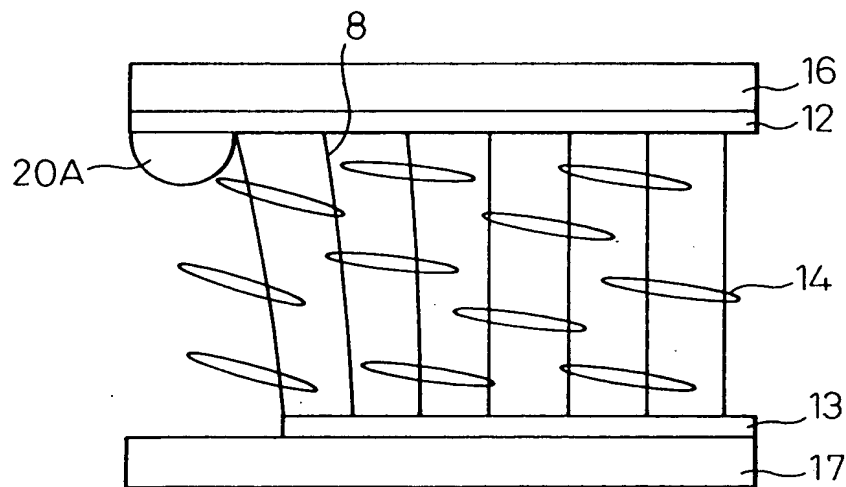
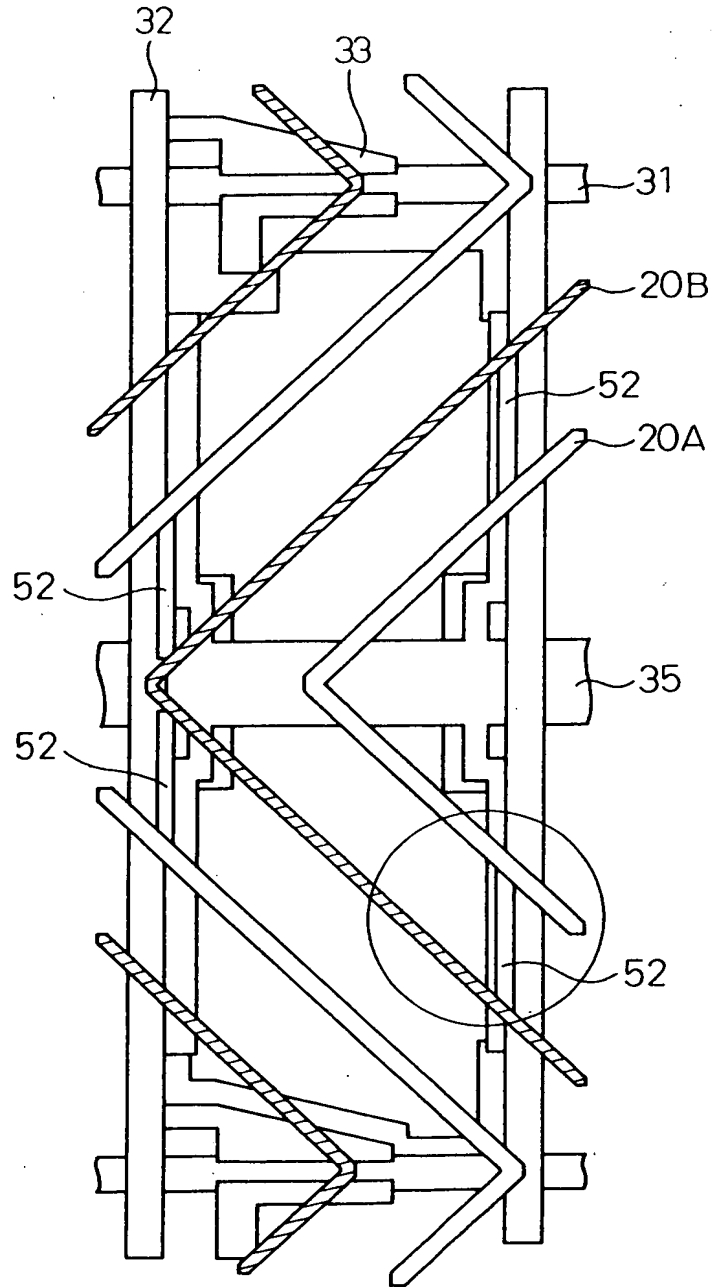
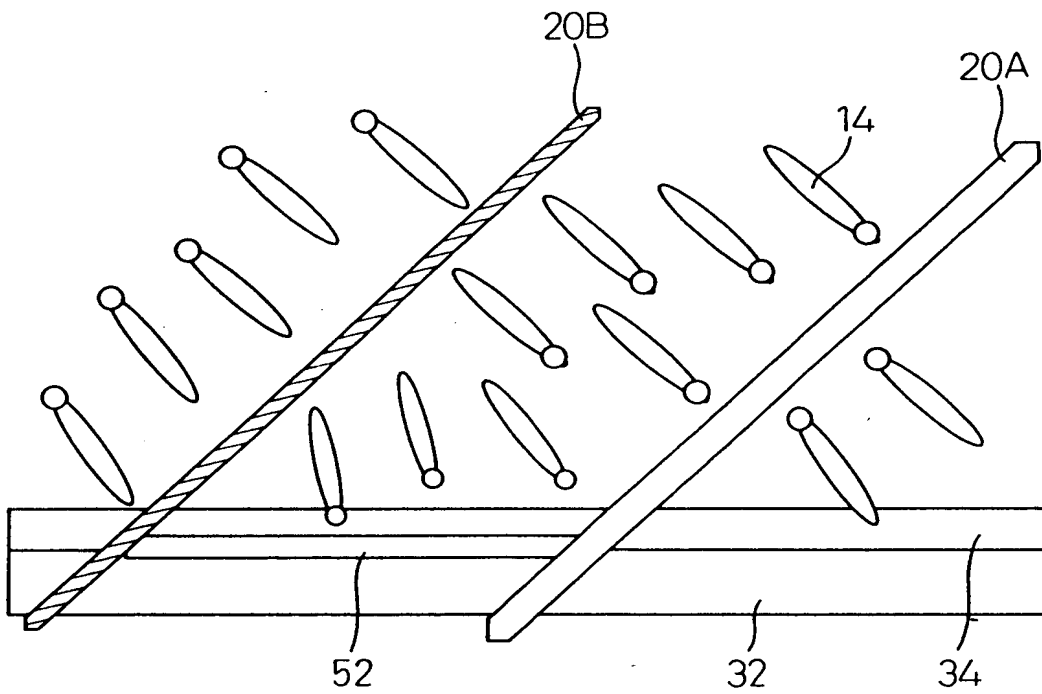


Fig. 63



62/246-326326

Fig.64



64/246

Fig. 65A

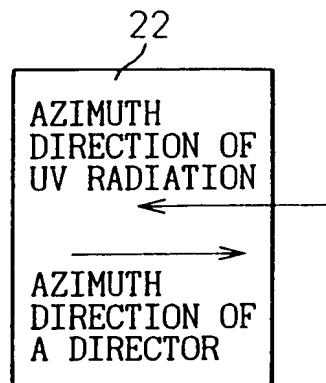
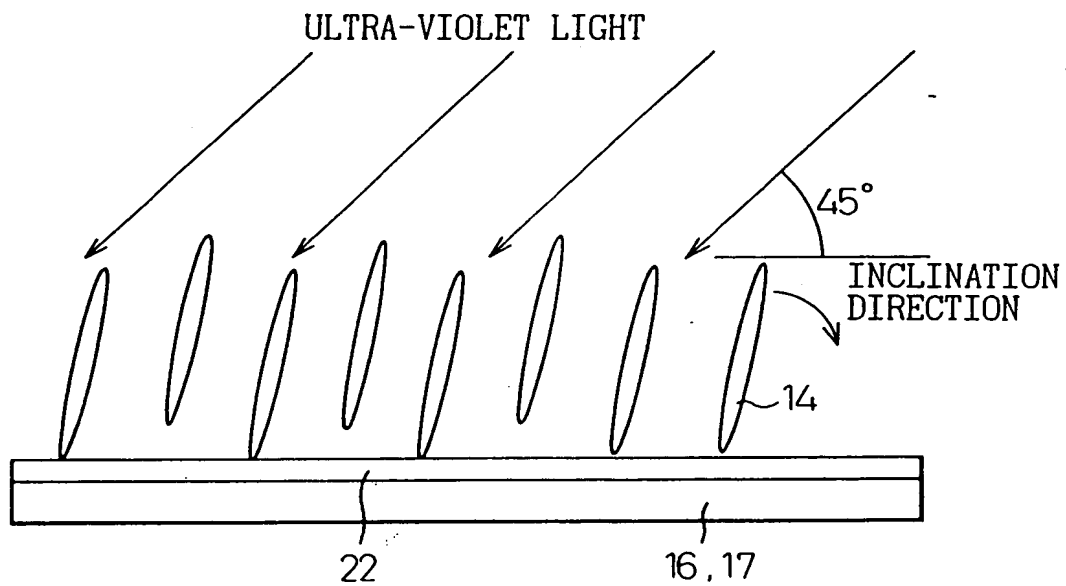


Fig. 65B



65/
246

Fig. 66

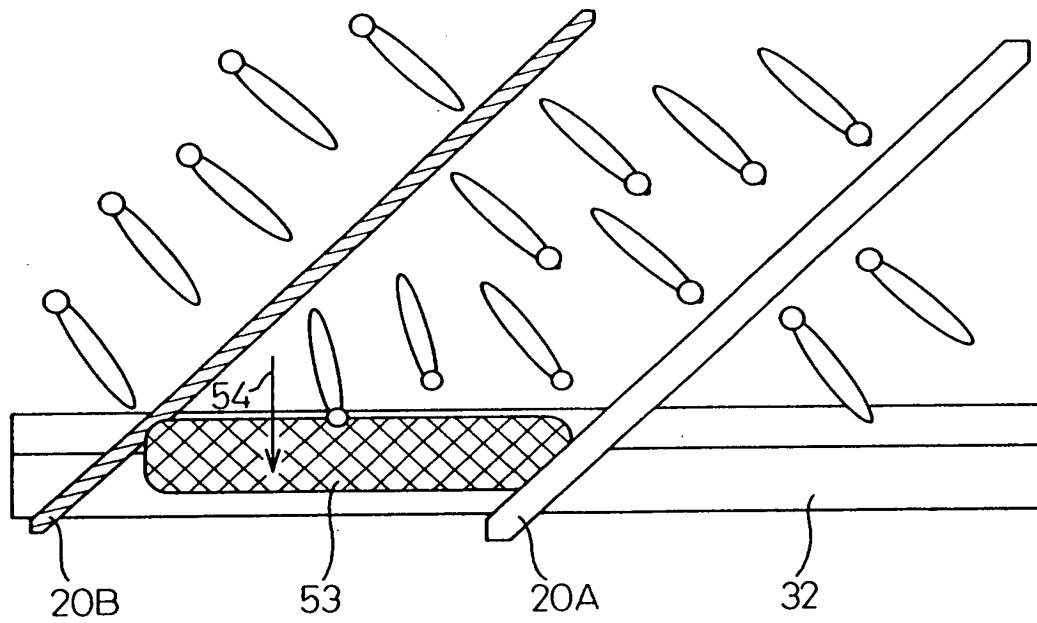


Fig.67A

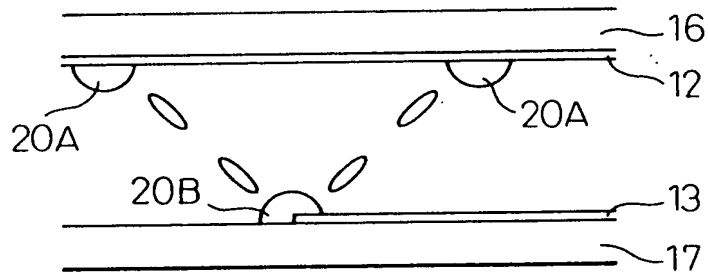


Fig.67B

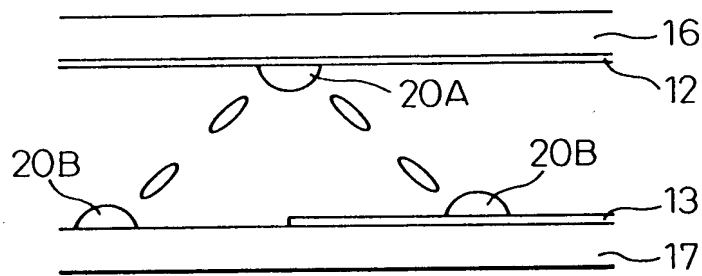


Fig.67C

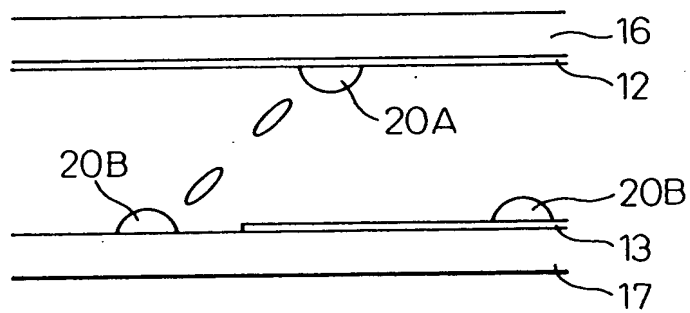


Fig. 68

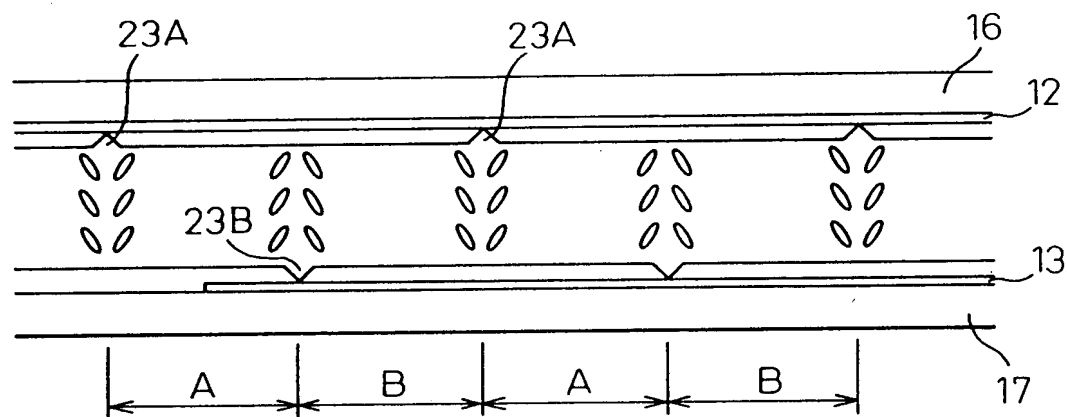


Fig. 69A

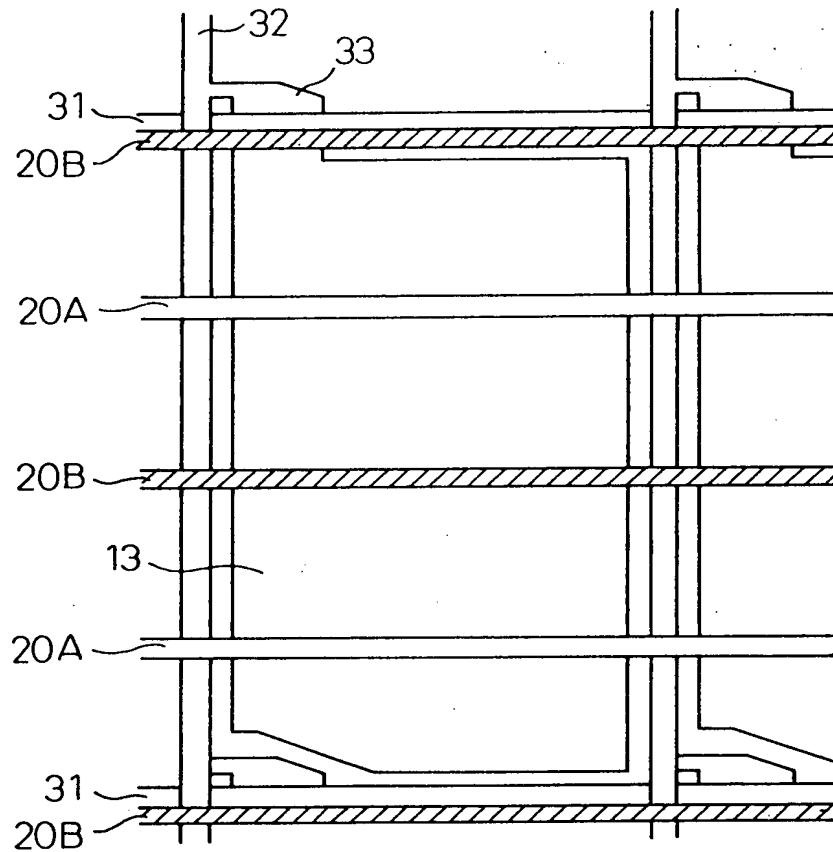


Fig. 69B

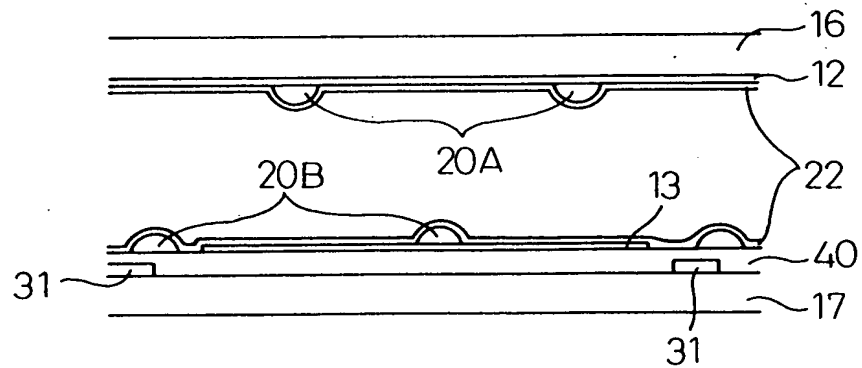


Fig.70A

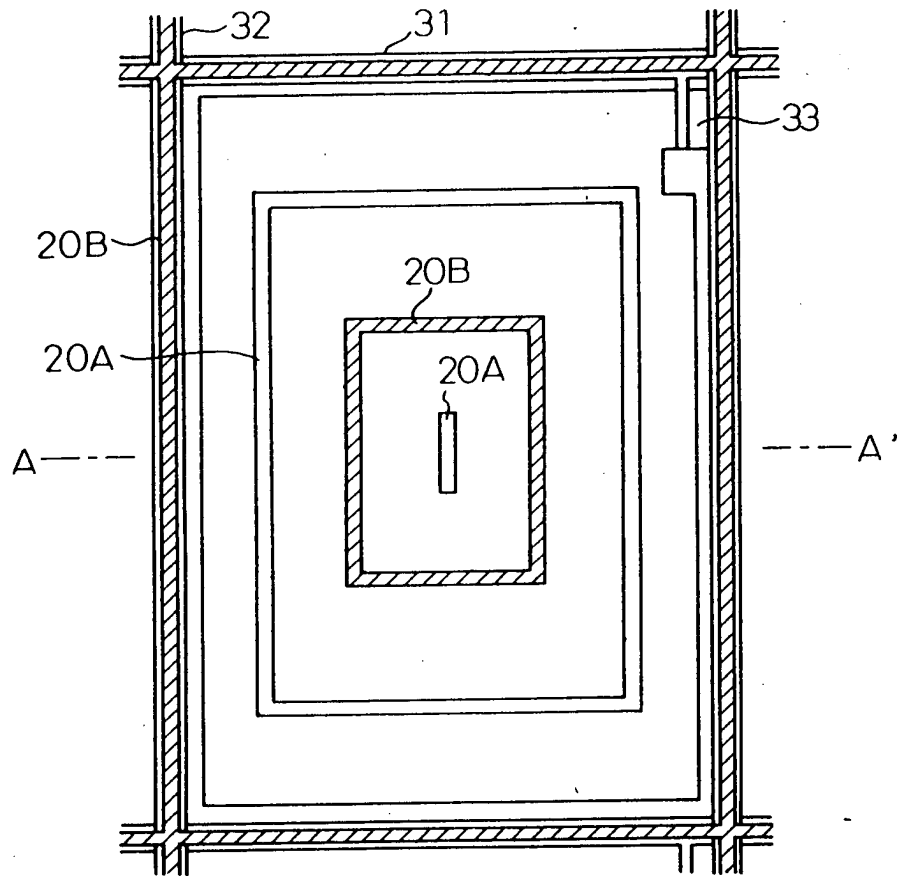


Fig.70B

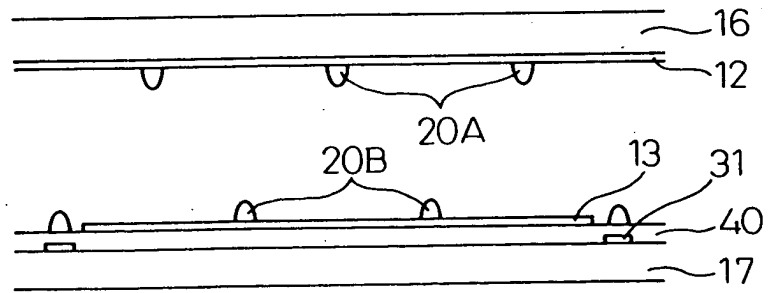


Fig.71

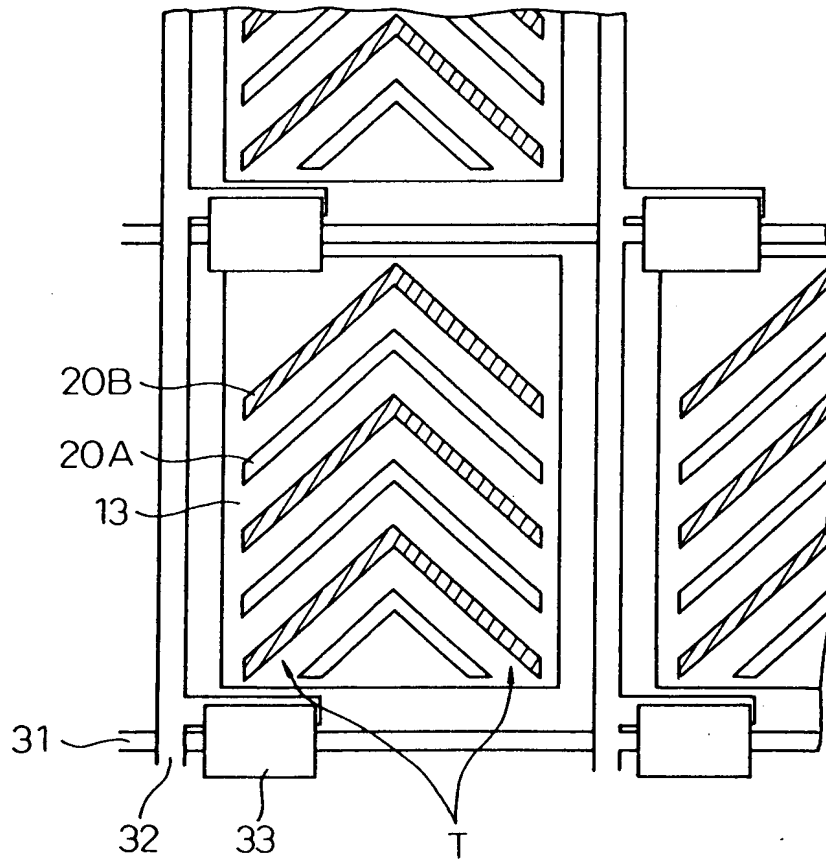
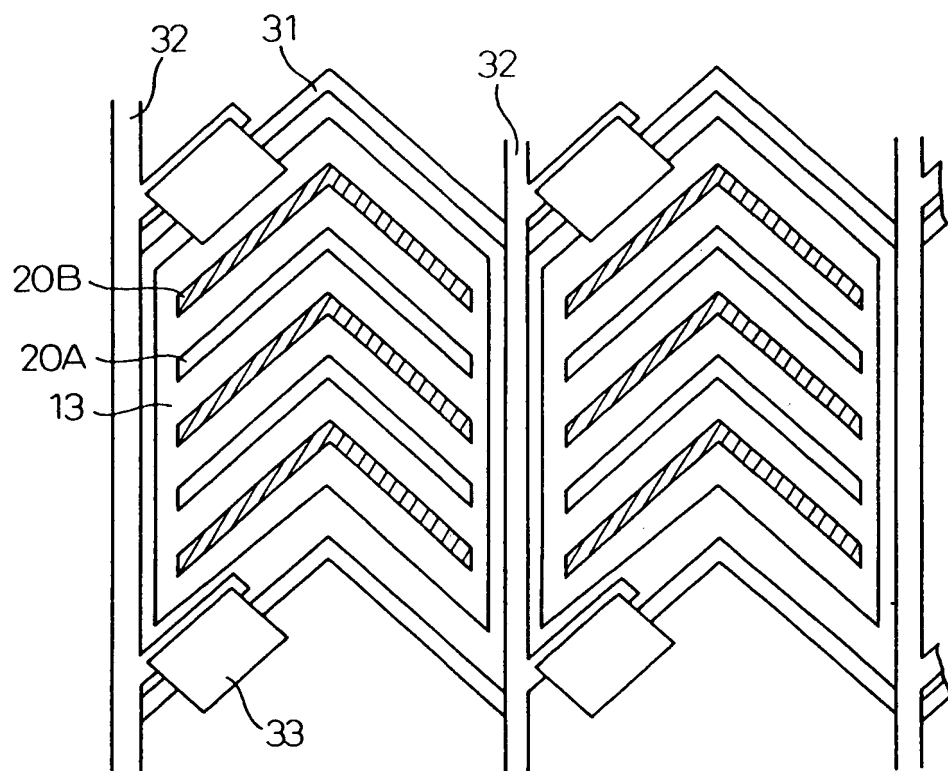
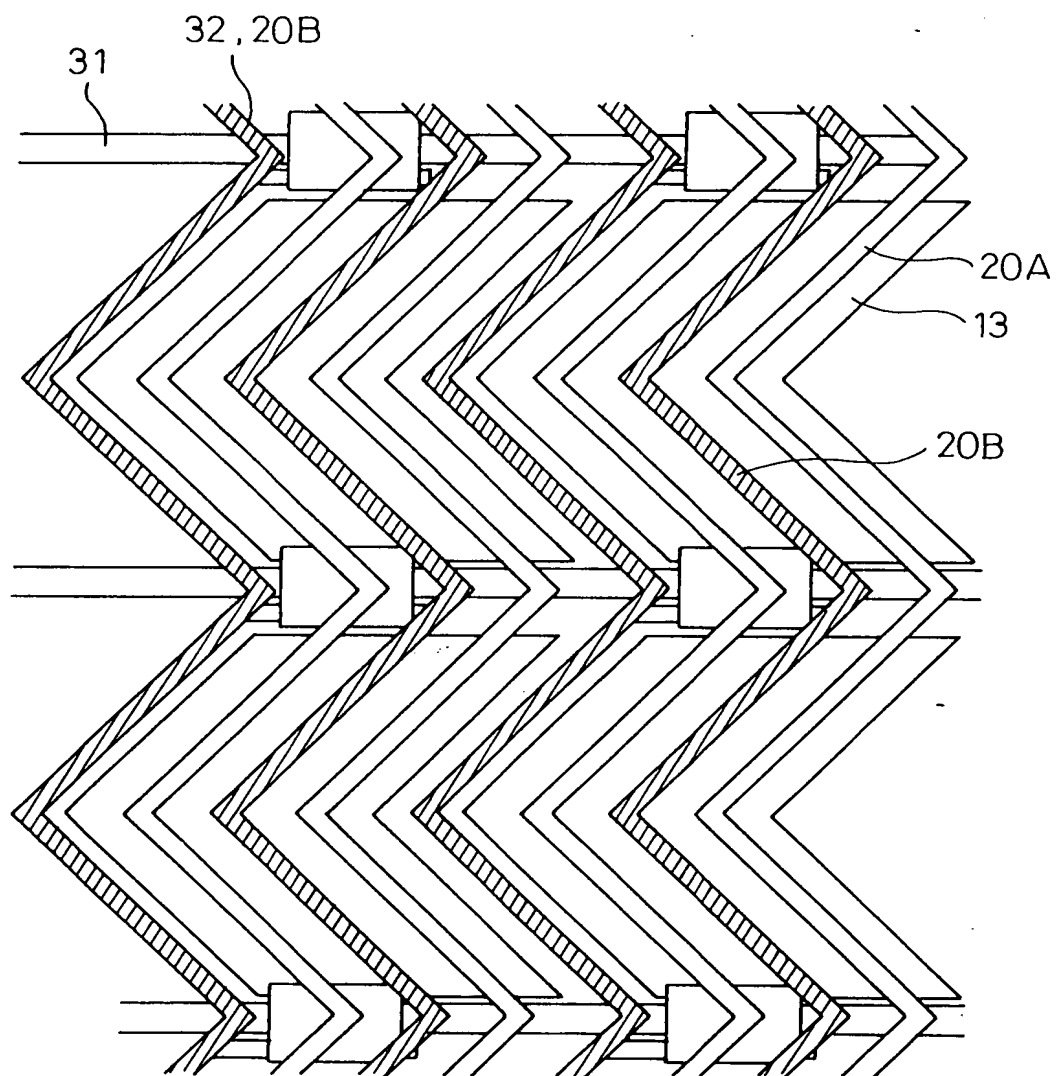


Fig. 72

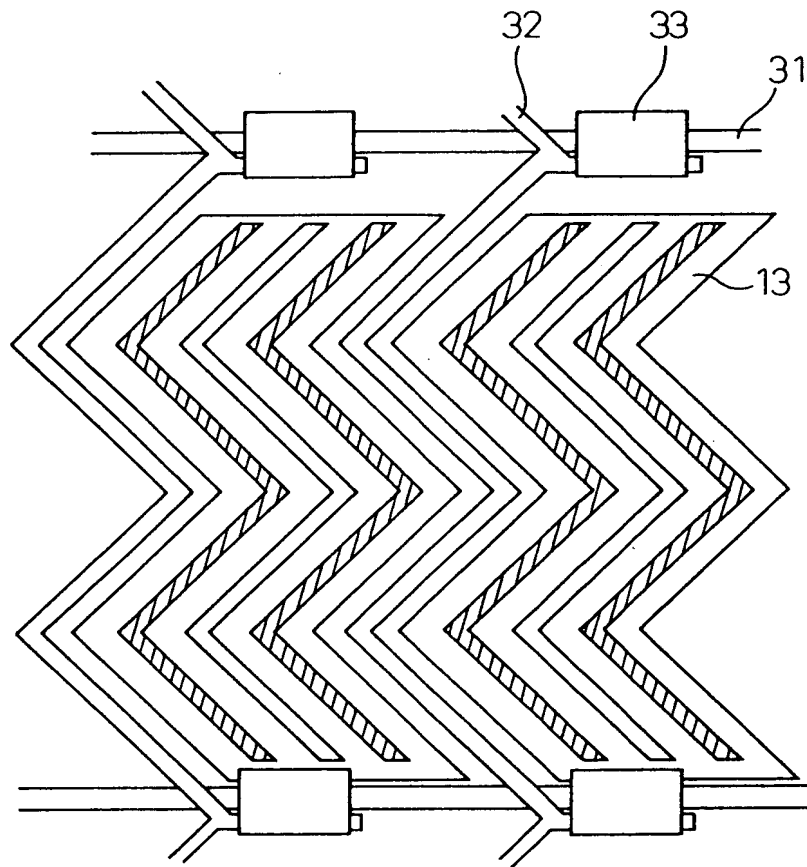


—



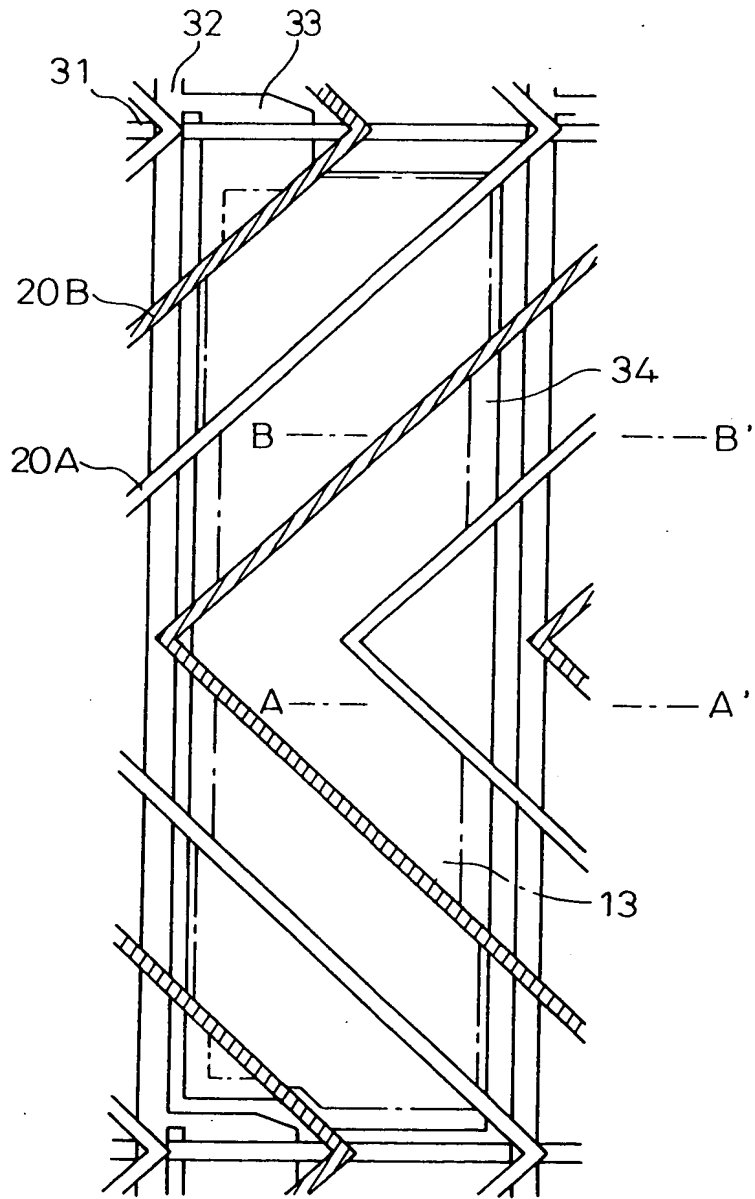
73/246

Fig. 74



74/246

Fig. 75



75/
246

Fig.76A

A-A'

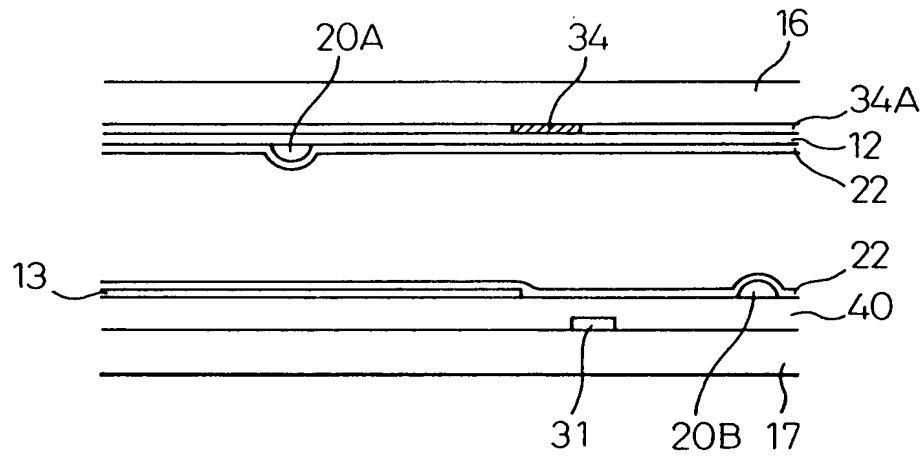


Fig.76B

B-B'

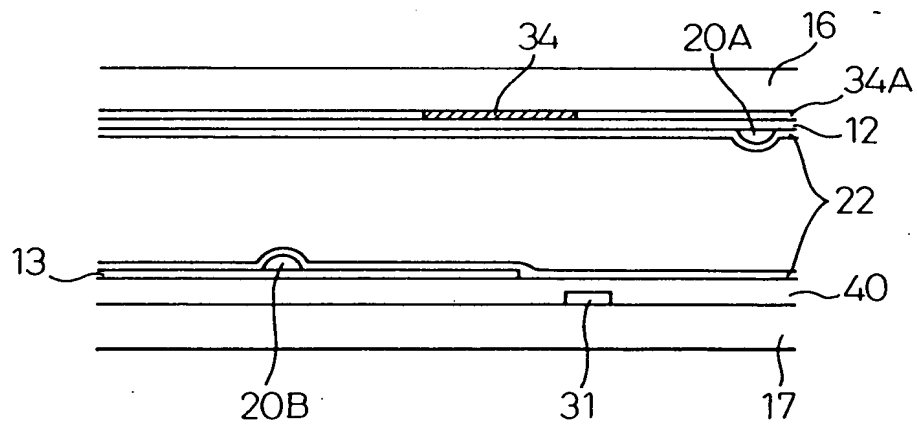


Fig.77A

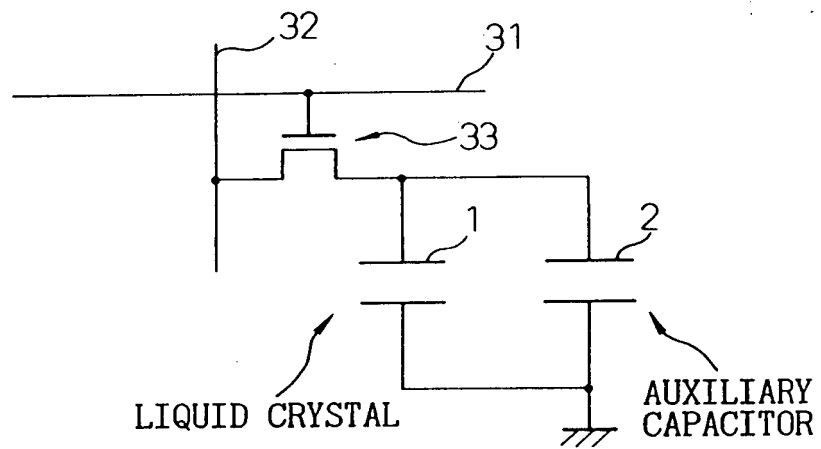


Fig.77B

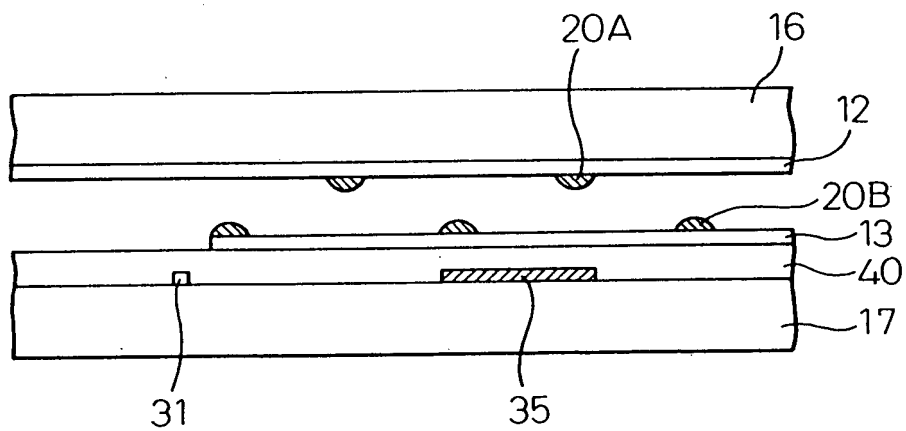


Fig.78A

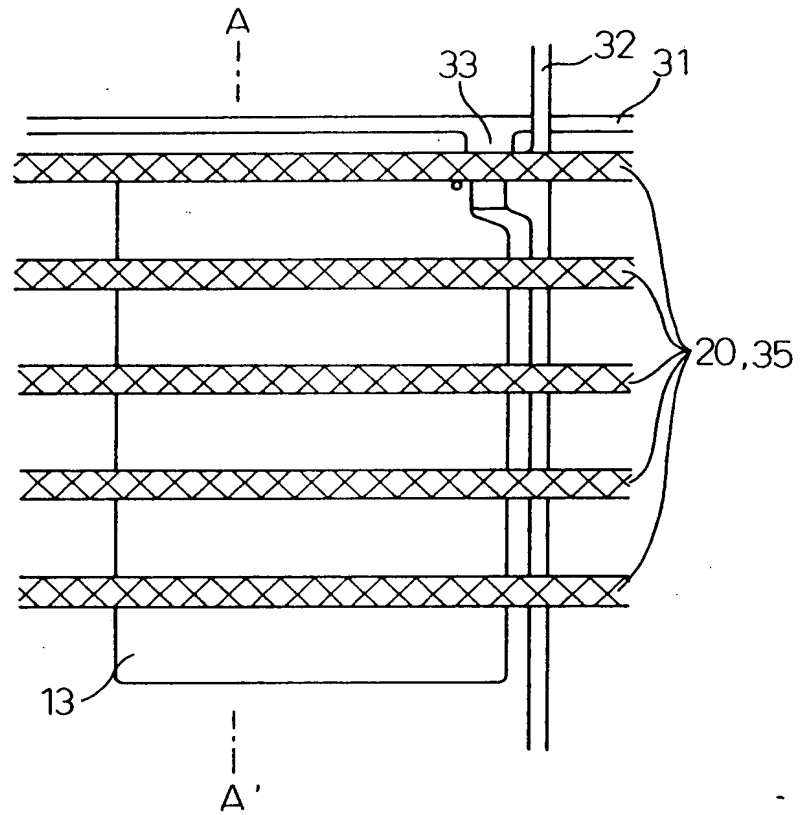
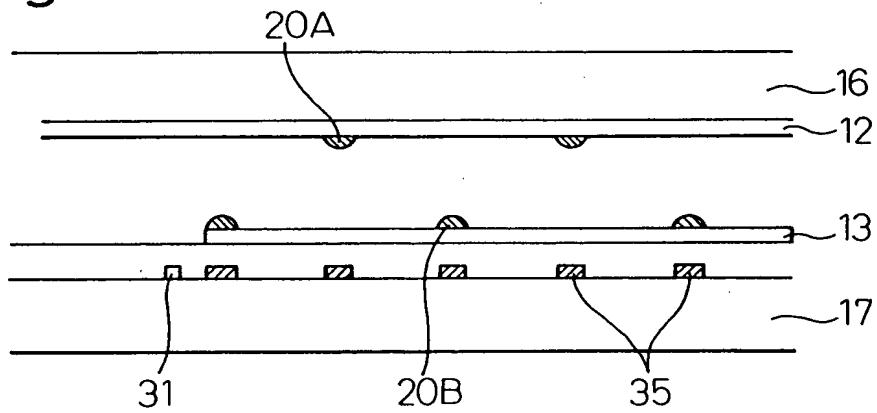


Fig.78B



78/246

Fig.79A

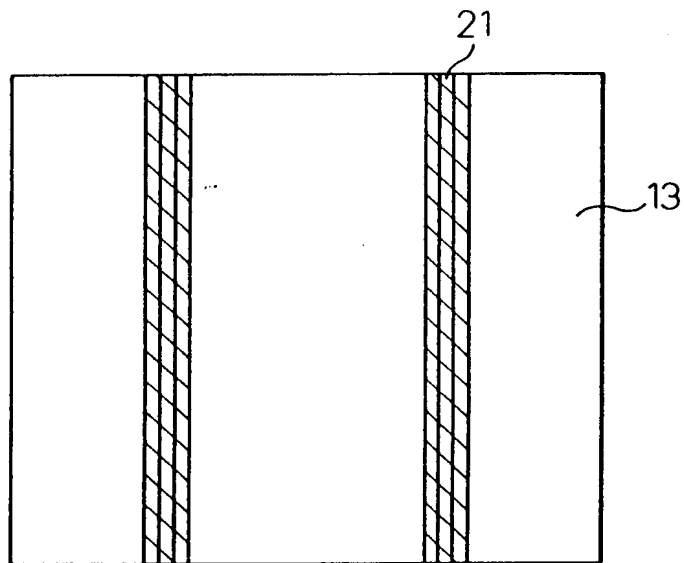
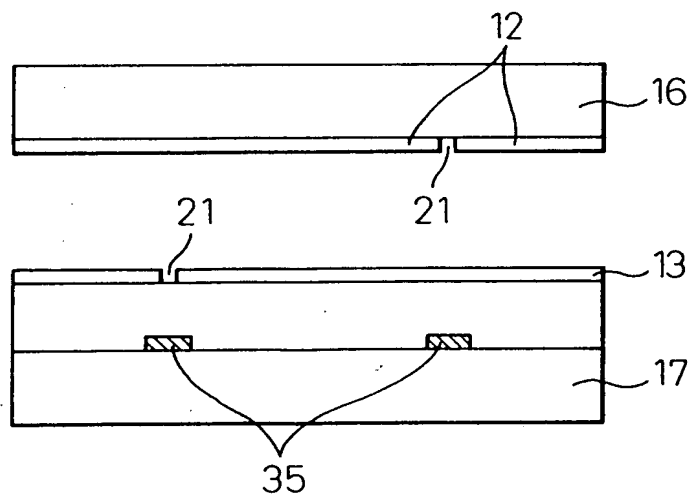


Fig.79B



79/246

Fig. 80A

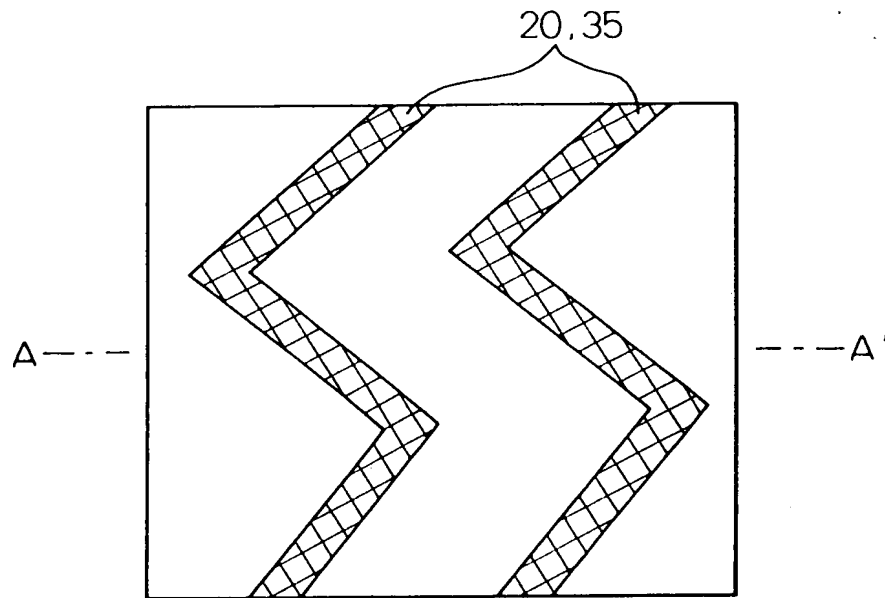
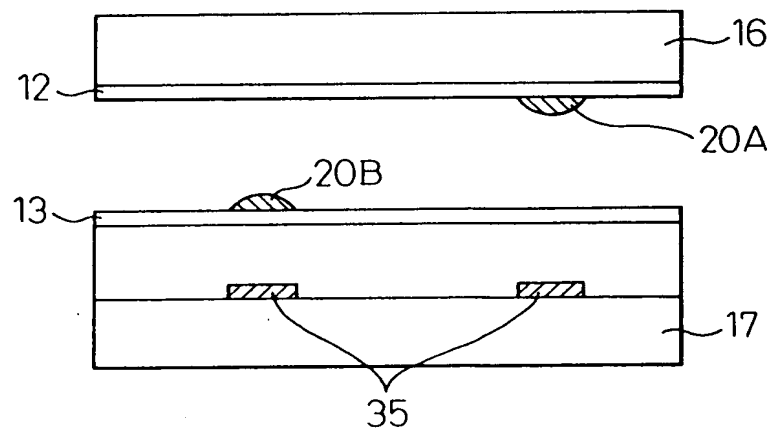


Fig. 80B



80/246

Fig.81A

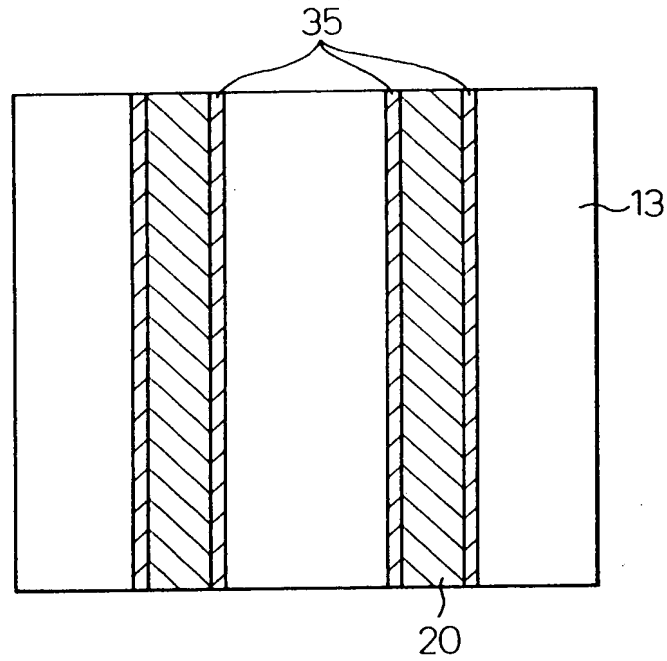


Fig.81B

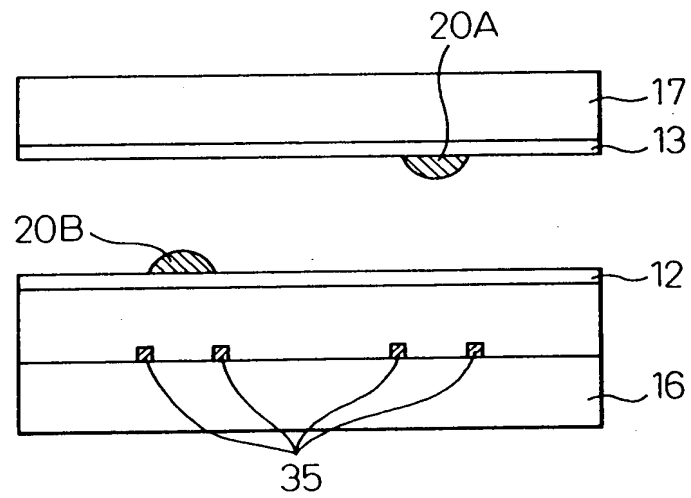
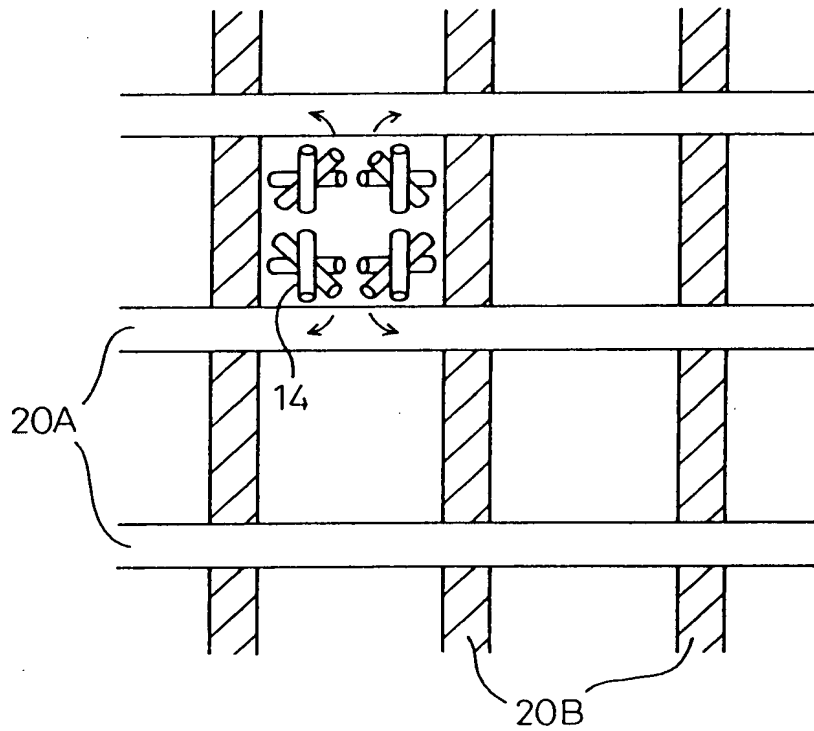


Fig. 82



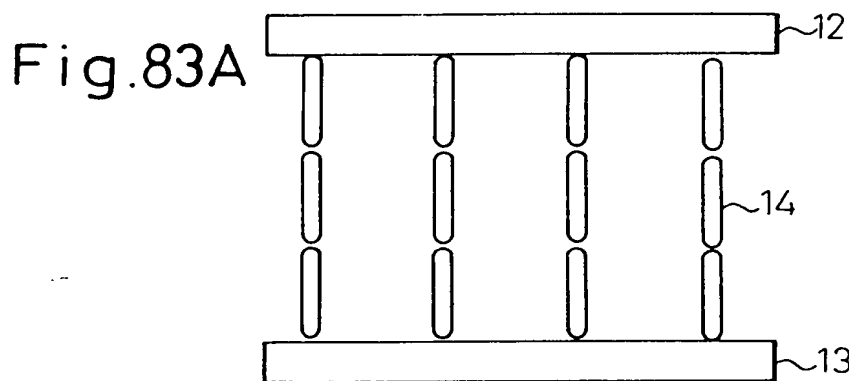


Fig.83B

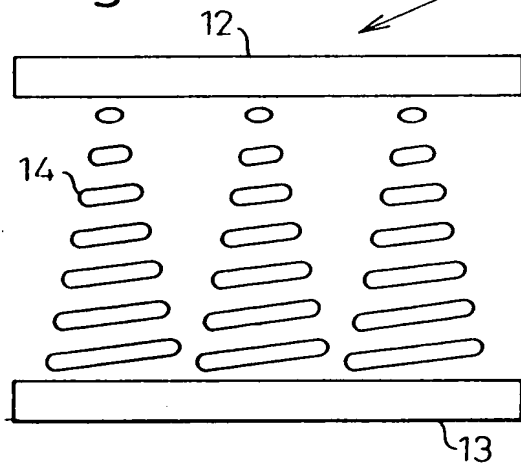


Fig.83C

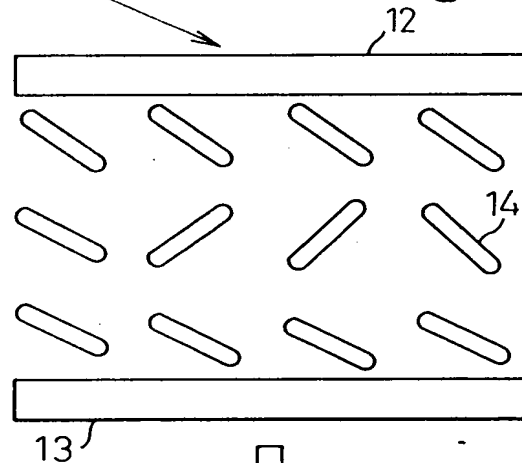
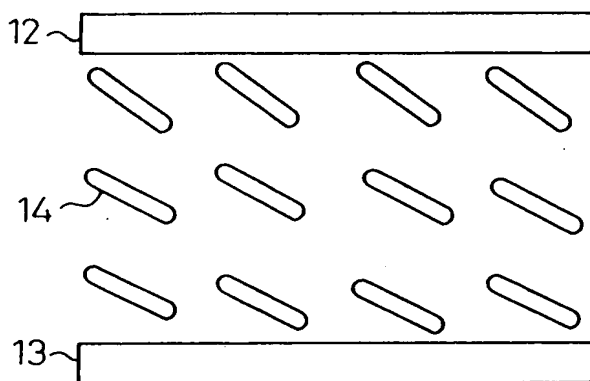
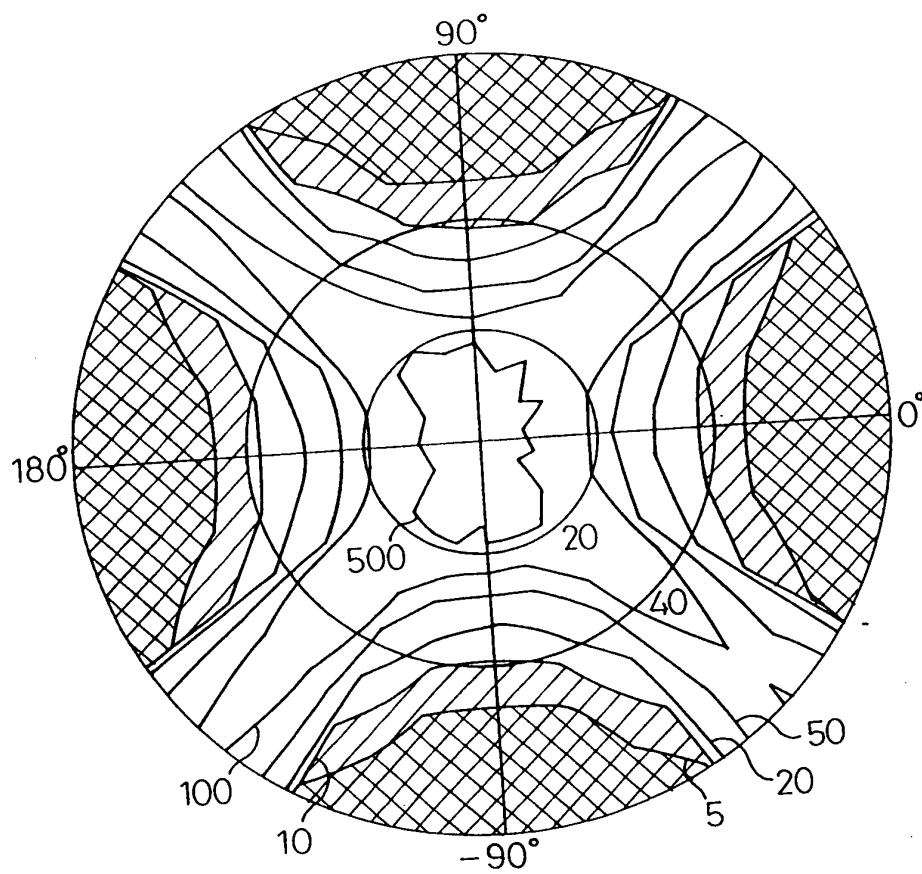


Fig.83D



83/246

Fig. 84



84/246

Fig. 85A

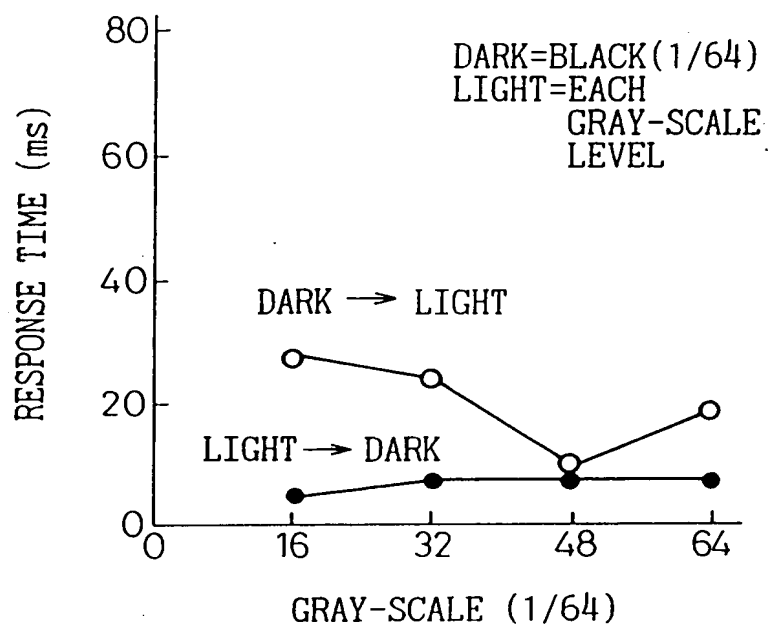
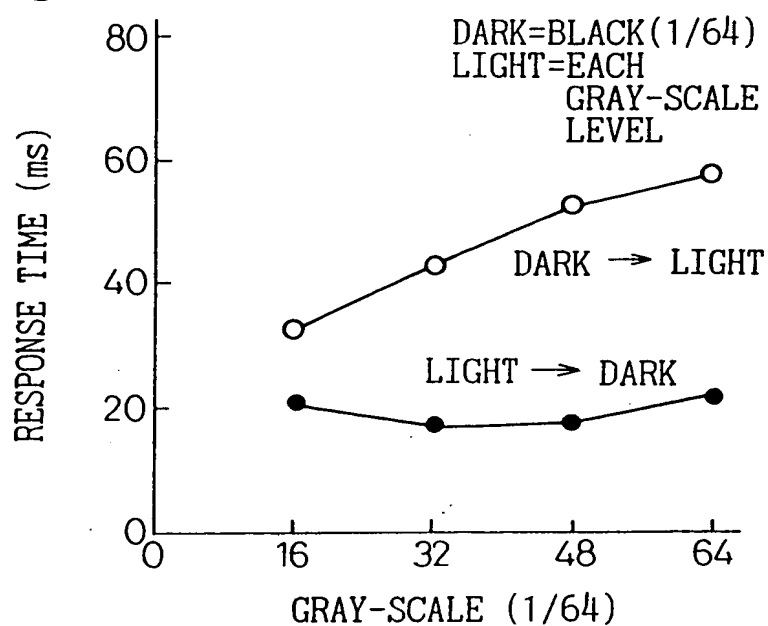


Fig. 85B



85/246

Fig.85C

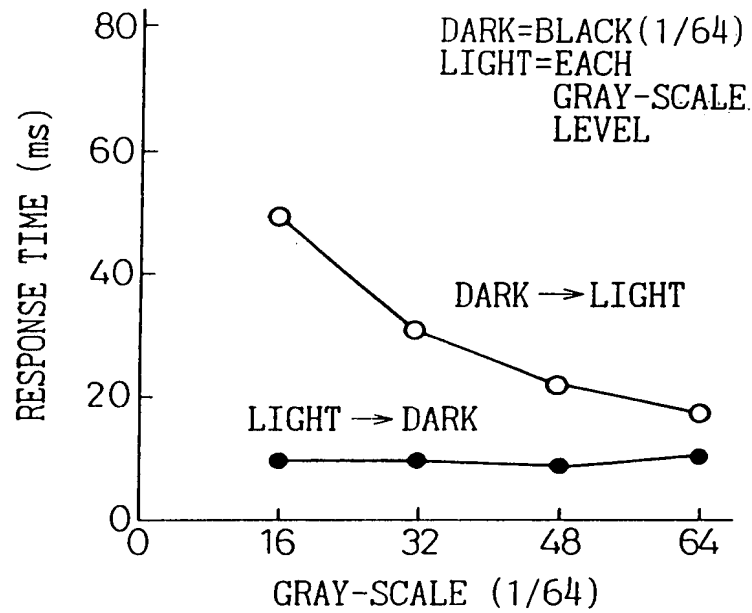


Fig.85D

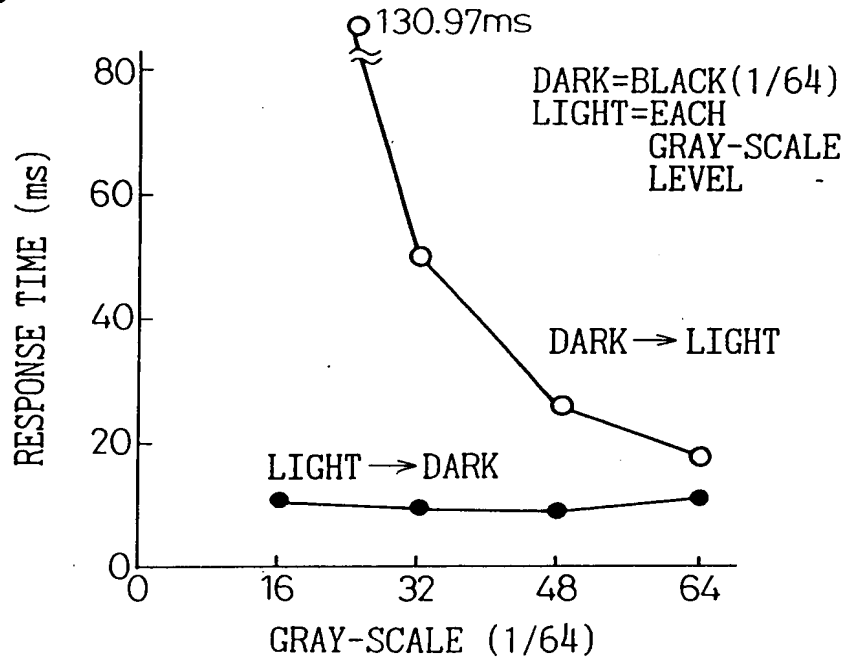


Fig.86A

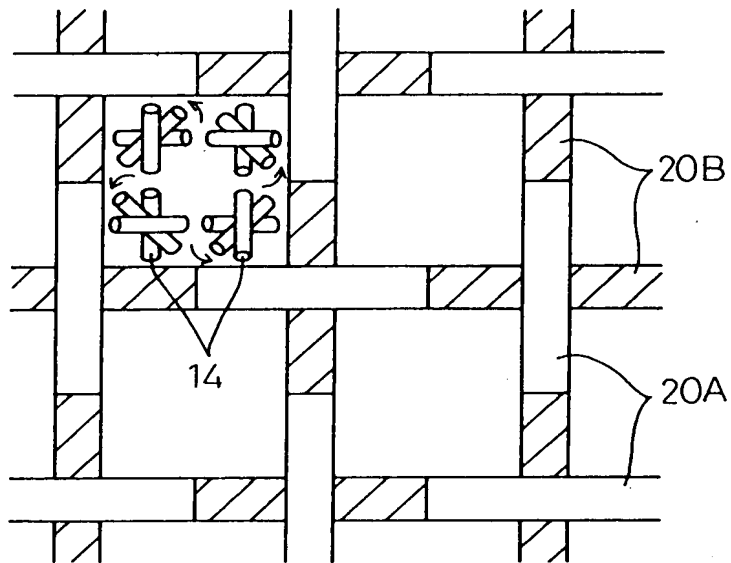
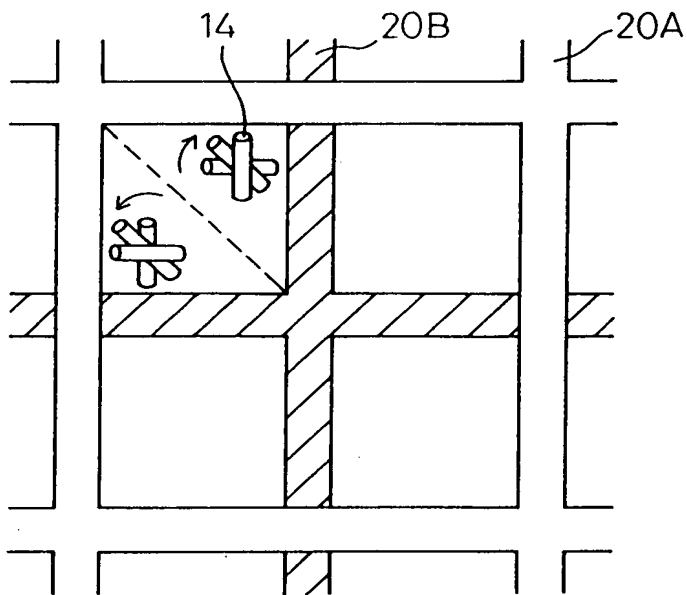


Fig.86B



87/246

Fig. 87

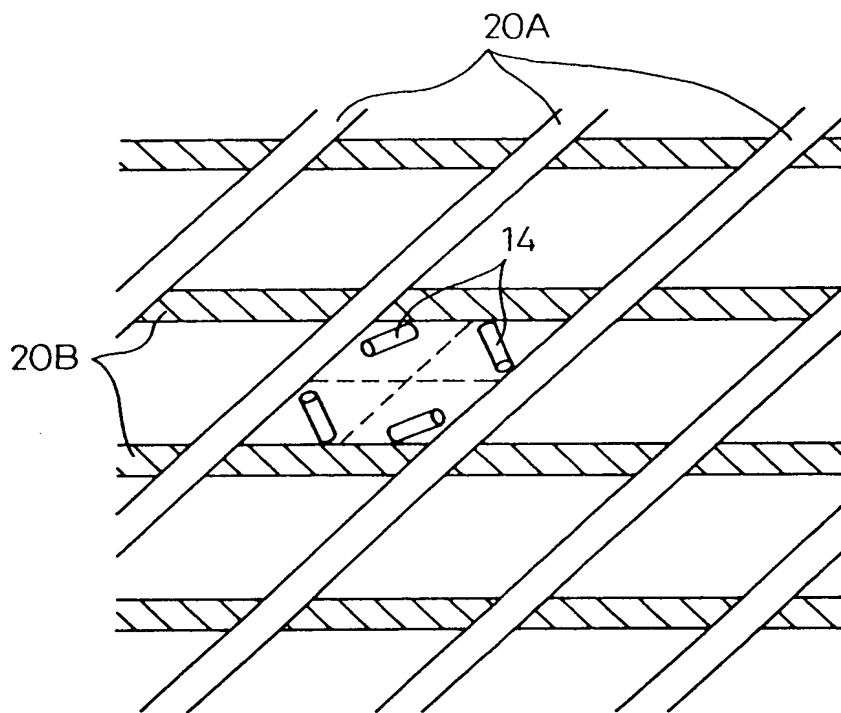


Fig. 88

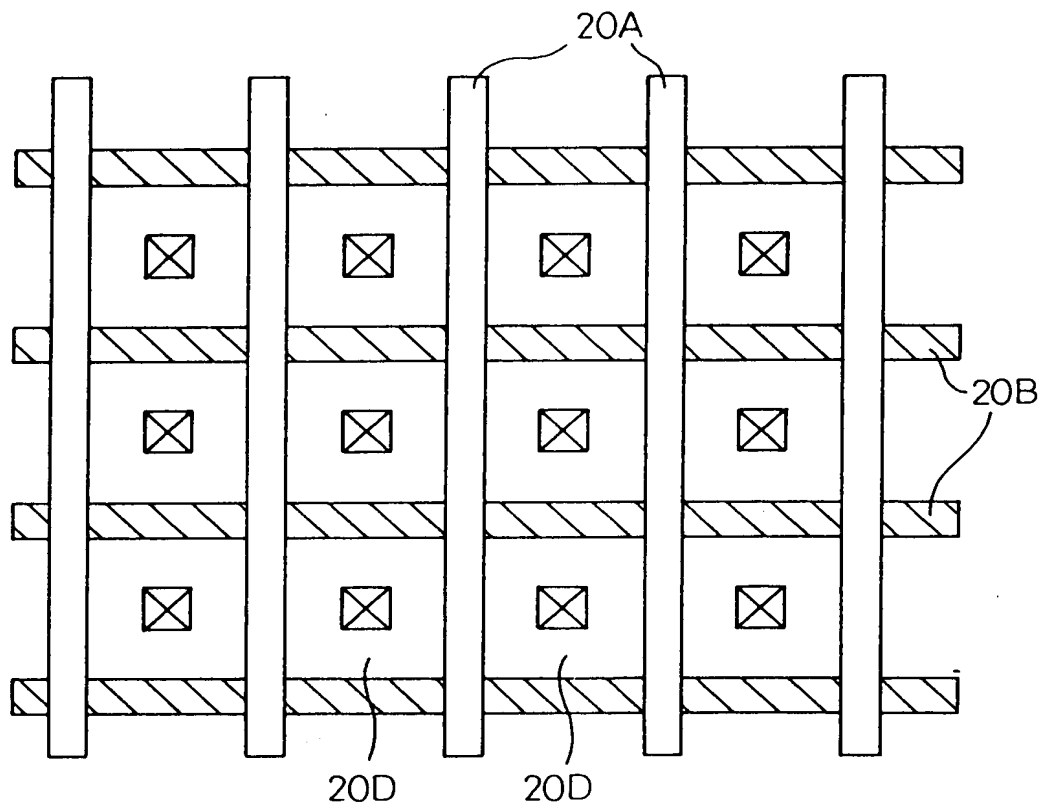
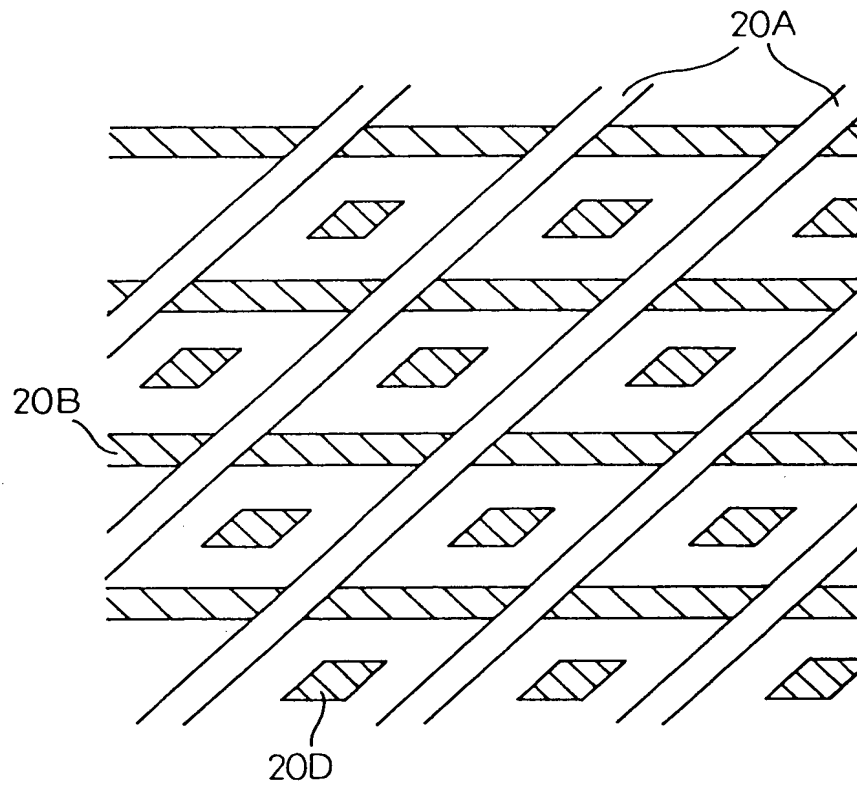


Fig. 89



90/246

Fig. 90A

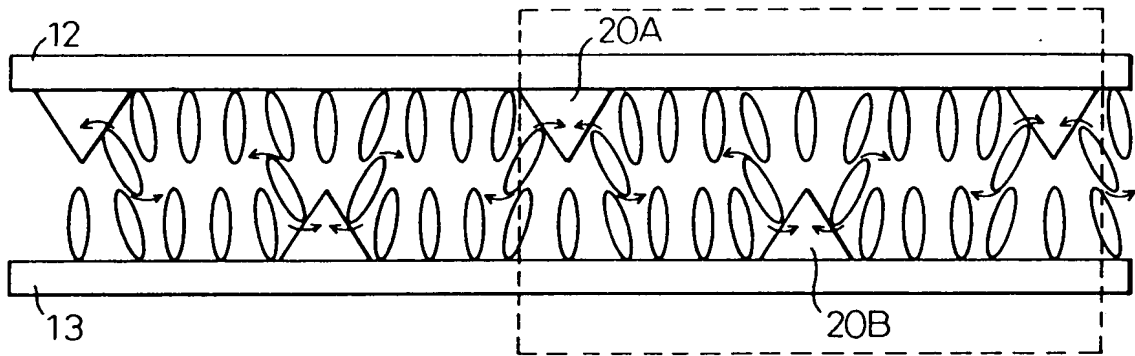


Fig. 90B

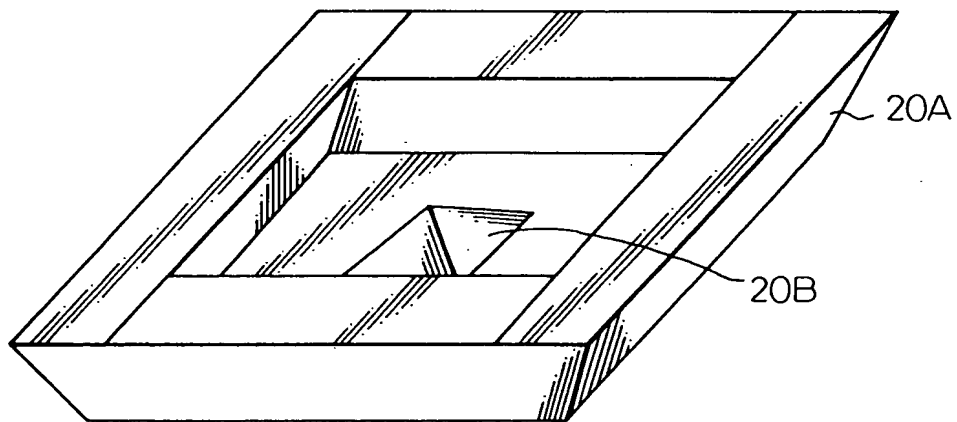
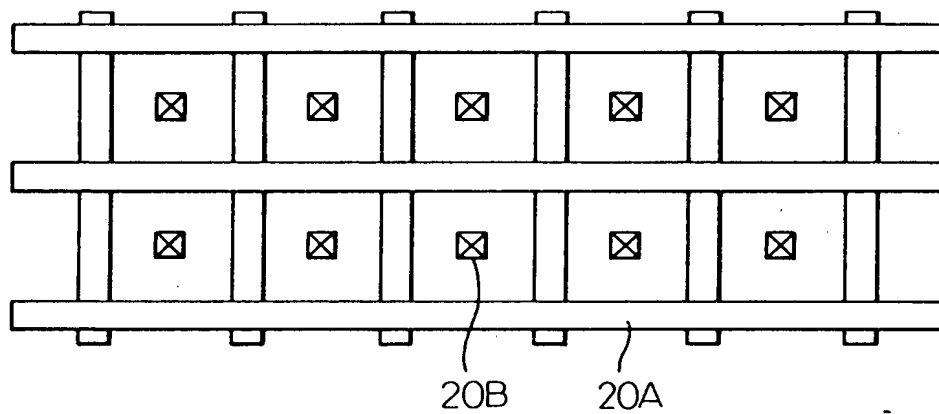


Fig. 91



92/246

Fig.92A

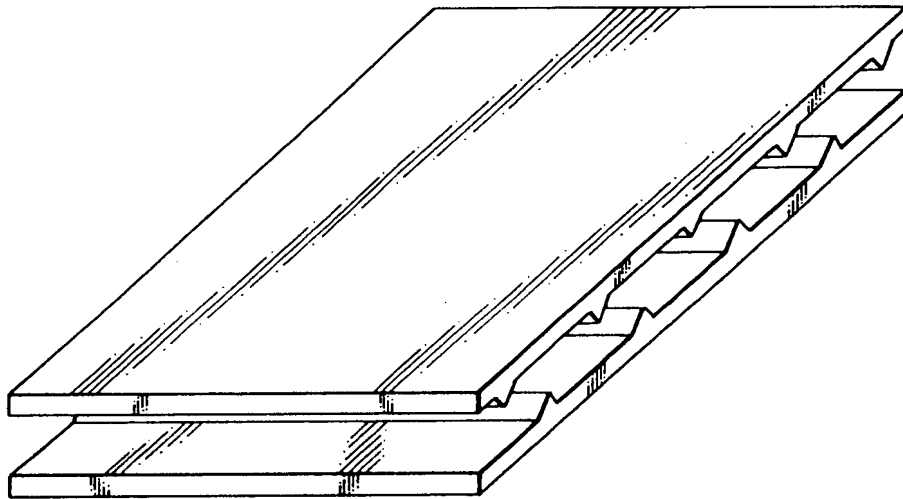


Fig.92B

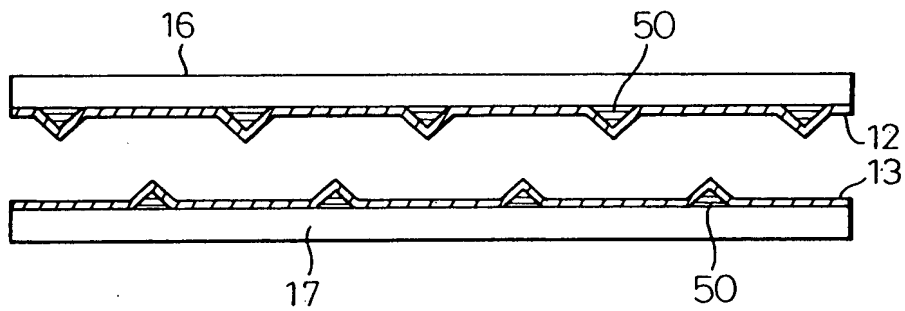


Fig. 93

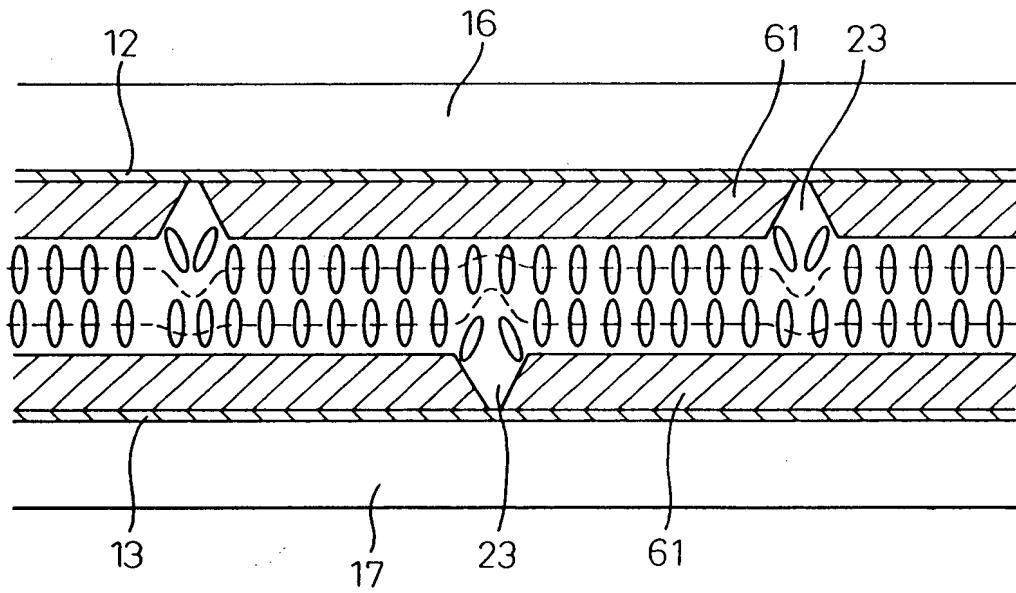


Fig.94

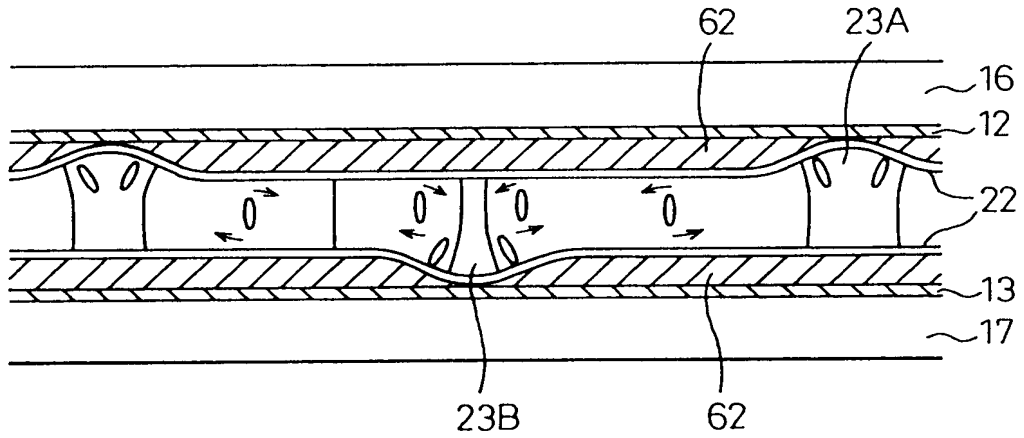
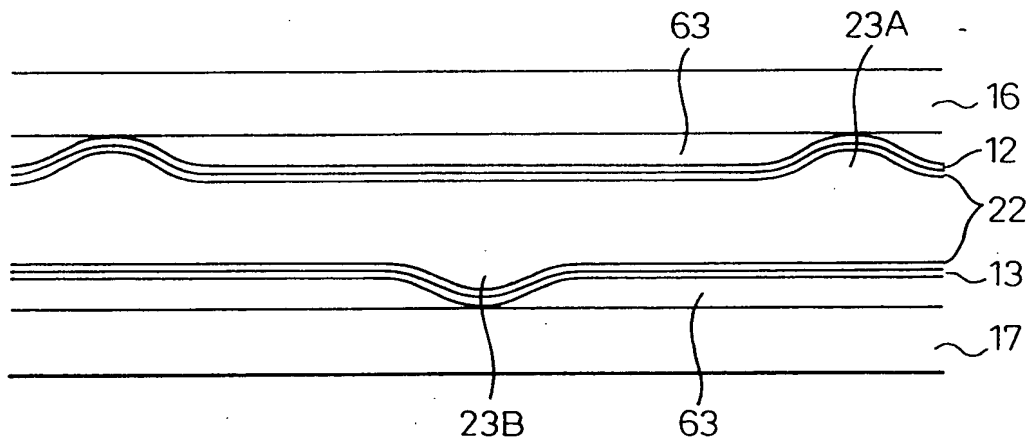


Fig.95



95/246

Fig.96

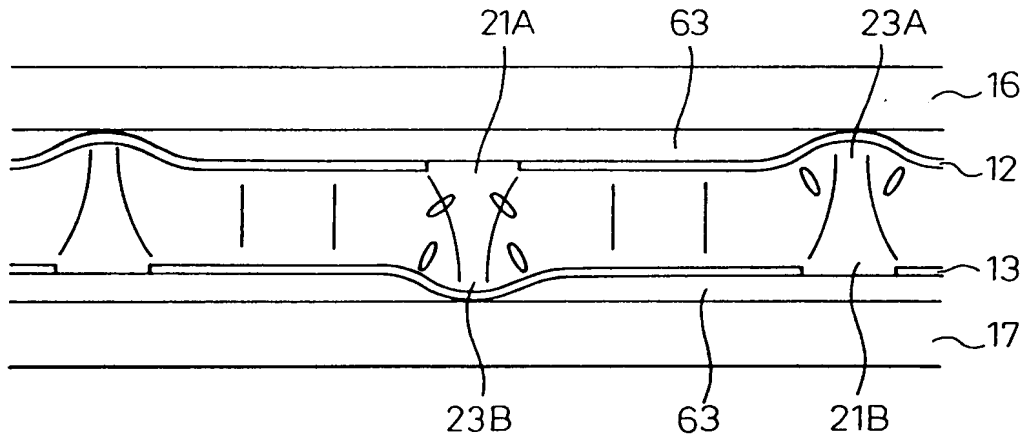


Fig.97

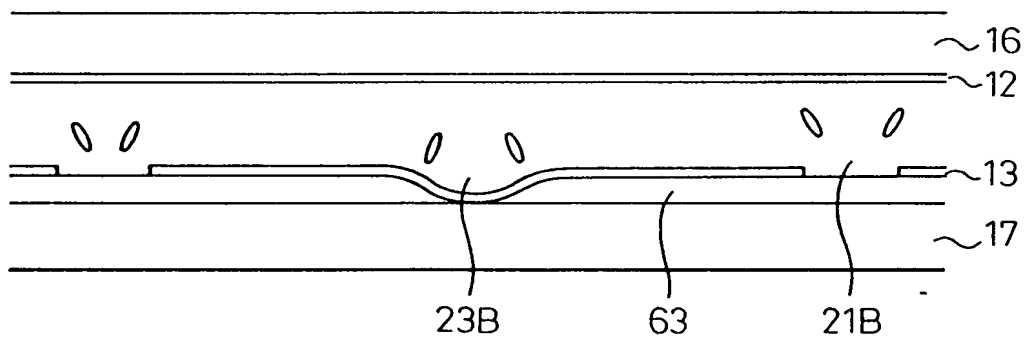
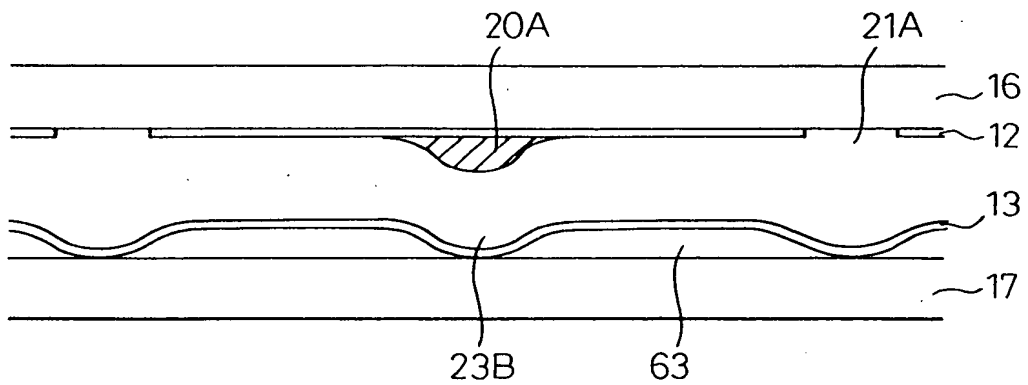


Fig.98



96/246

Fig.99A

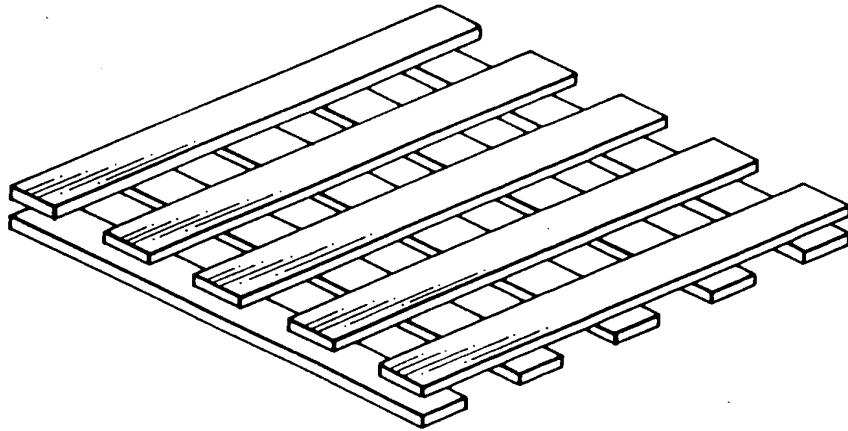


Fig.99B

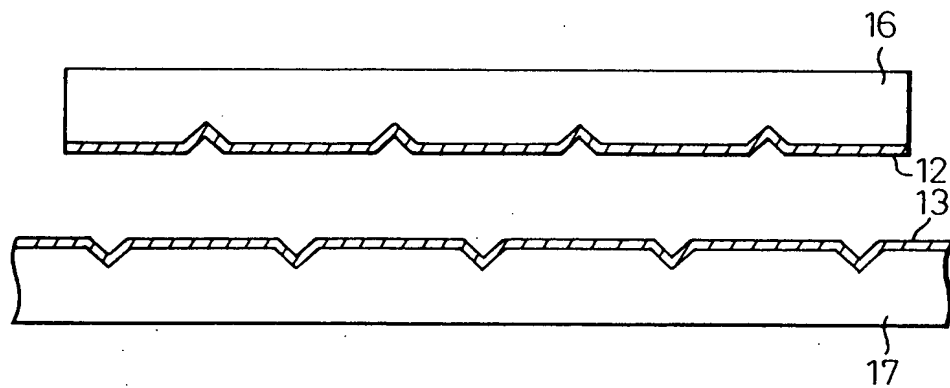


Fig.100A

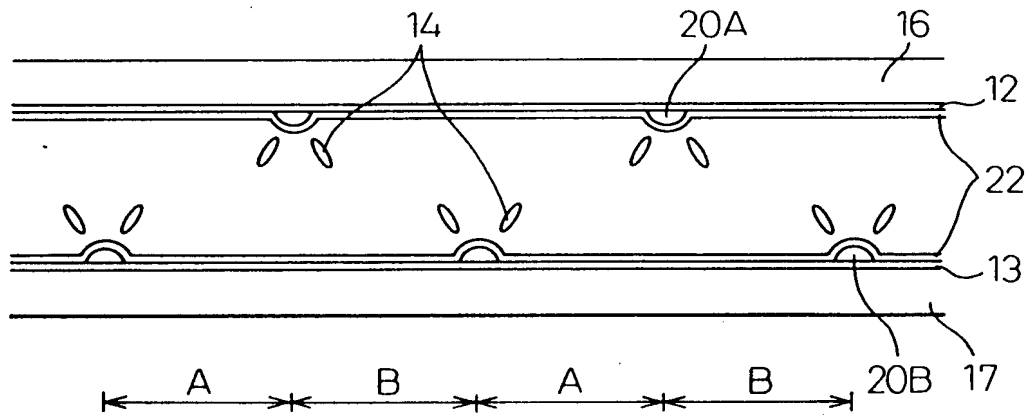


Fig.100B

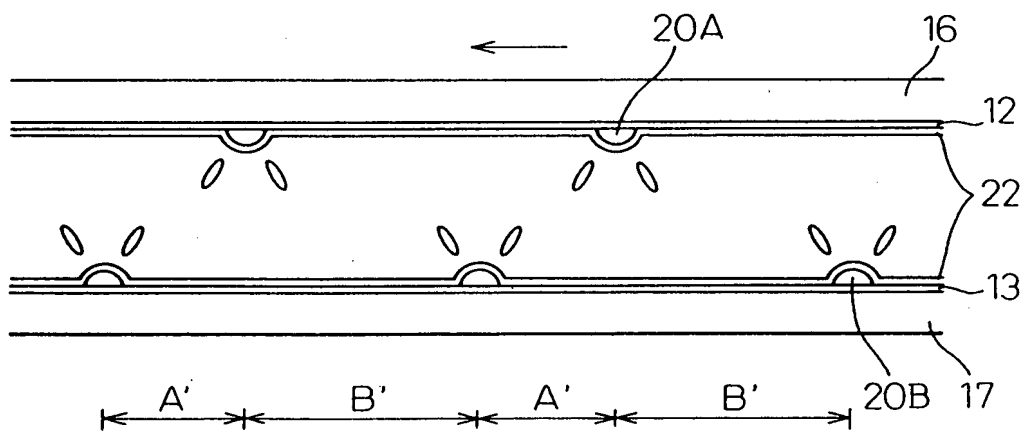


Fig. 101A

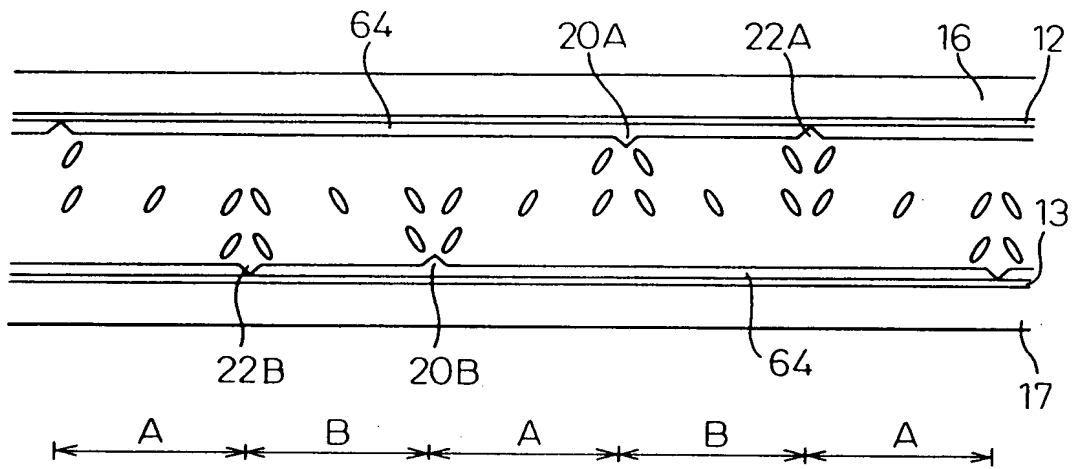


Fig. 101B

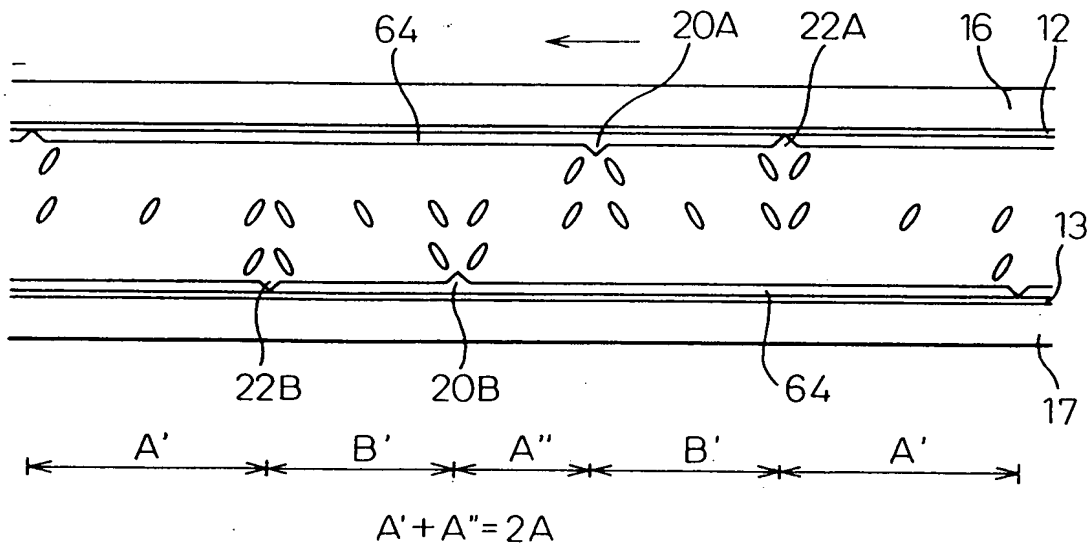
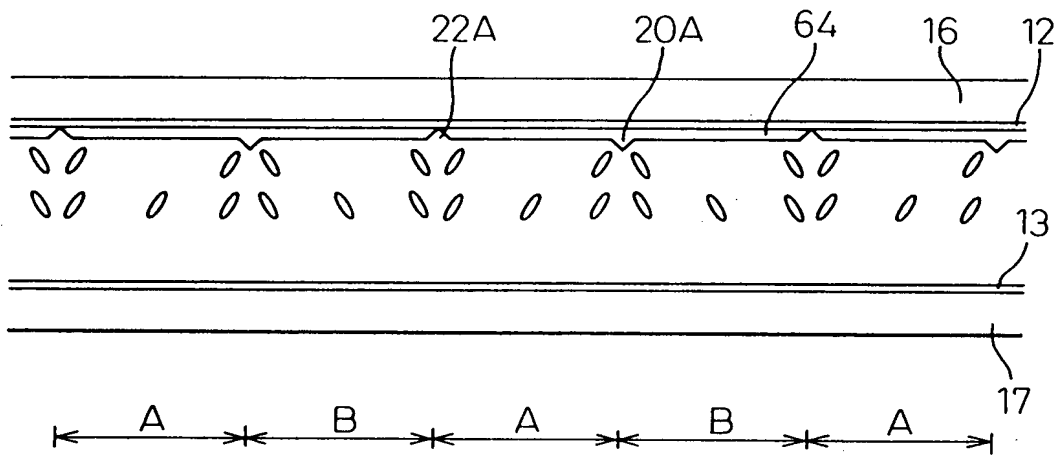


Fig.102



101/246

Fig.104

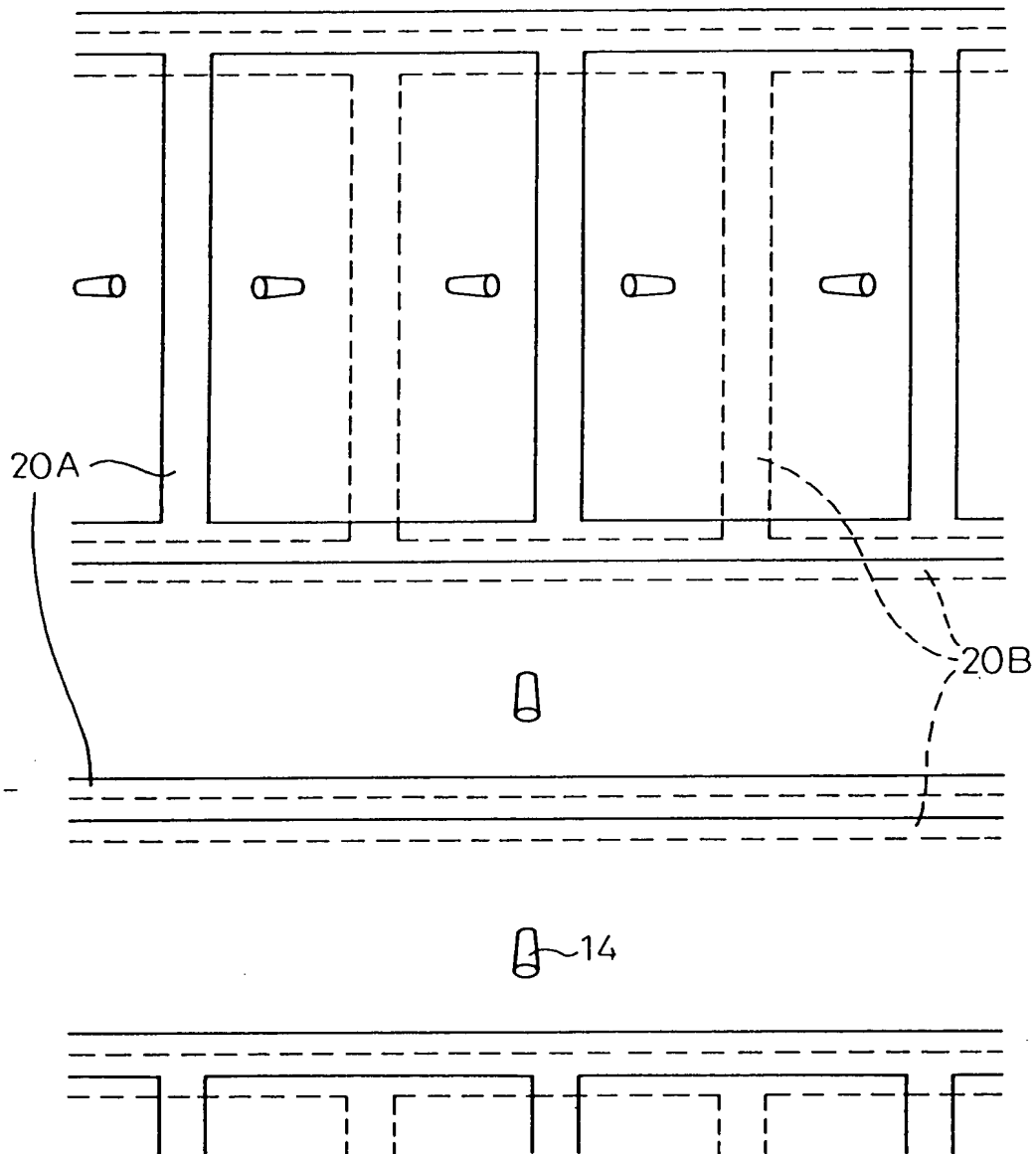


Fig.105A

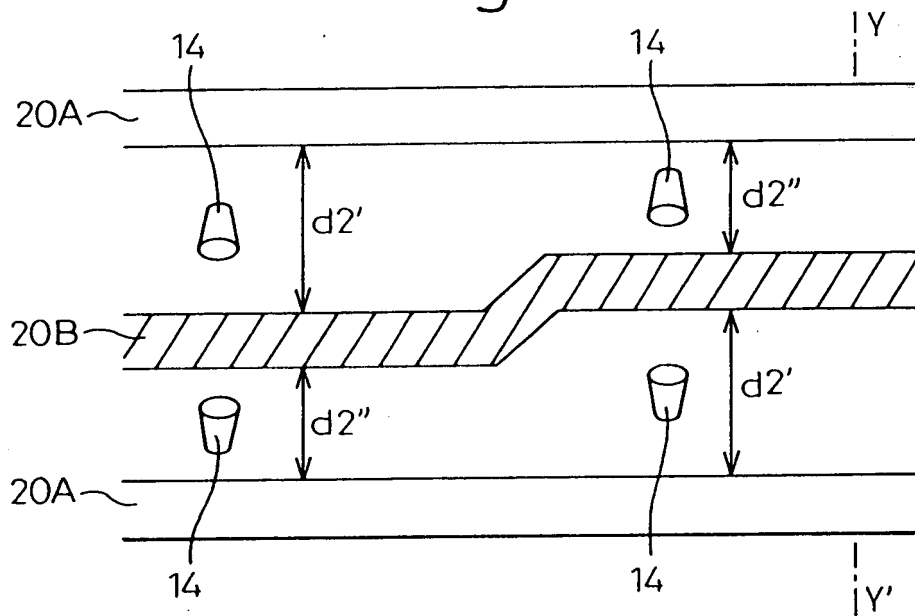


Fig.105B

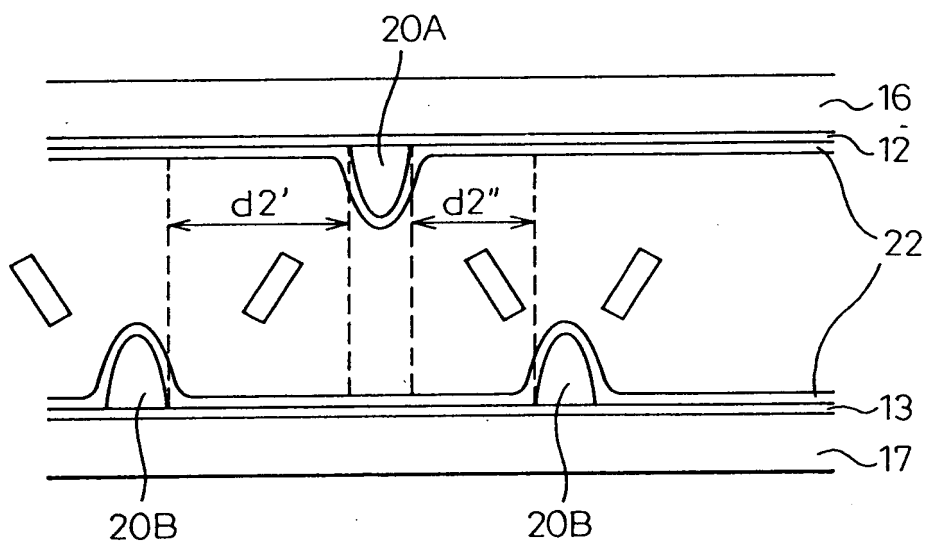


Fig.106

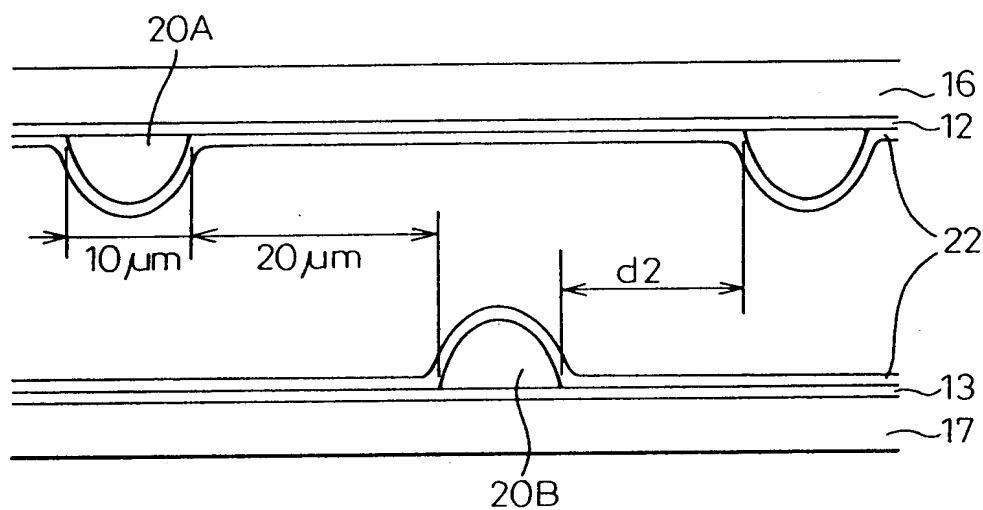
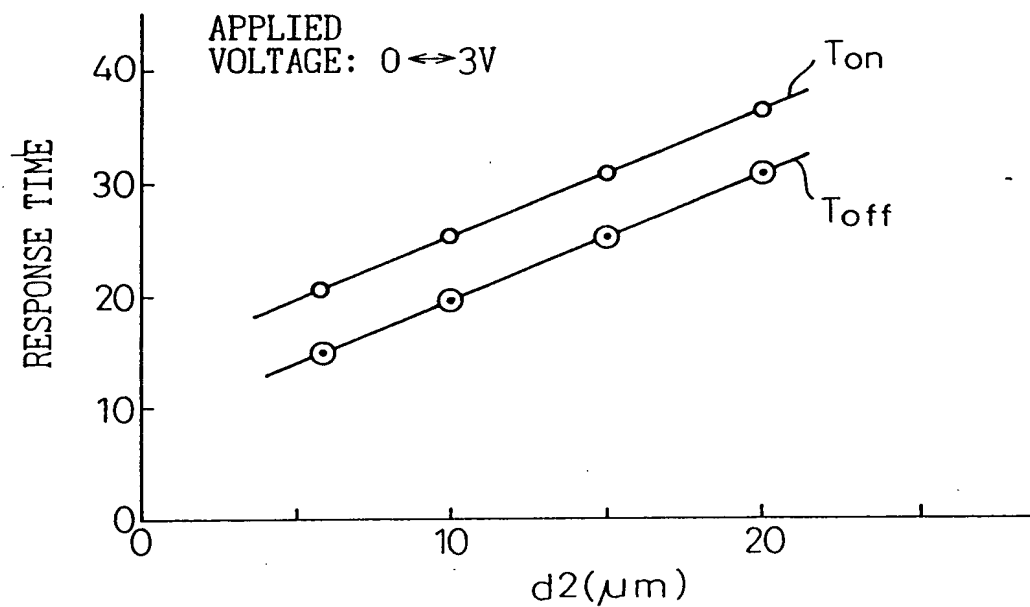


Fig.107



104/246

Fig.108A

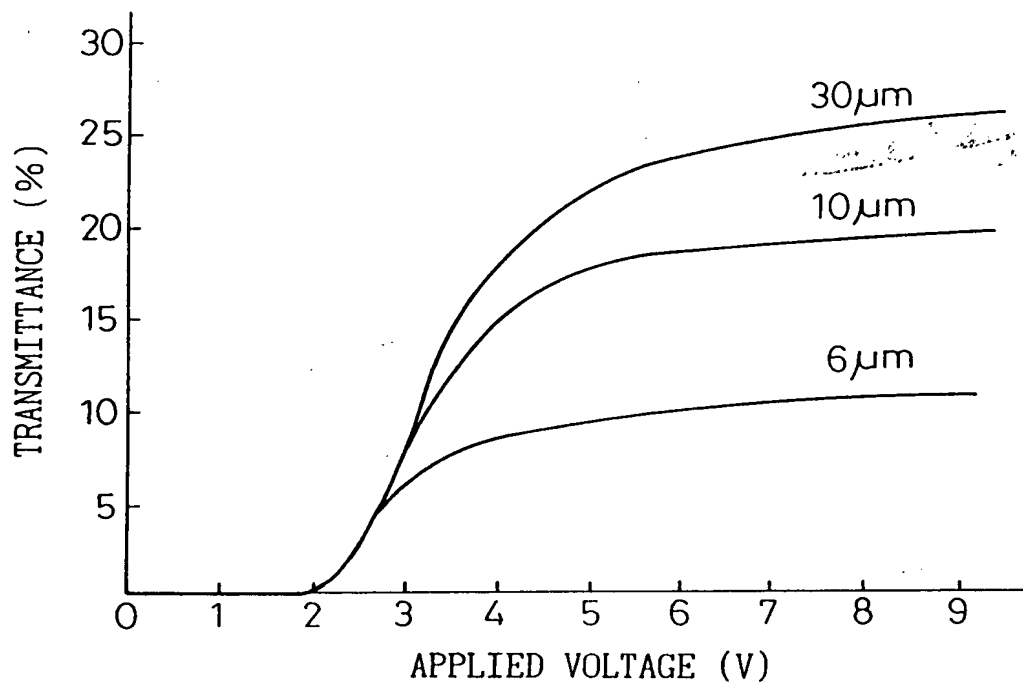
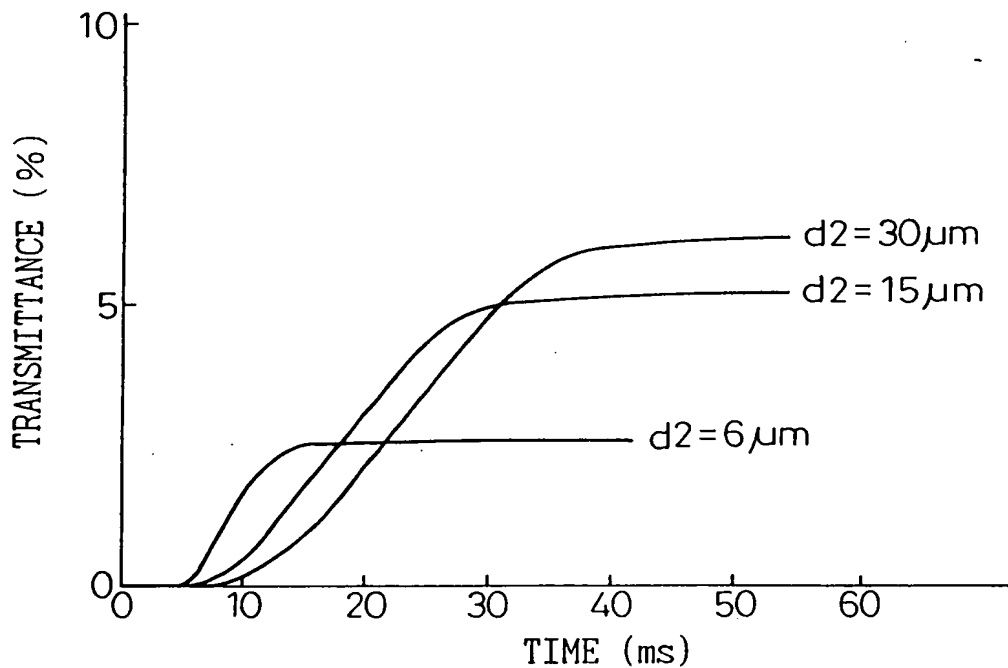


Fig.108B



105/
246

Fig.109A

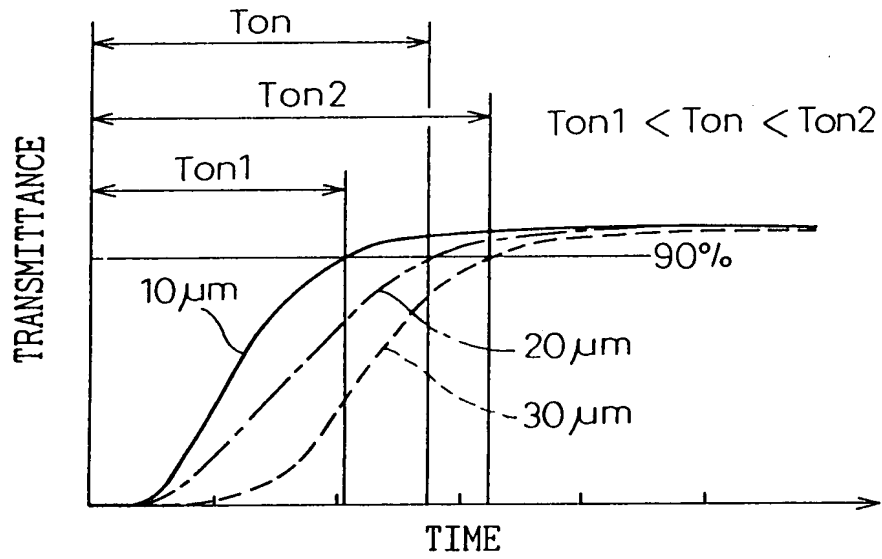


Fig.109B

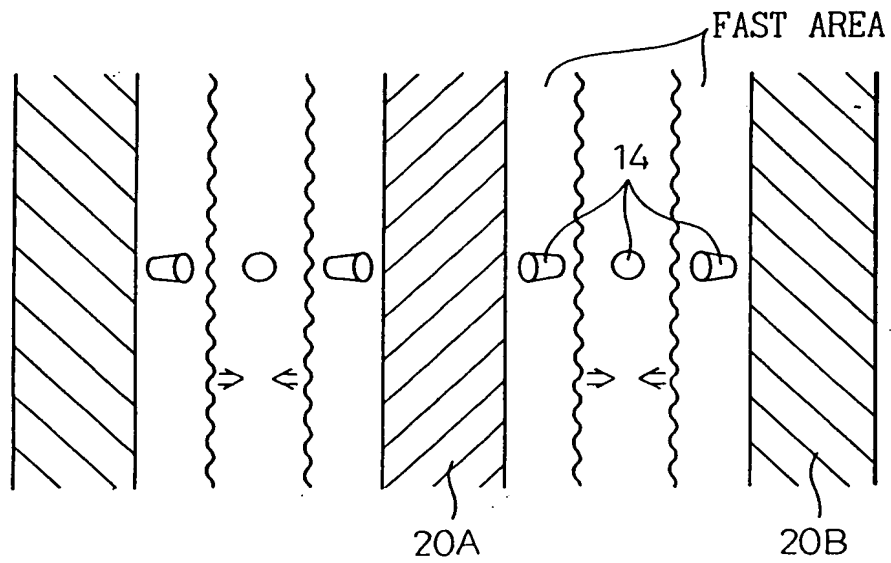
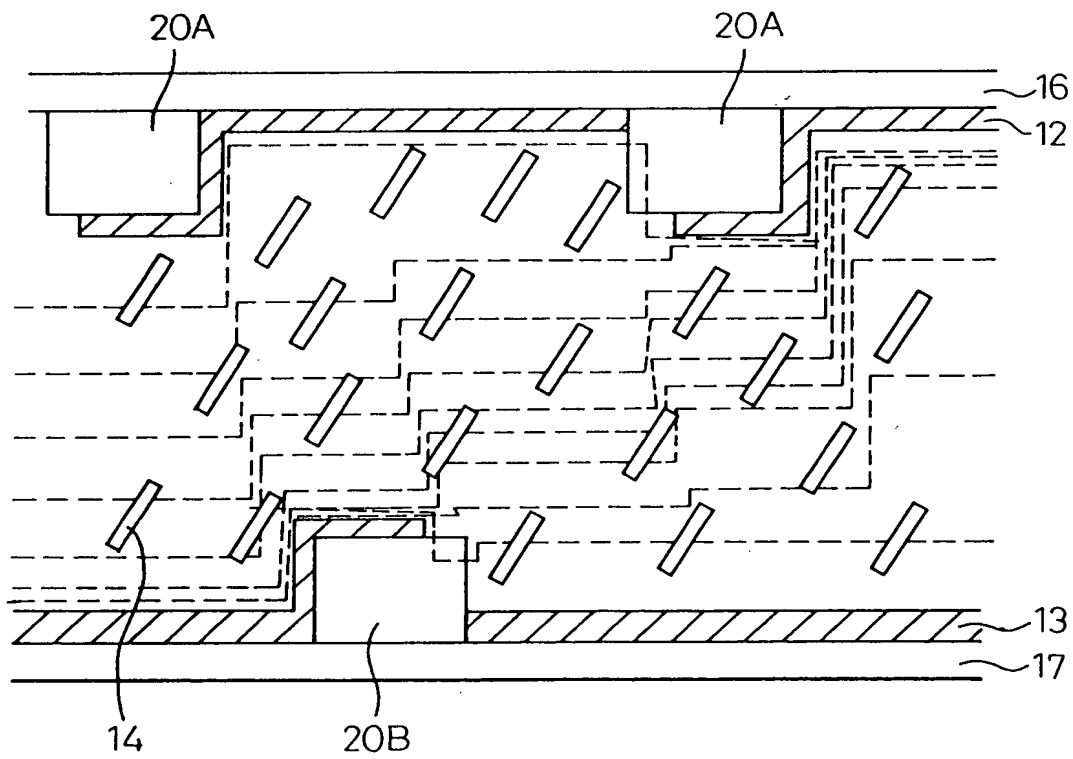


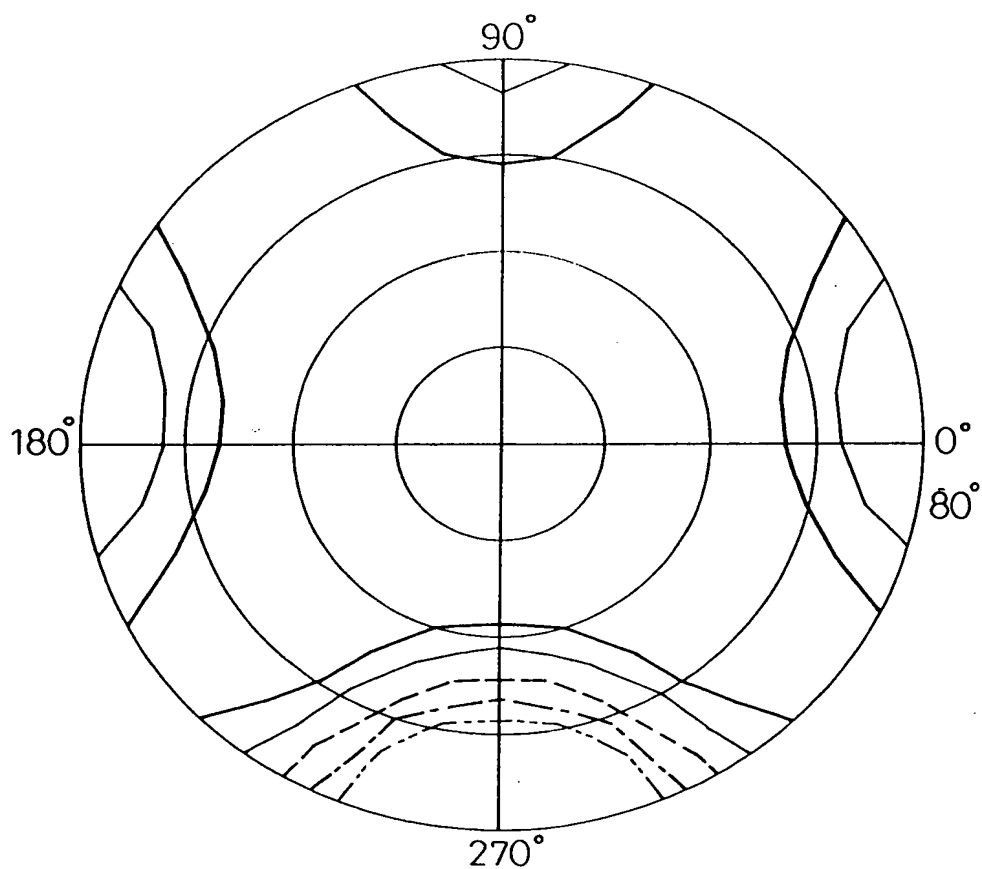
Fig. 110



$$\frac{107}{246}$$

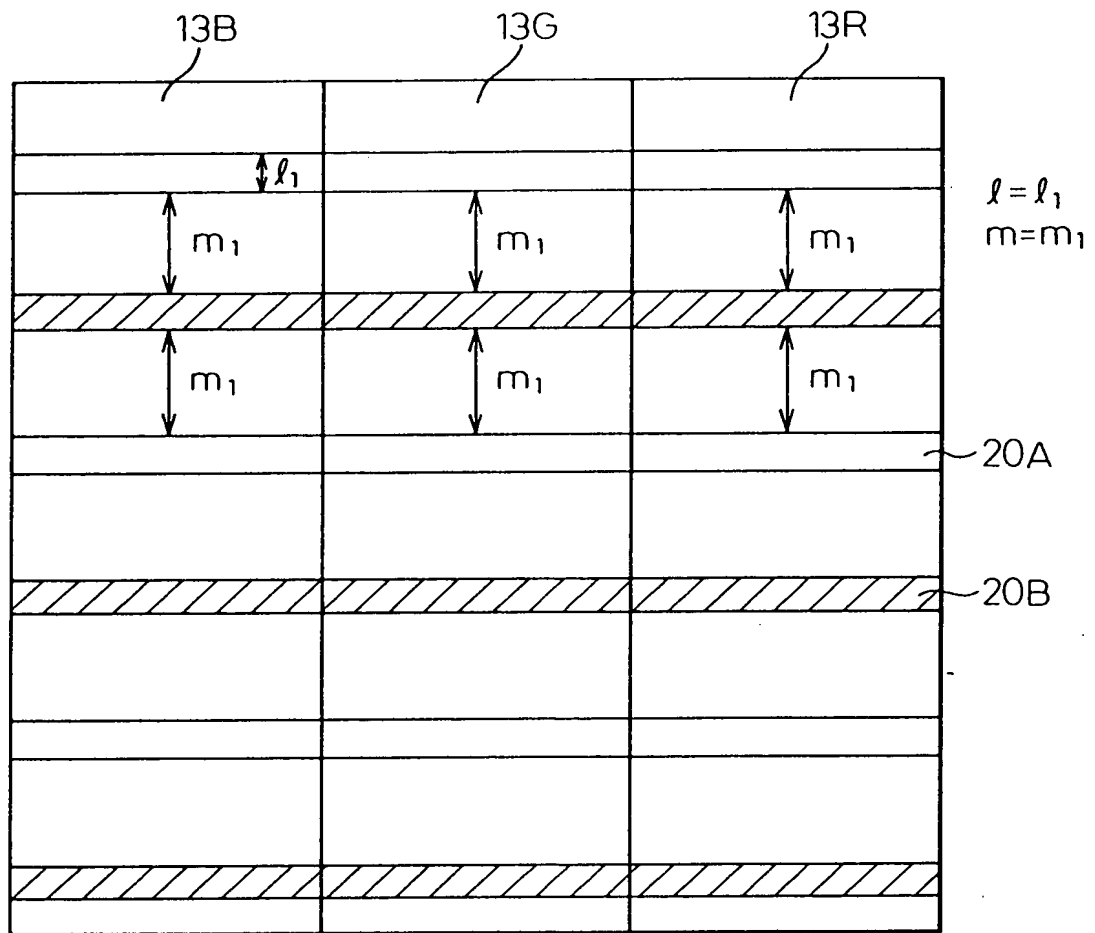
Fig. 111

CONTRAST RATIO	
_____	100.000
_____	50.000
-----	20.000
-----	10.000
-----	5.000



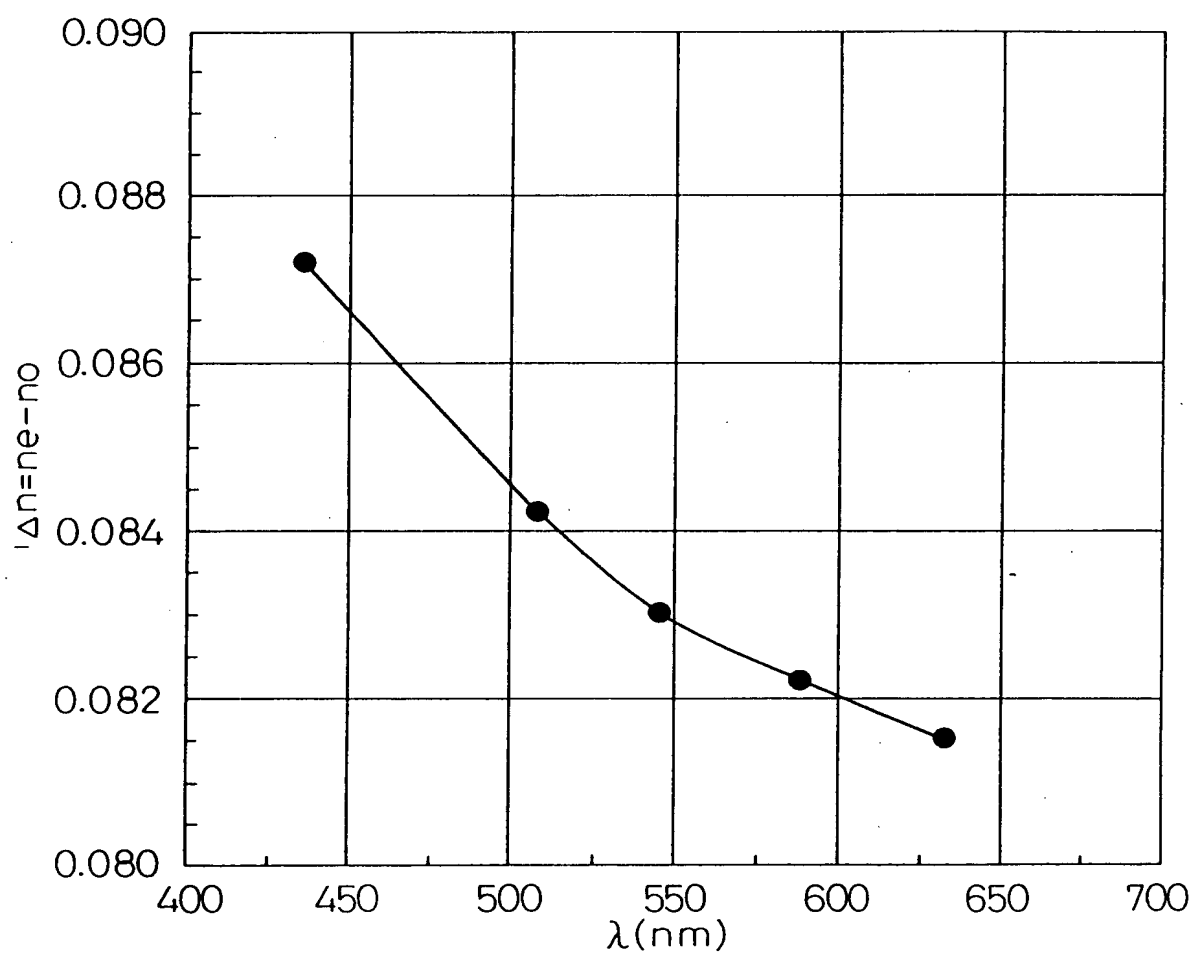
18

Fig.112



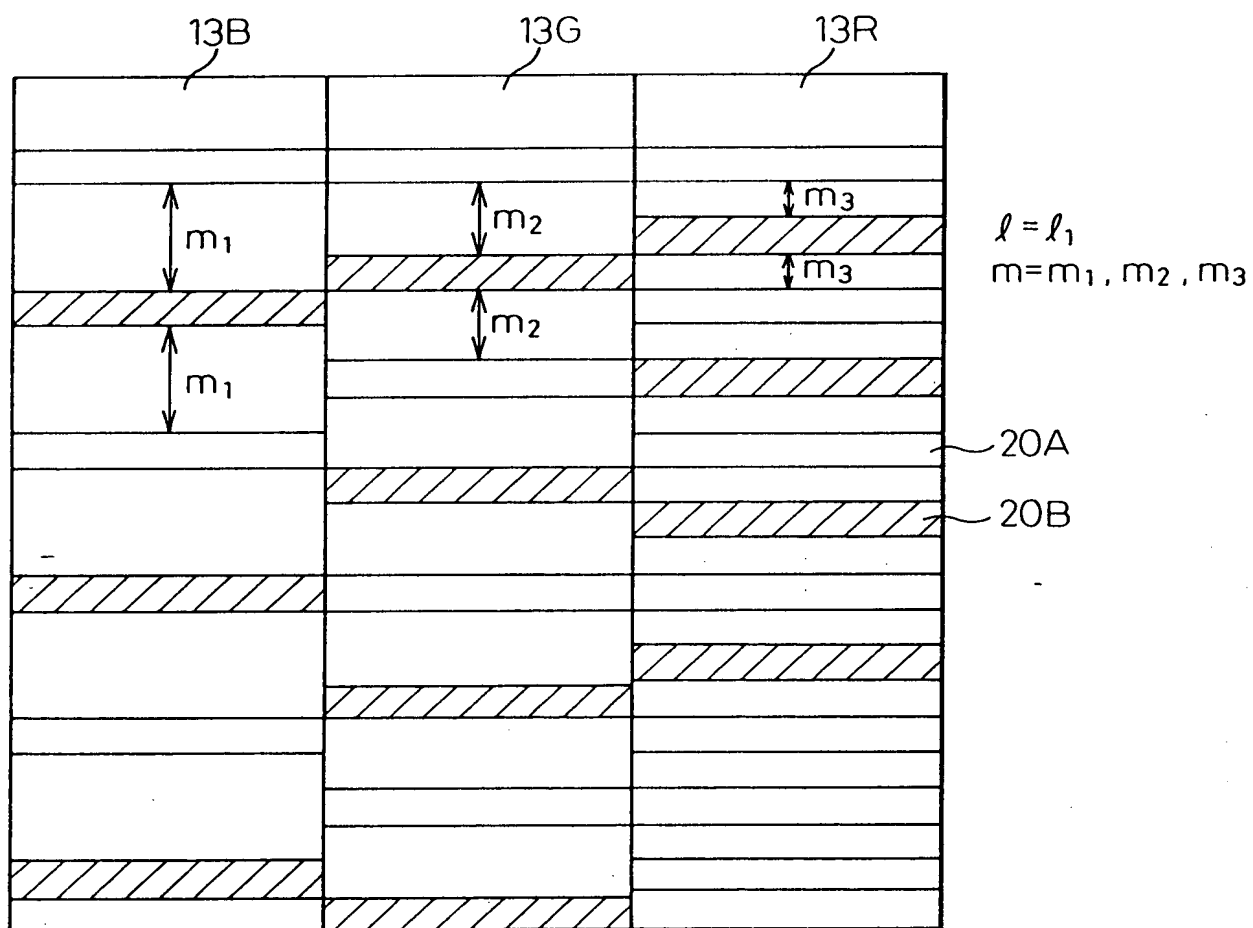
109/246

Fig.113



110/
246

Fig.114



111/246

Fig. 115

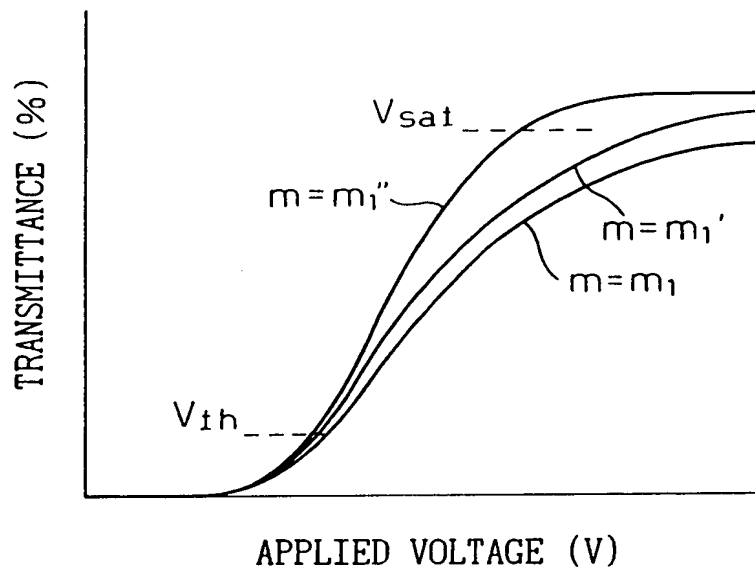


Fig.116

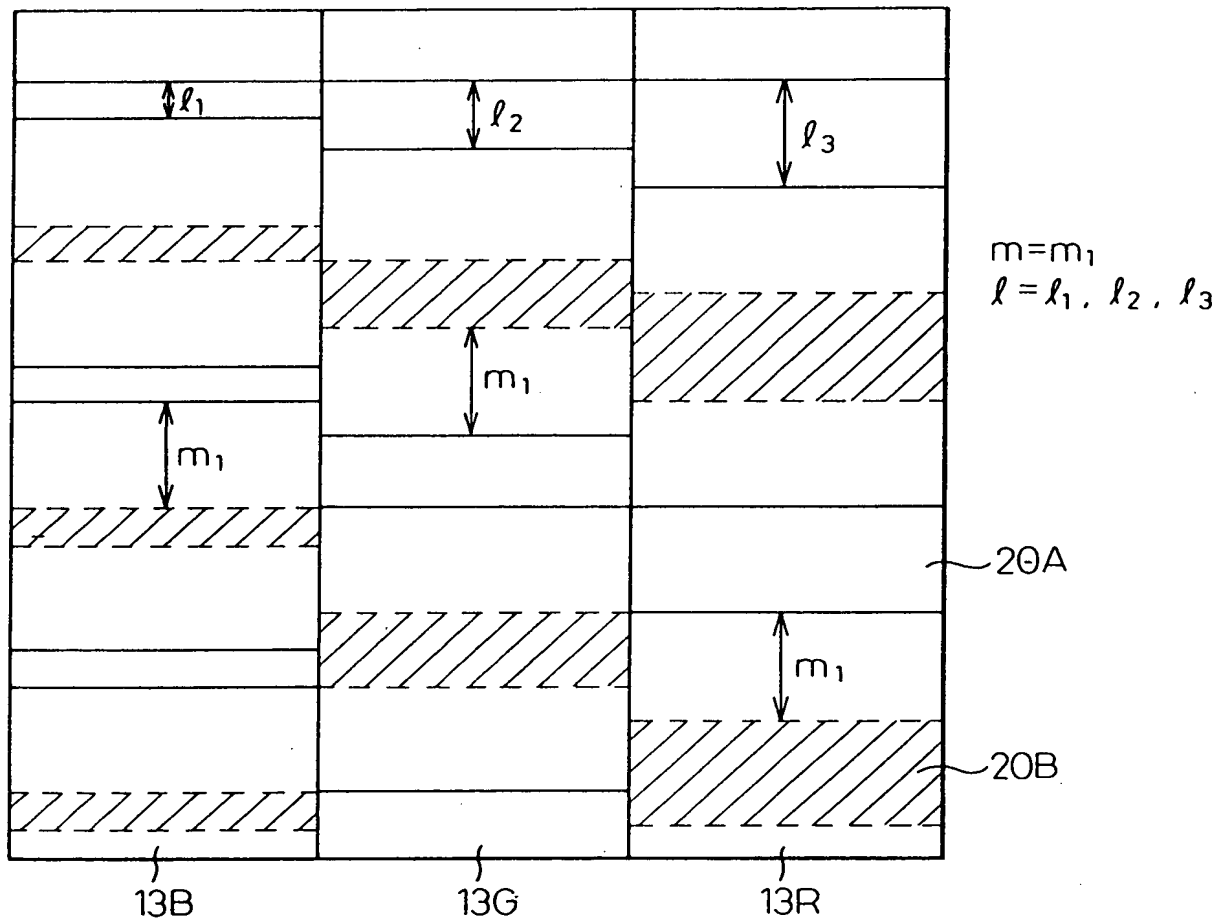


Fig.117

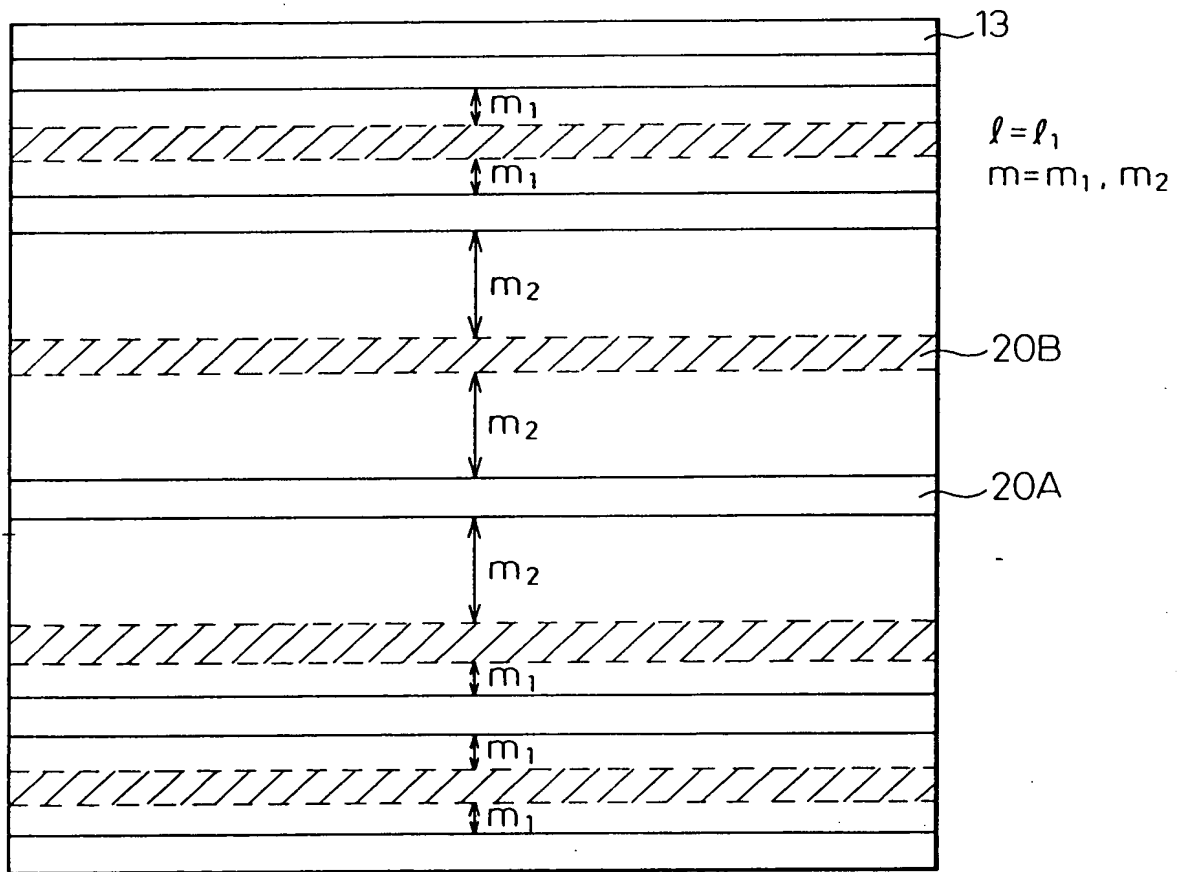


Fig.118

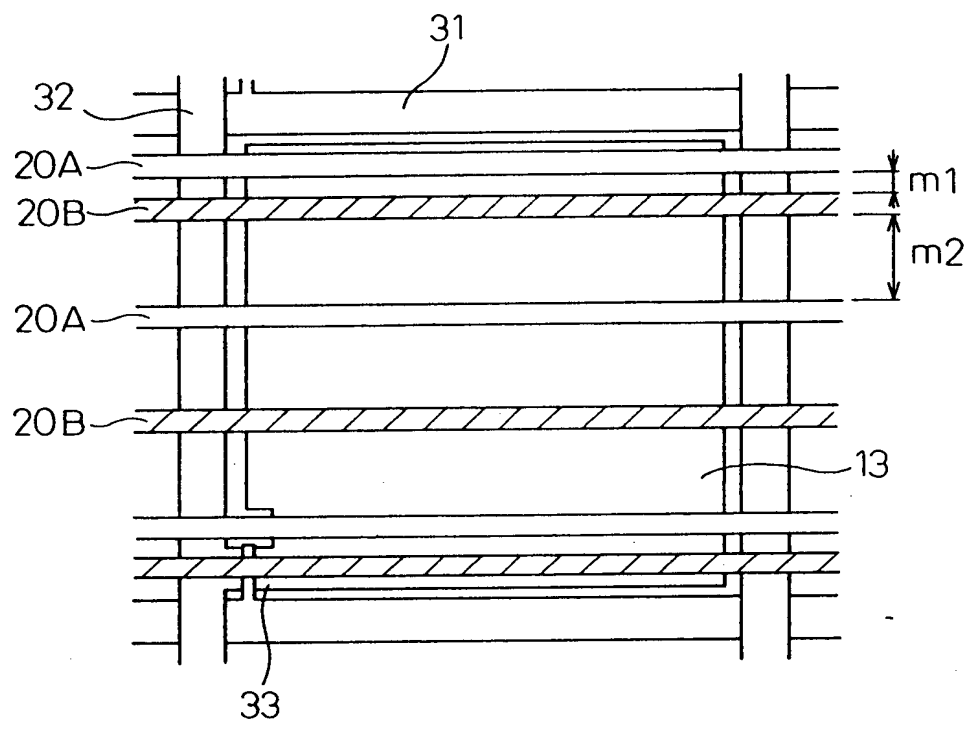
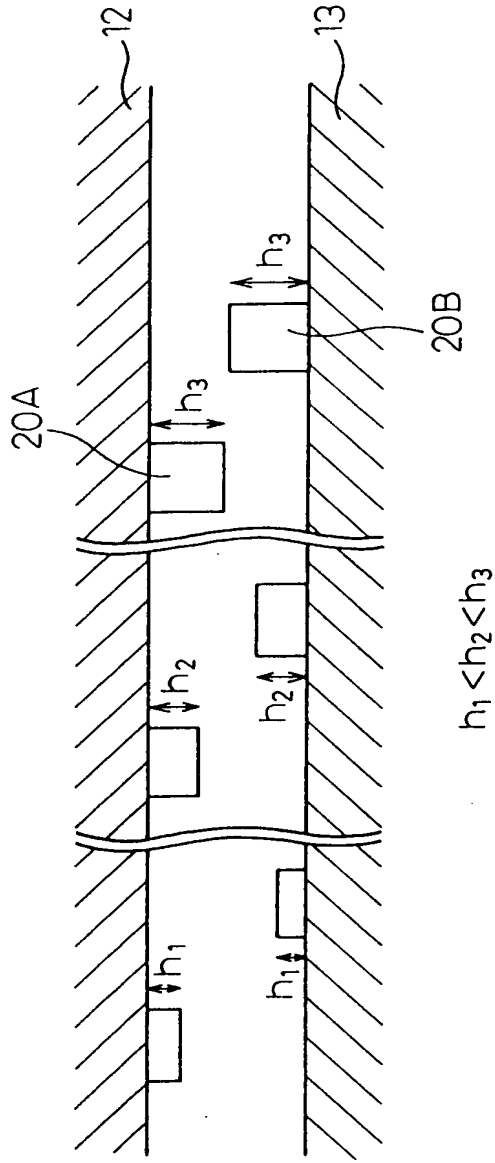


Fig. 119



115/246

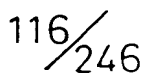
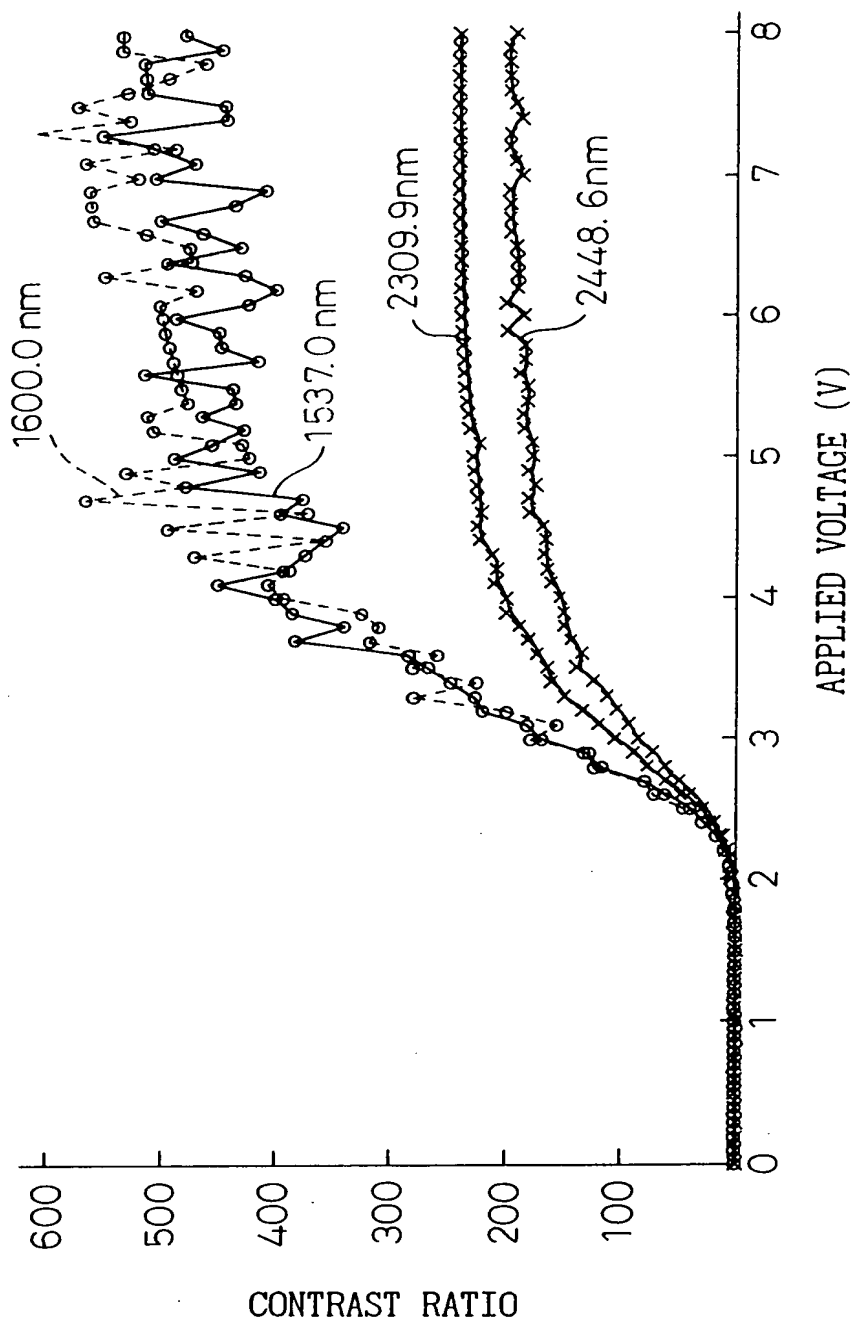
[illegible]

Fig. 121



33.

$$\frac{118}{246}$$

Fig. 122

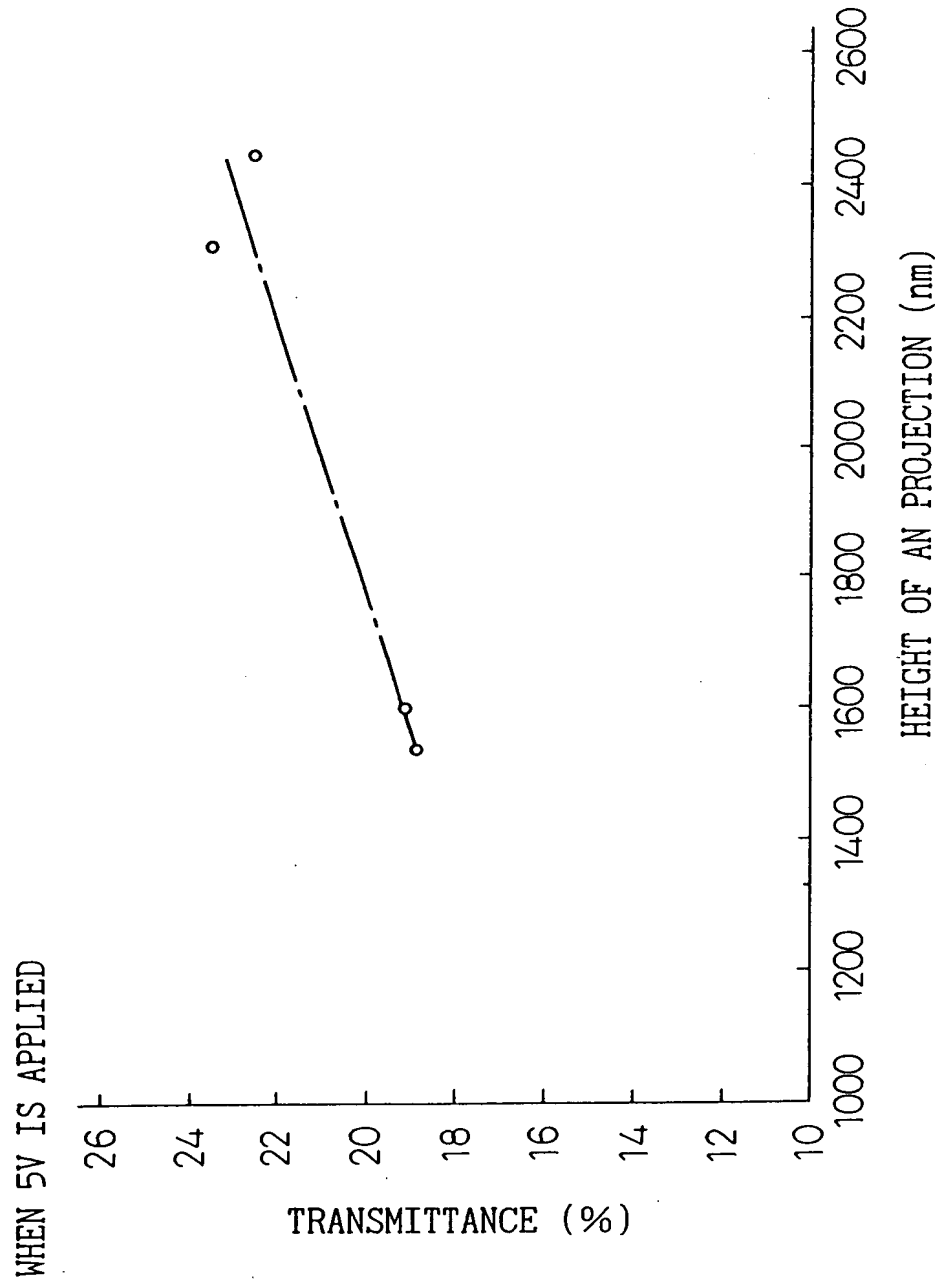


Fig. 123

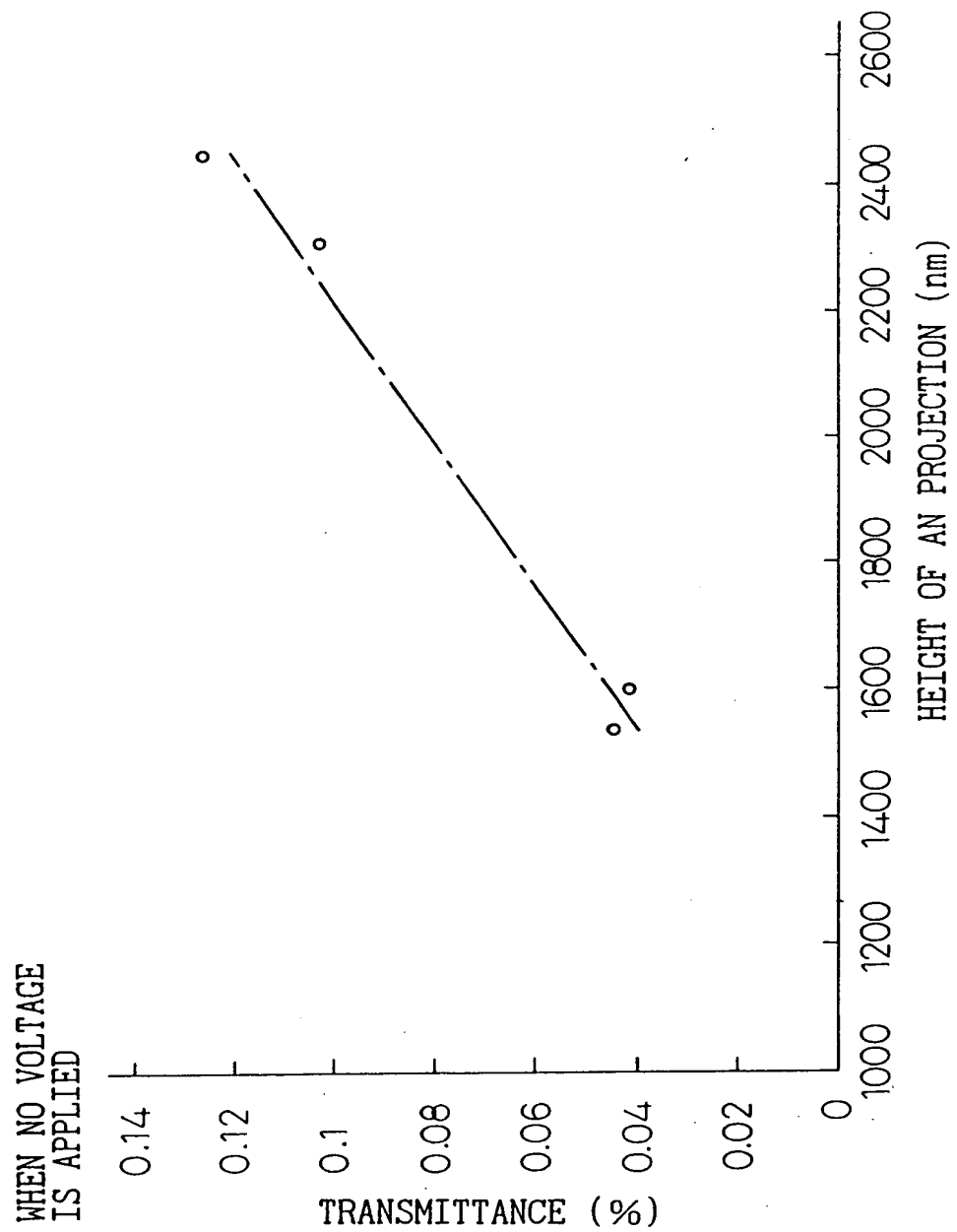


Fig. 124A

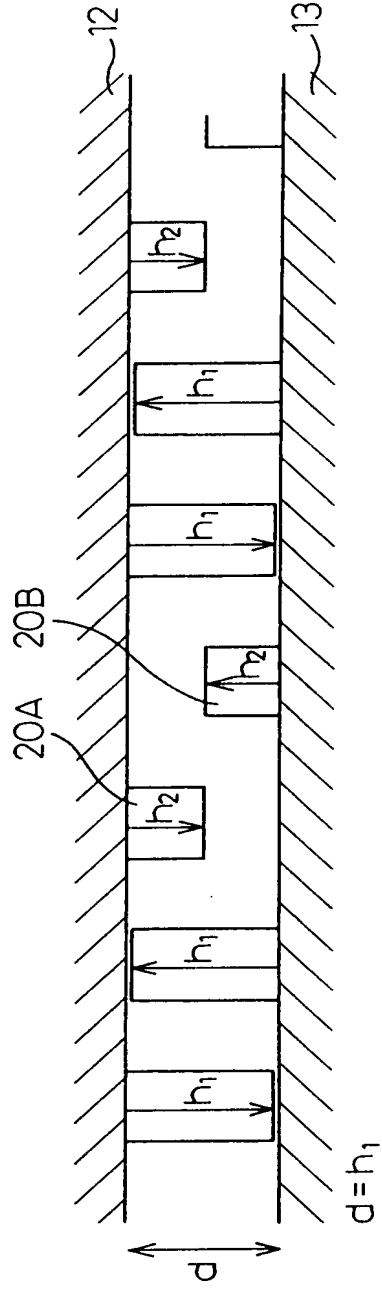


Fig. 124B

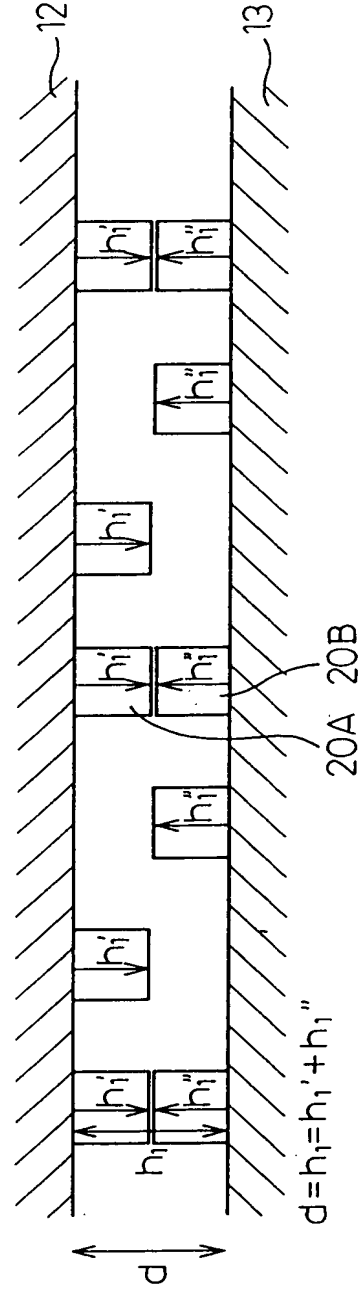


Fig. 125A

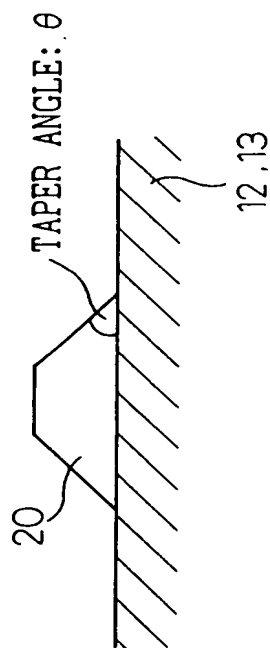


Fig. 125B

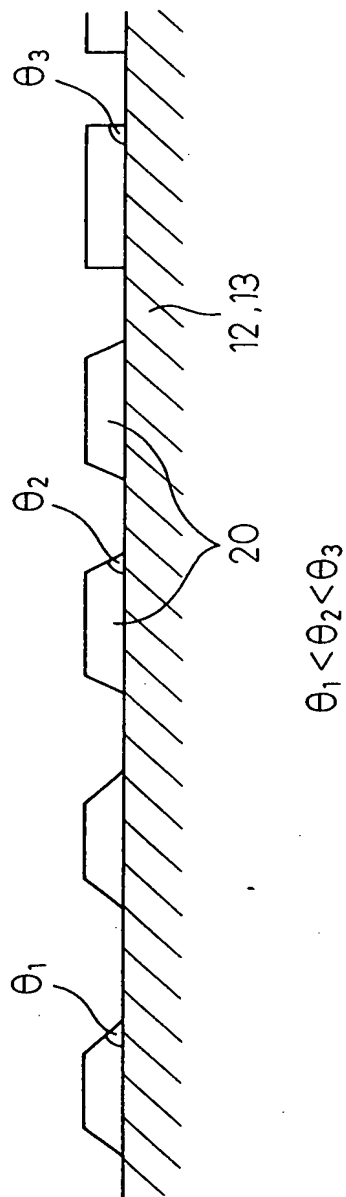
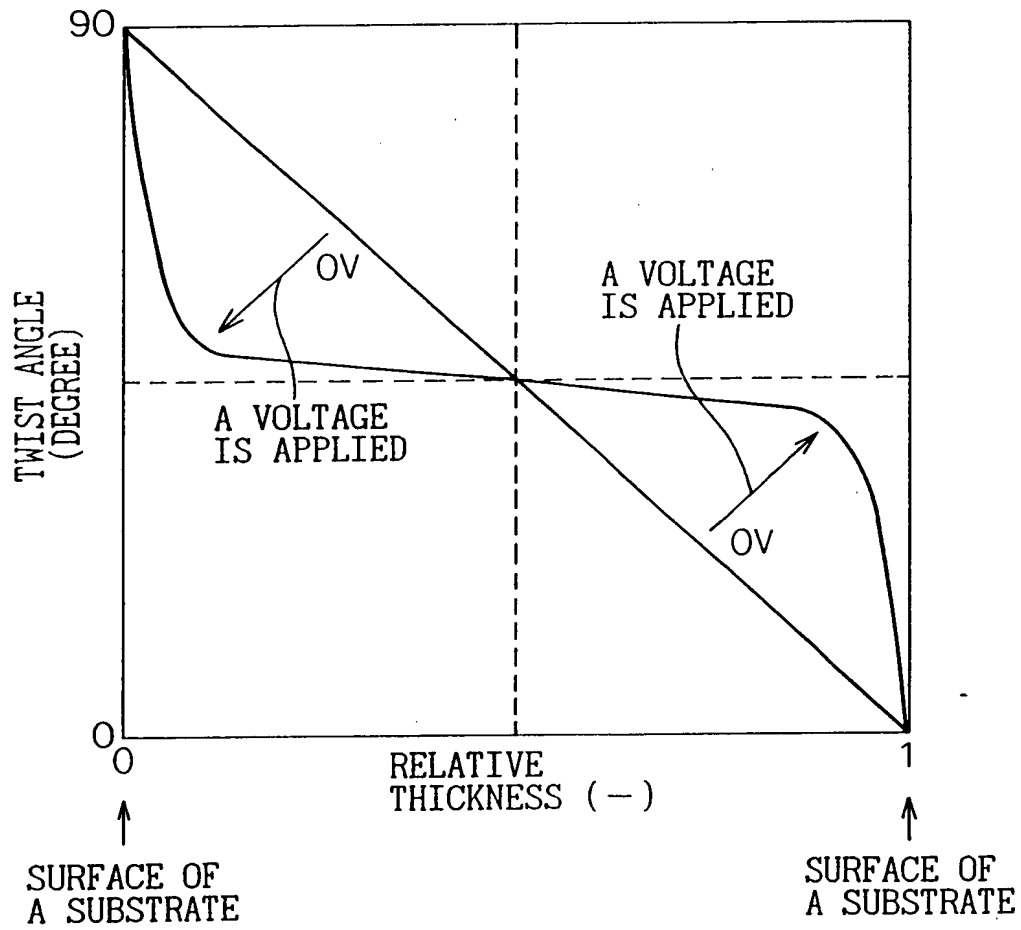
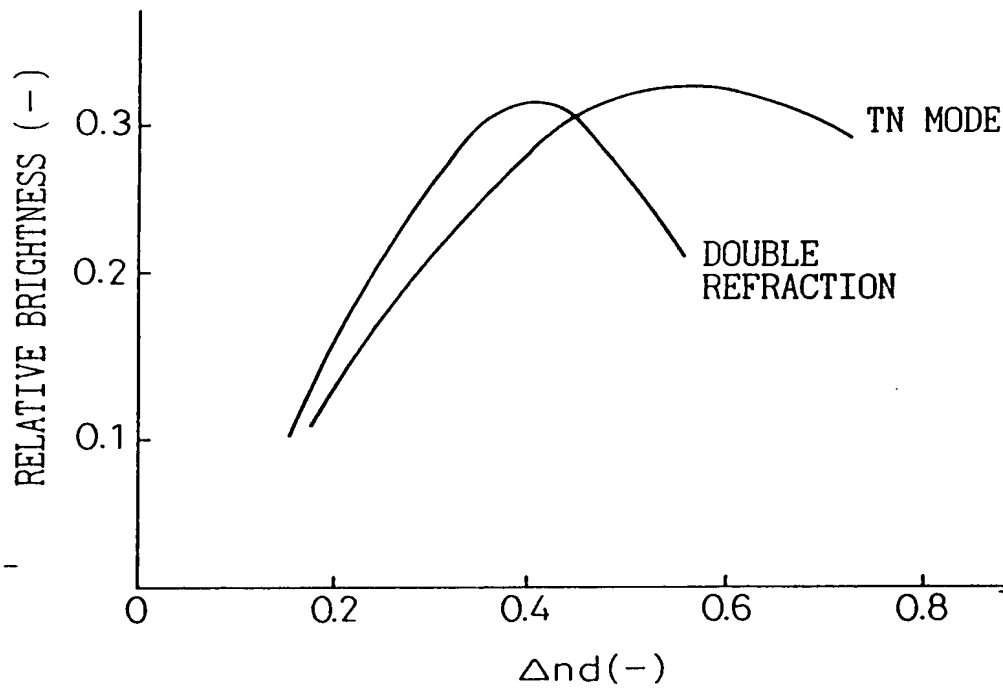


Fig .126



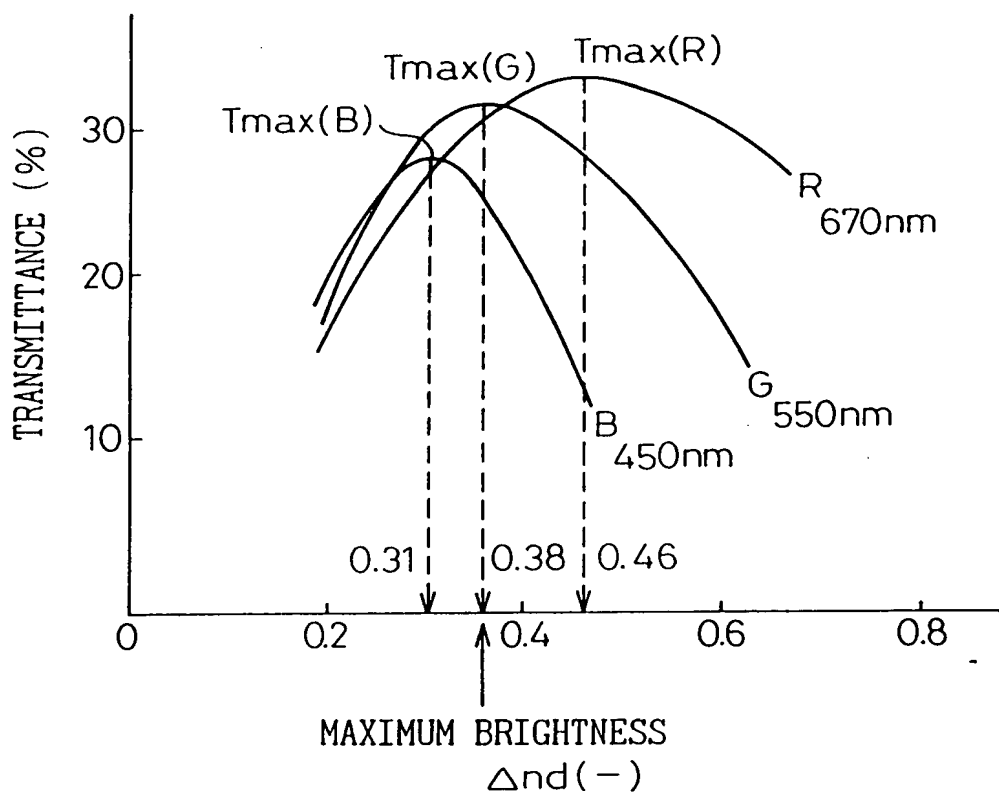
123/246

Fig. 127



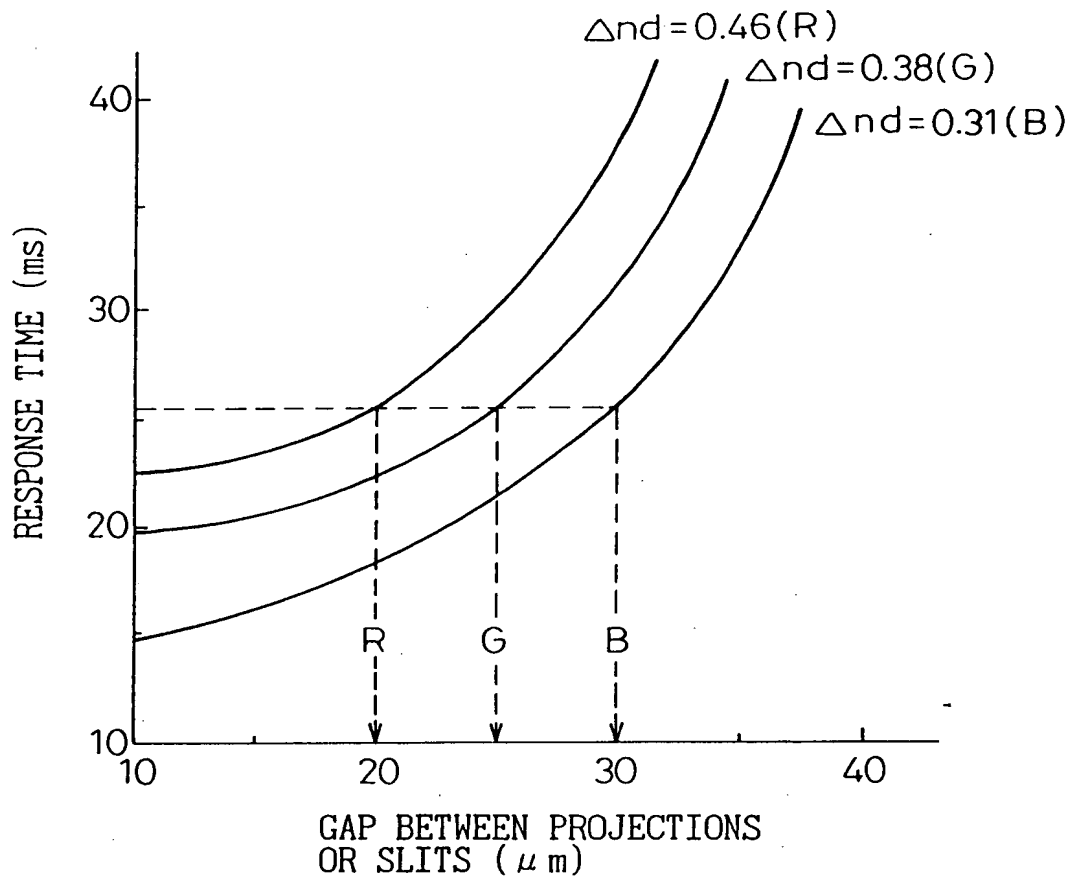
124/
246

Fig .128



125/
246

Fig. 129



126/246

Fig .130

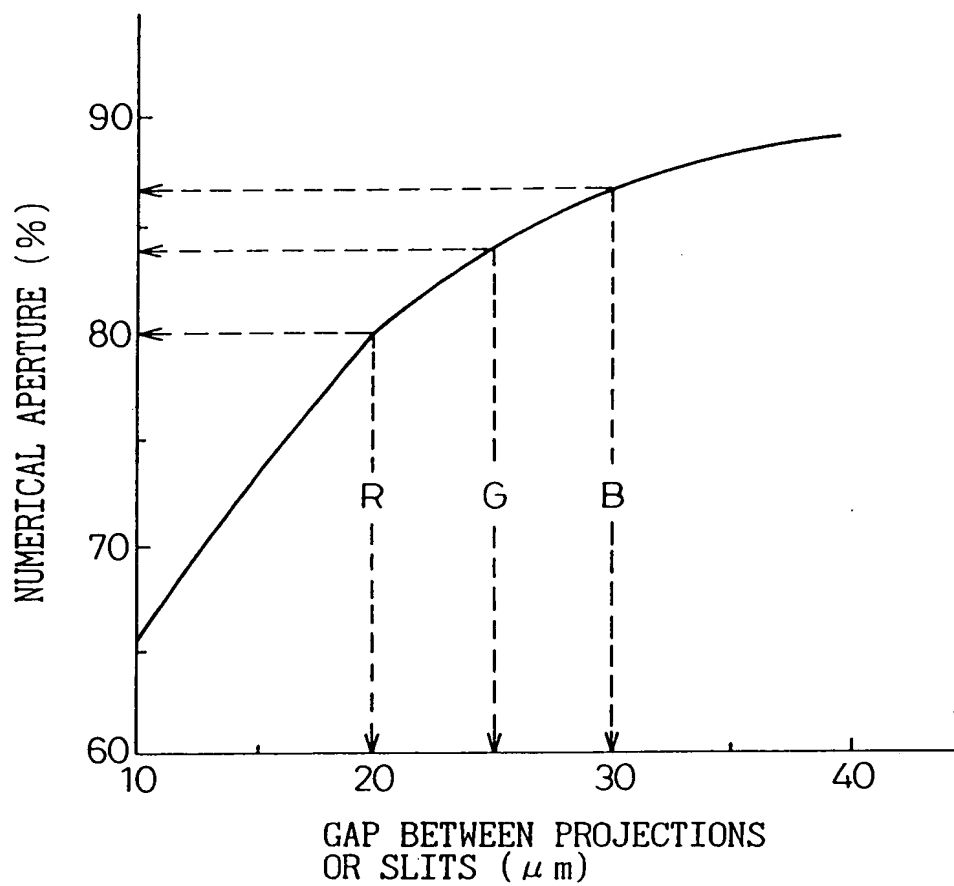


Fig. 131

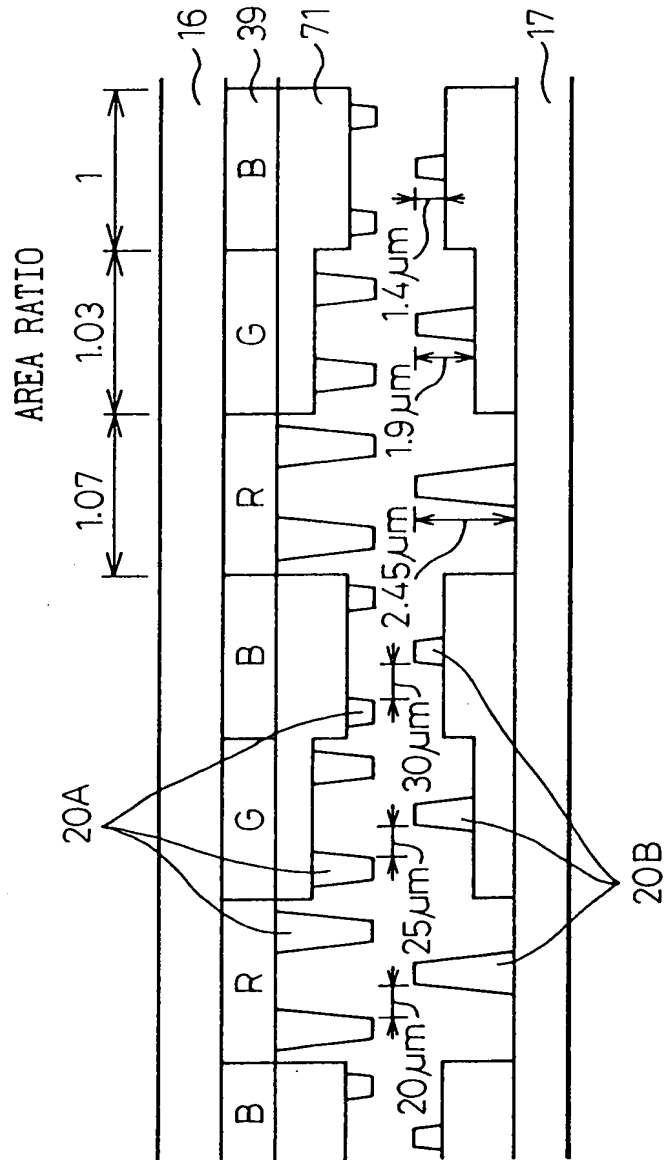


Fig. 132

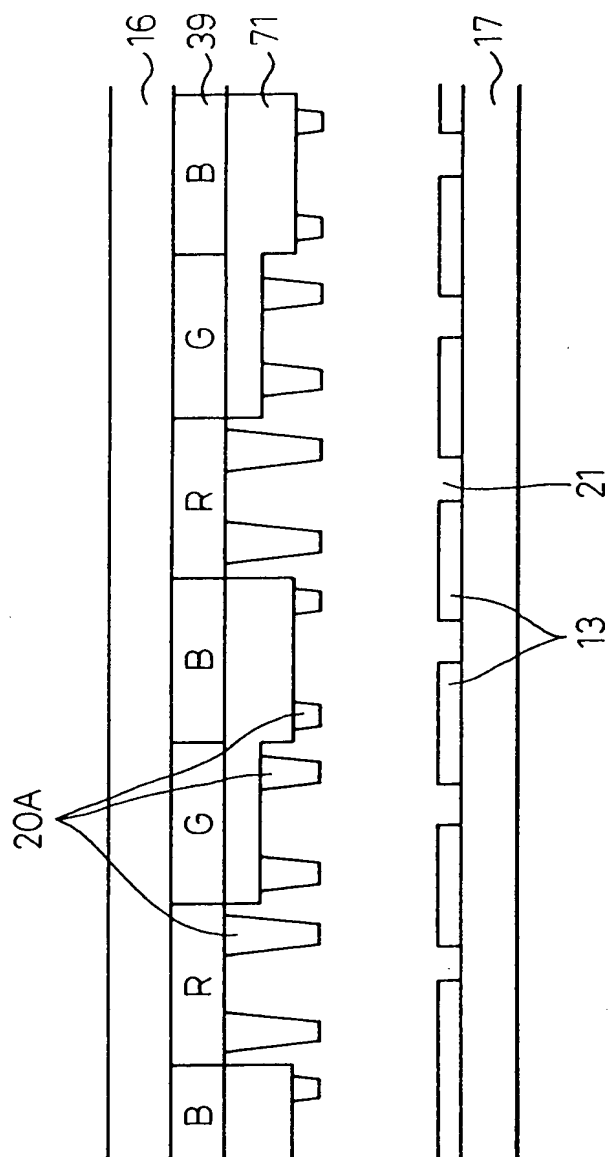


Fig. 133

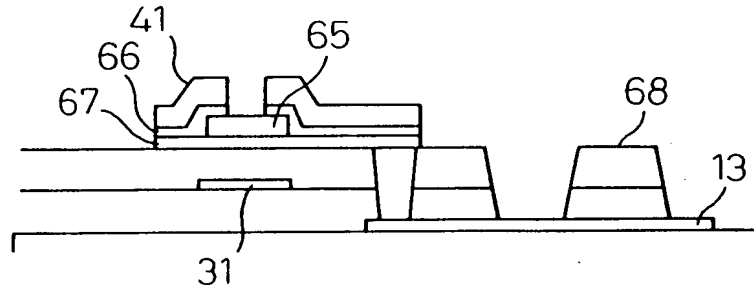


Fig. 134A

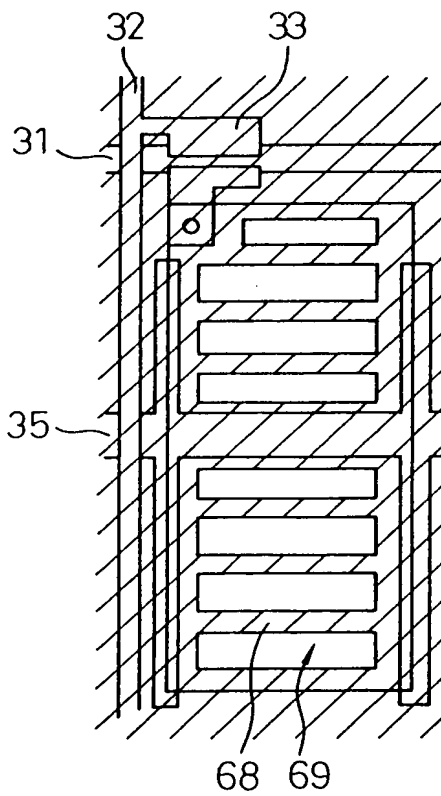


Fig. 134B

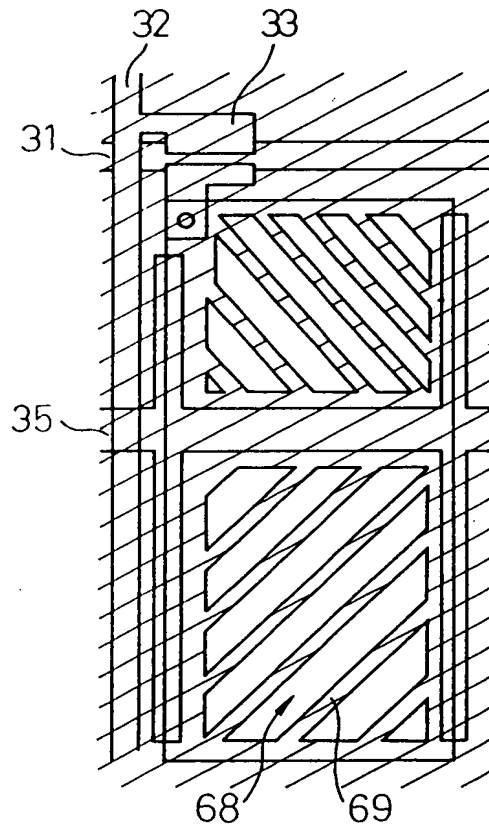
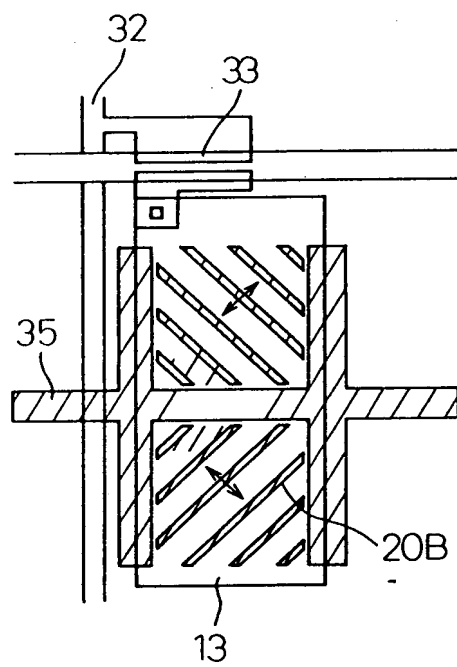
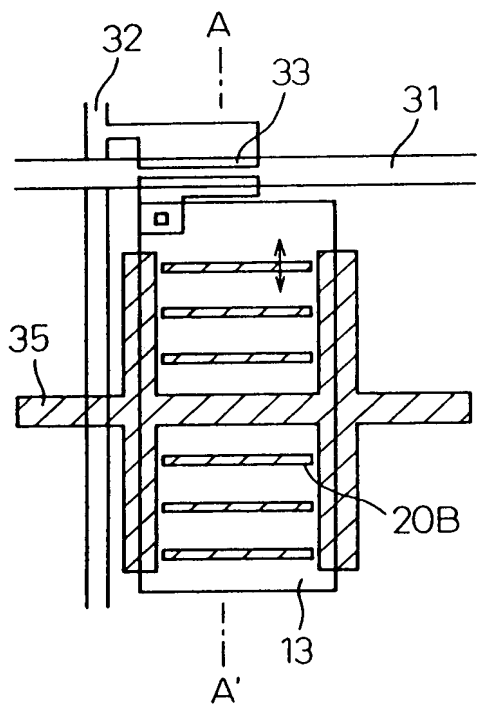




Fig.136A

Fig.136B



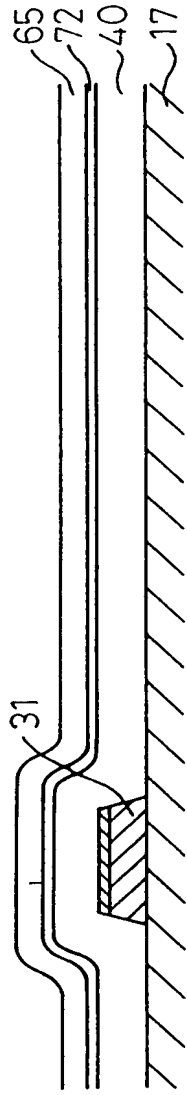


Fig. 137A

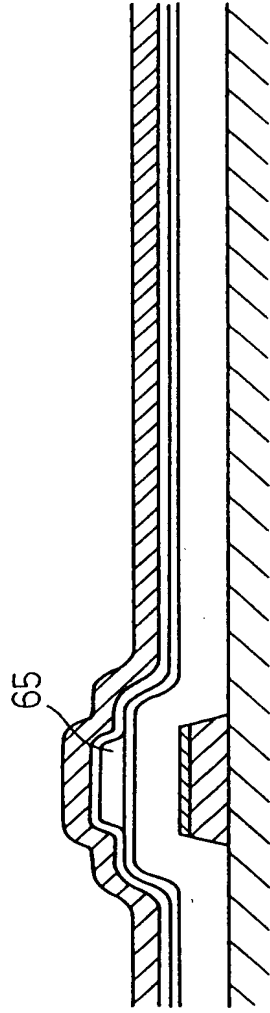


Fig. 137B

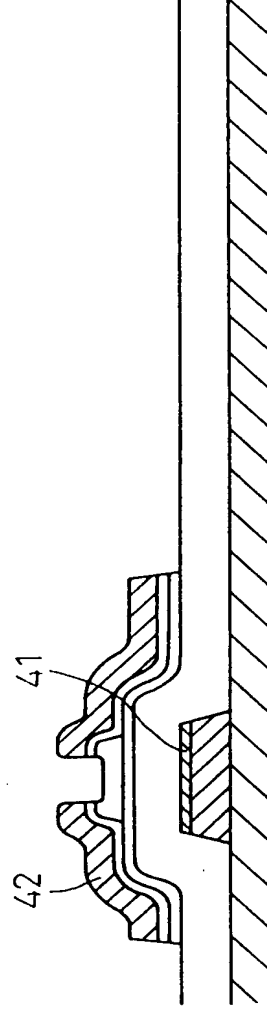


Fig. 137C

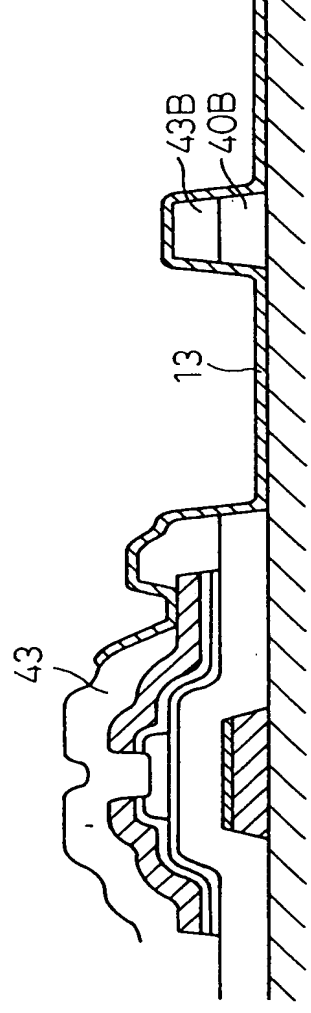
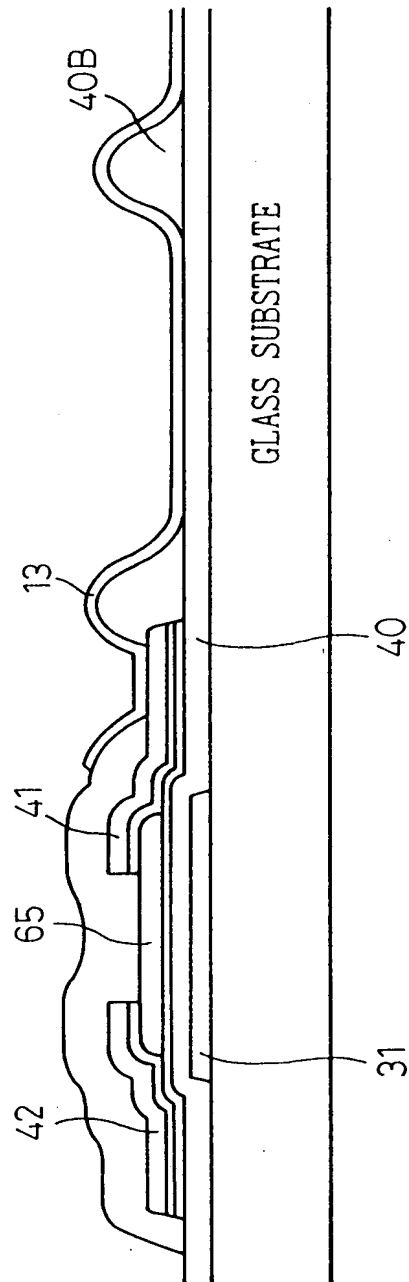


Fig. 137D

Fig. 138



133/246

Fig. 139A

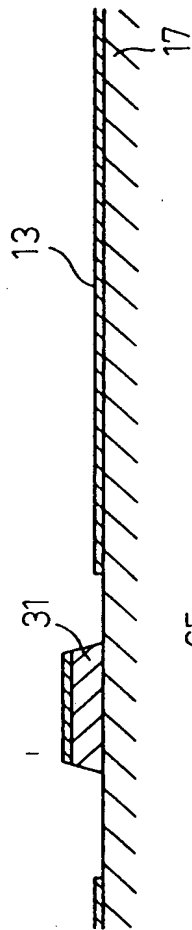


Fig. 139B

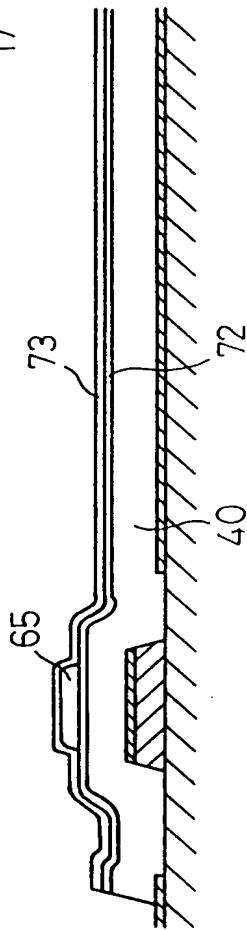


Fig. 139C

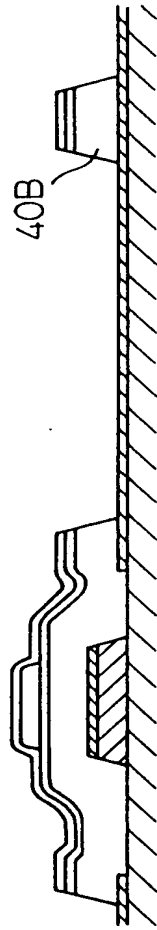


Fig. 139D

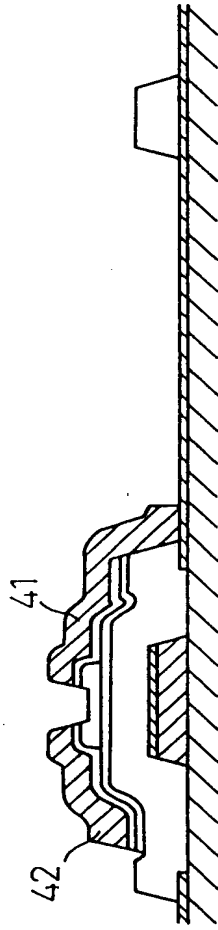
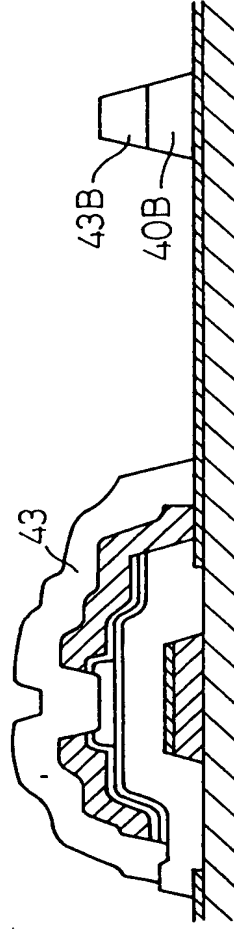


Fig. 139E



135/
246

Fig.140A

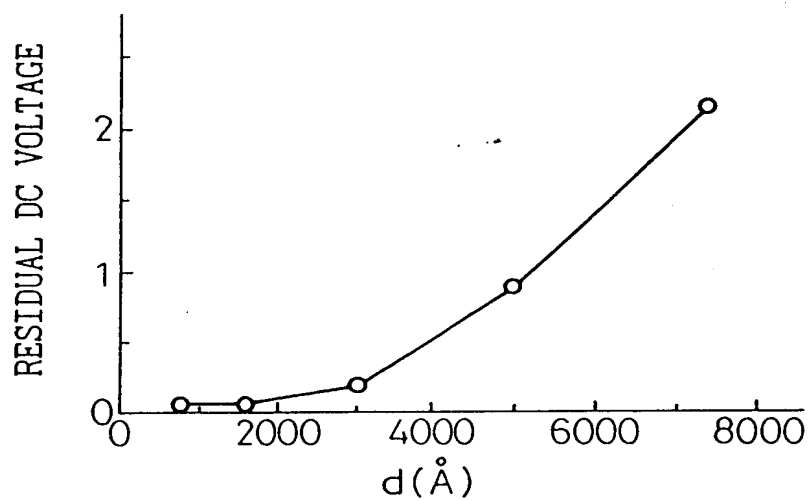
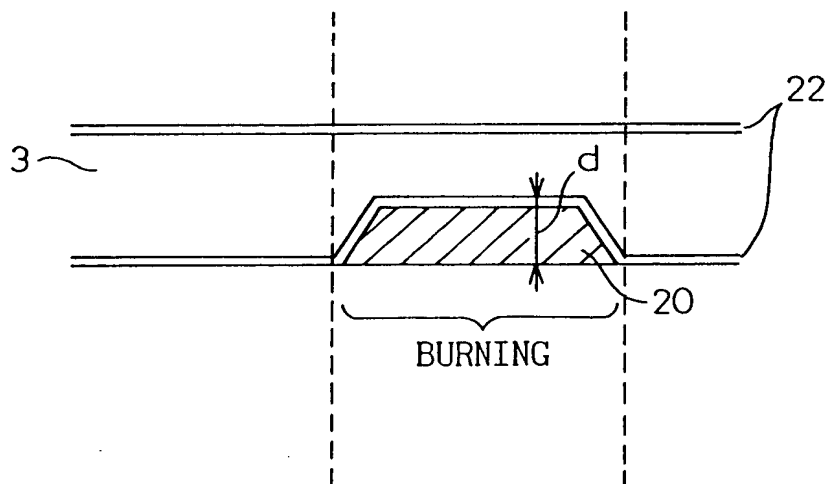


Fig.140B



136/246

Fig. 141A

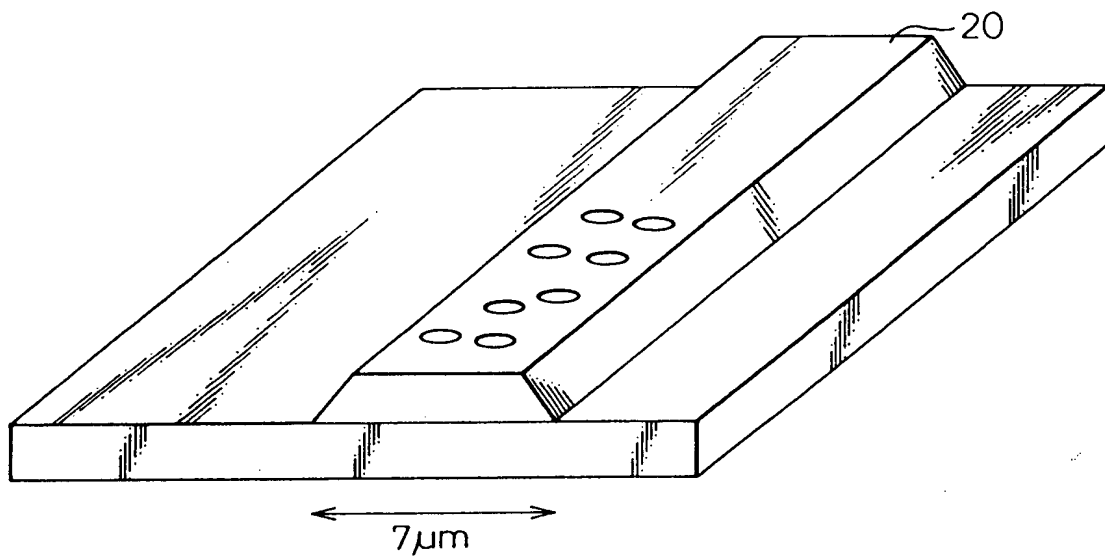
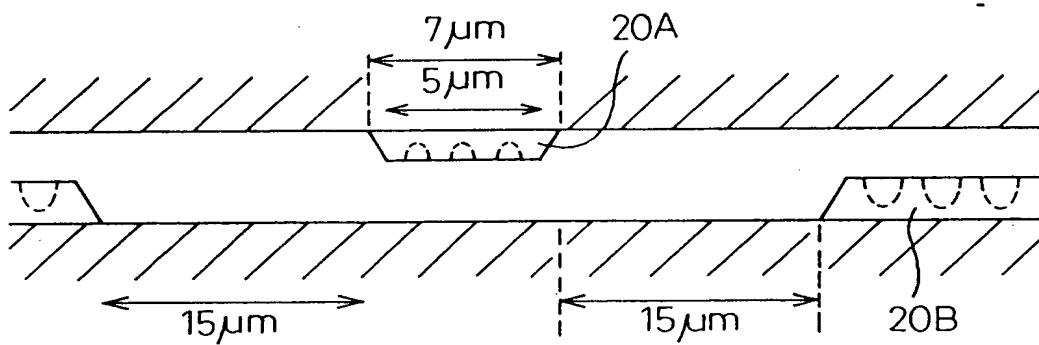


Fig. 141B



137/246

Fig.142A

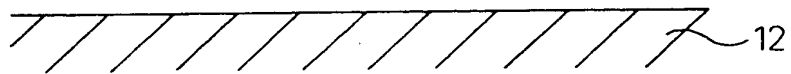


Fig.142B

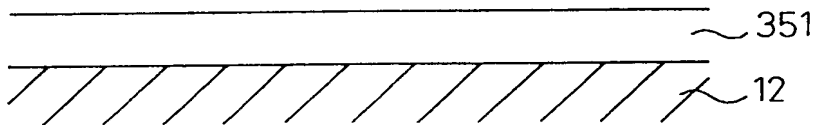


Fig.142C

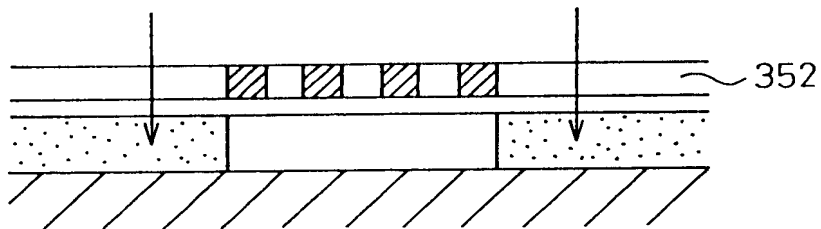


Fig.142D

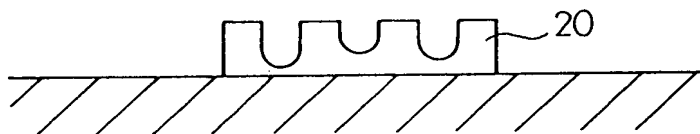
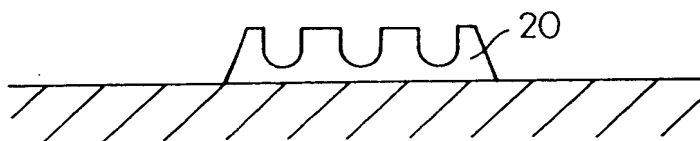
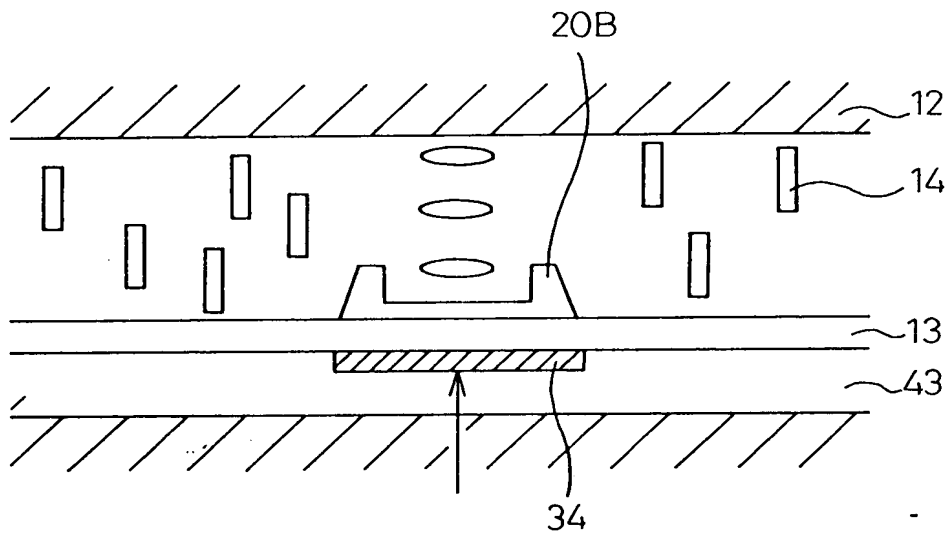


Fig.142E



138/
246

Fig.143



139/
246

Fig. 144A

BEFORE BAKING

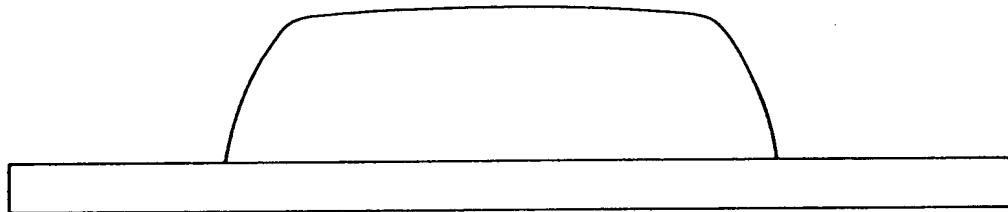
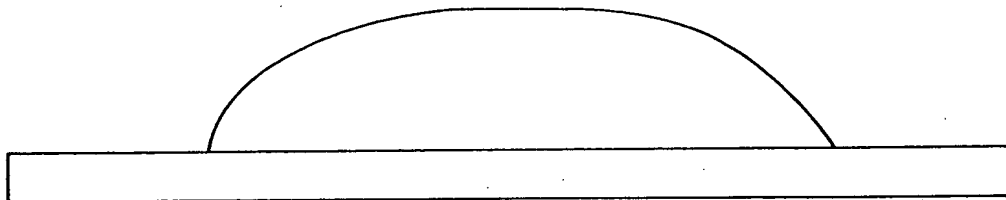
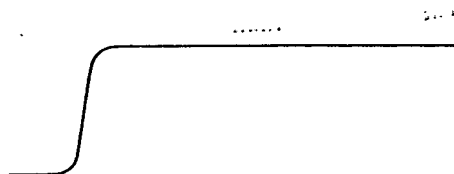


Fig. 144B

AFTER BAKING



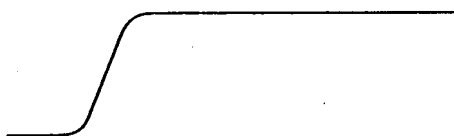
NO BAKING



120°C



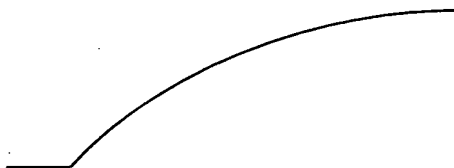
130°C



140°C



150°C

[illegible]

$\frac{1}{\sqrt{\pi}} \int_{-\infty}^{\infty} f(x) e^{-x^2} dx = \frac{1}{\sqrt{\pi}} \int_{-\infty}^{\infty} f(x) e^{-x^2} dx$

Fig. 146A

2 μ m WIDTH



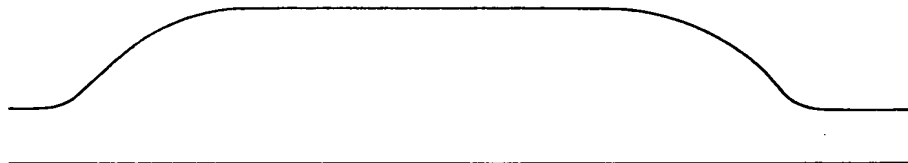
Fig .146B

5 μ m WIDTH



Fig. 146C

10 μ m WIDTH.



142/246

Fig. 147A

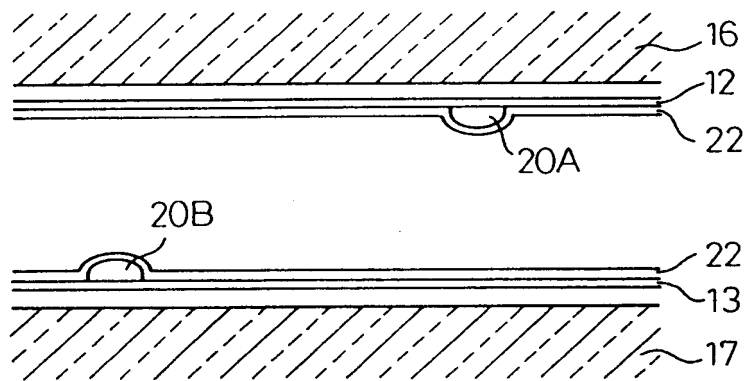
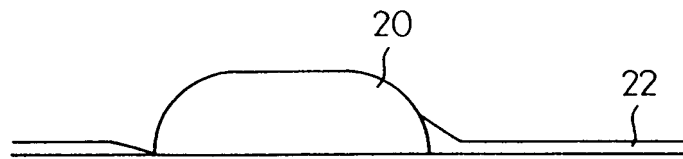


Fig. 147B



143/
246

Fig.148A

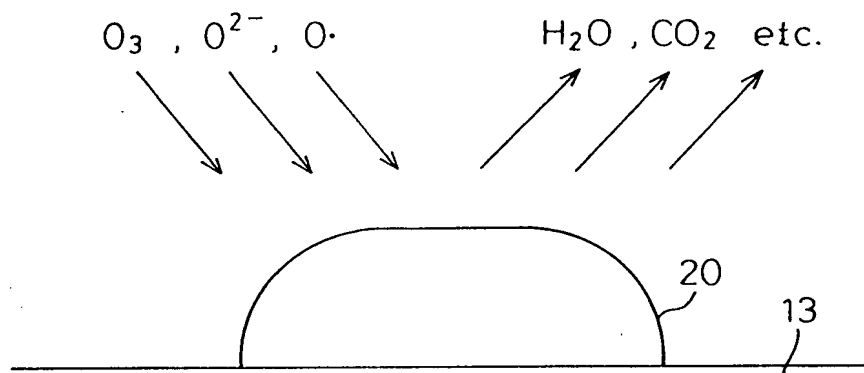


Fig.148B

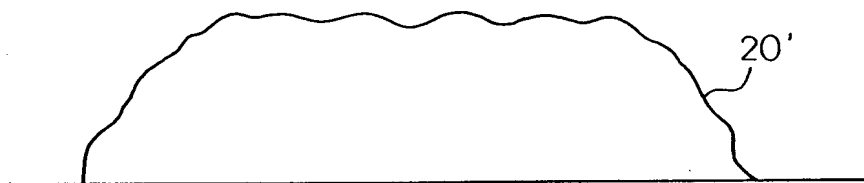
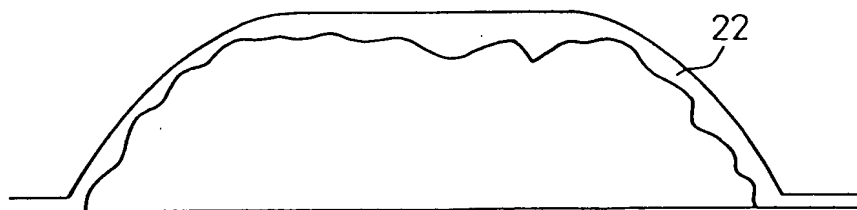


Fig.148C



144/246

Fig.149A

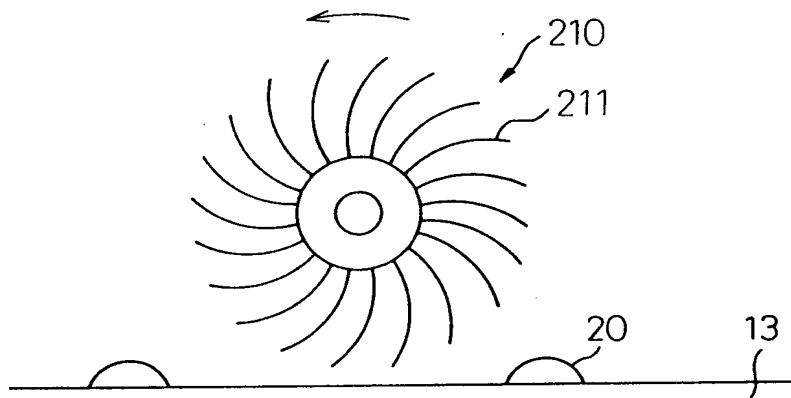
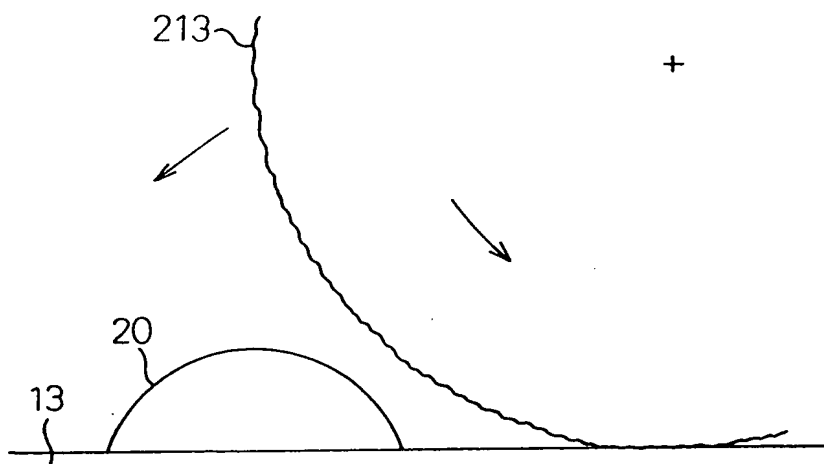
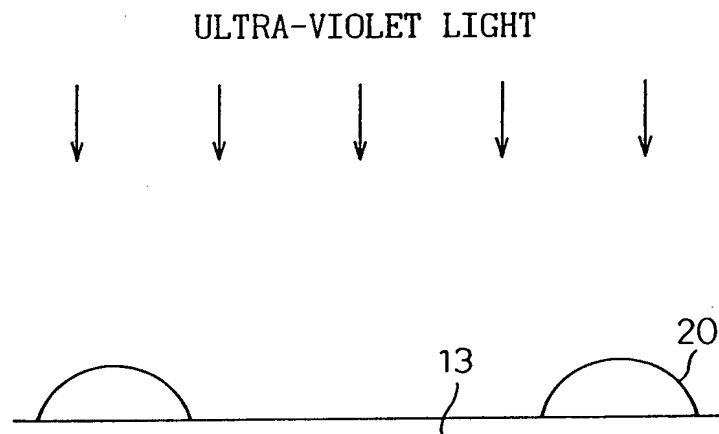


Fig.149B



145/
246

Fig. 150



146/
246

Fig.151A

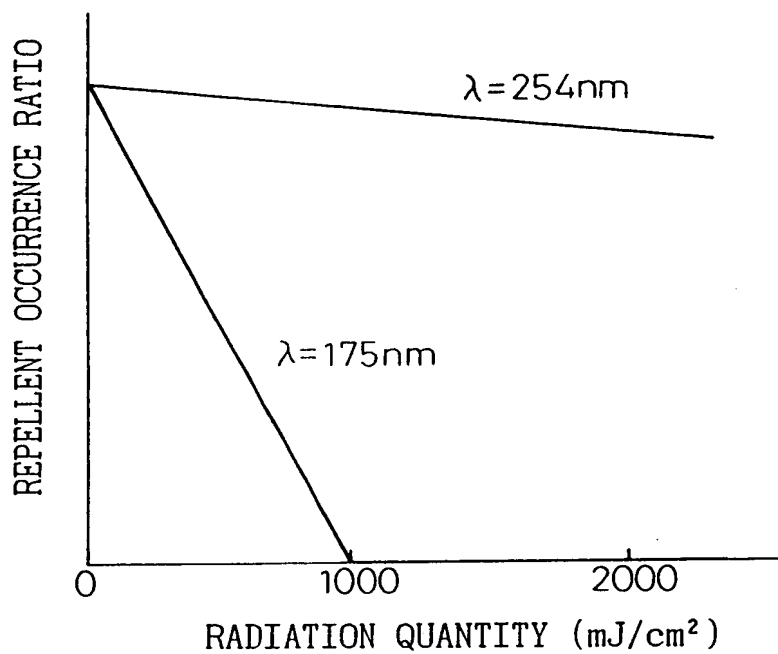


Fig.151B

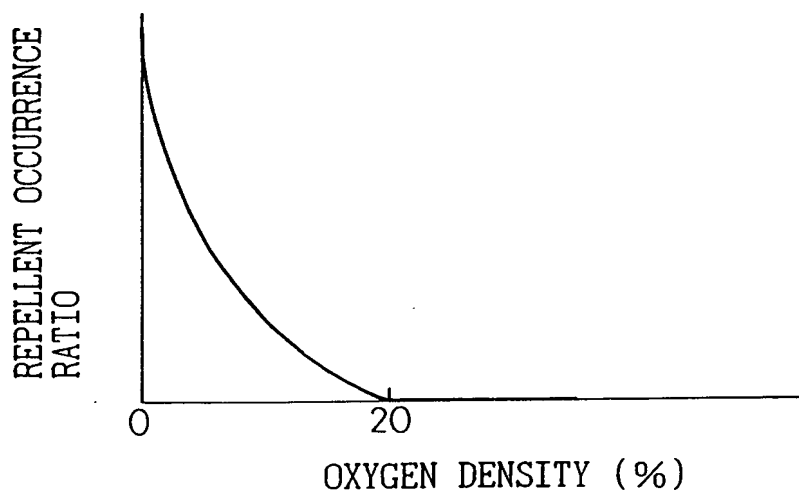


Fig.152A

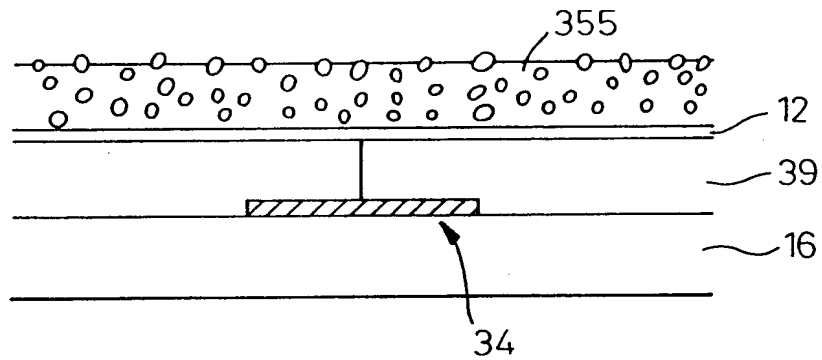


Fig.152B

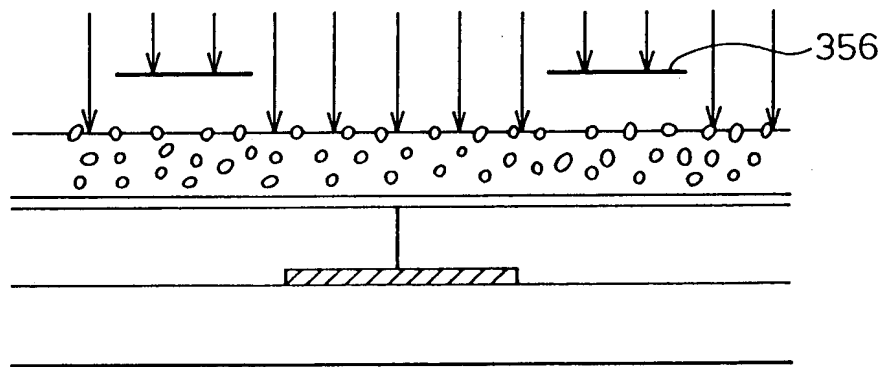
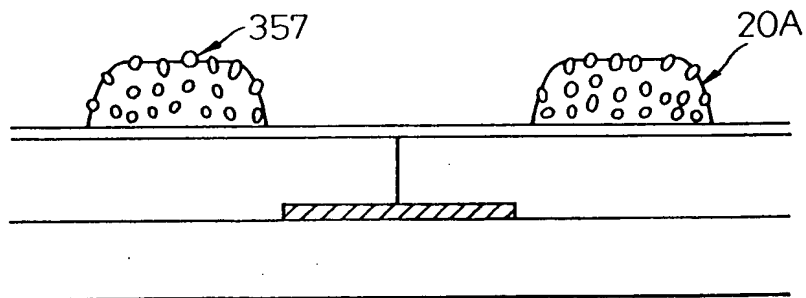


Fig.152C



148/246

Fig.153A

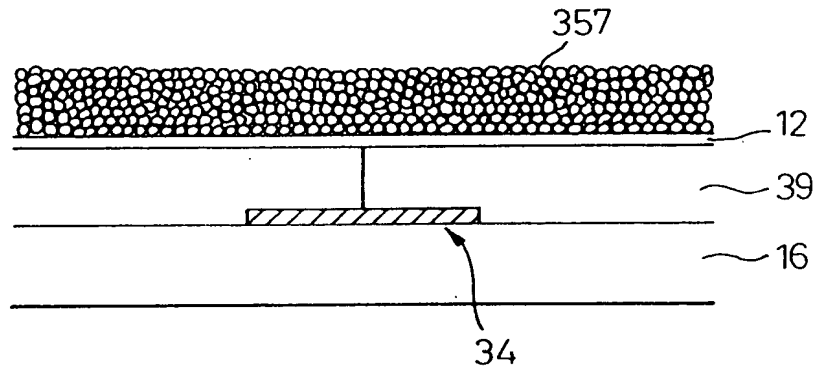


Fig.153B

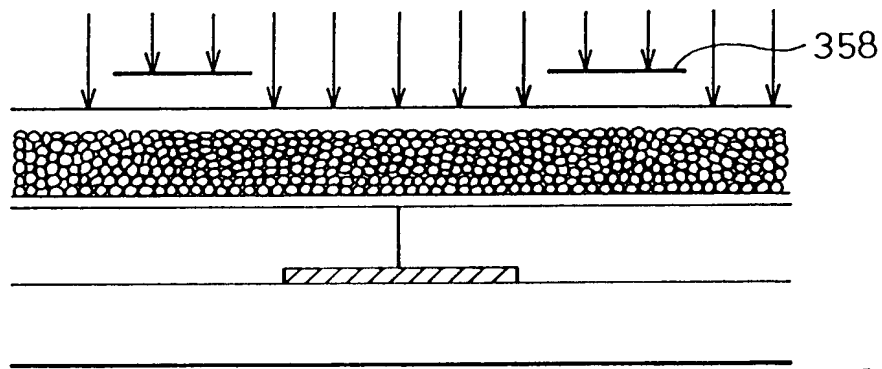
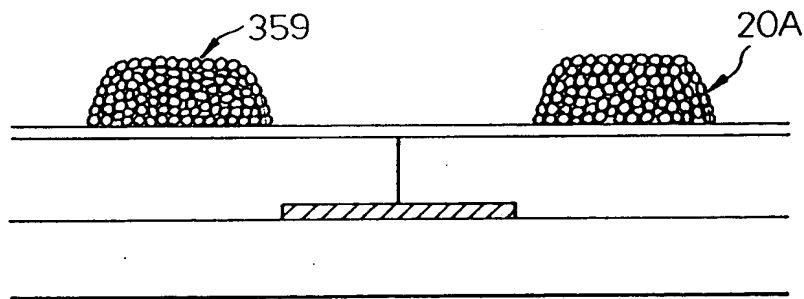


Fig.153C



149/
246

Fig.154A

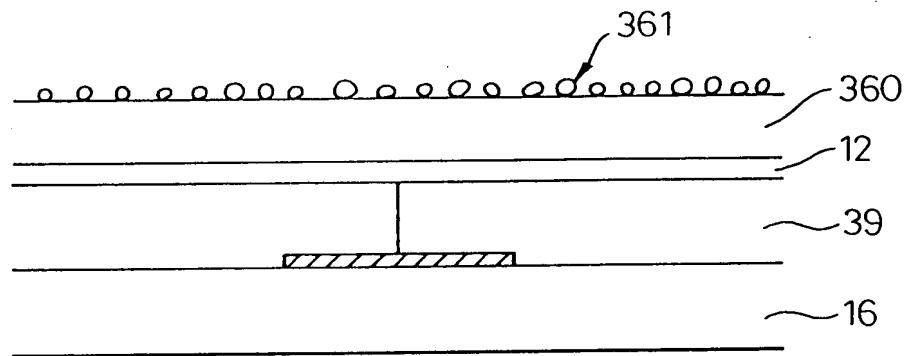
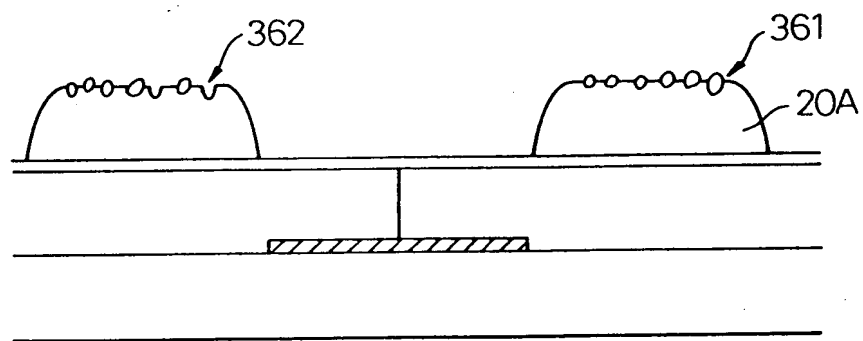


Fig.154B



150/
246

Fig.155A

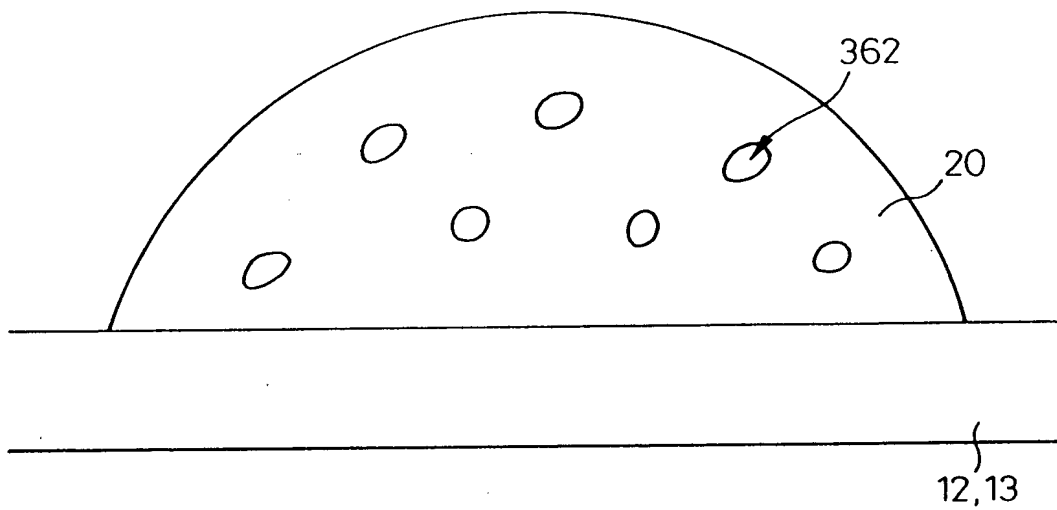


Fig.155B

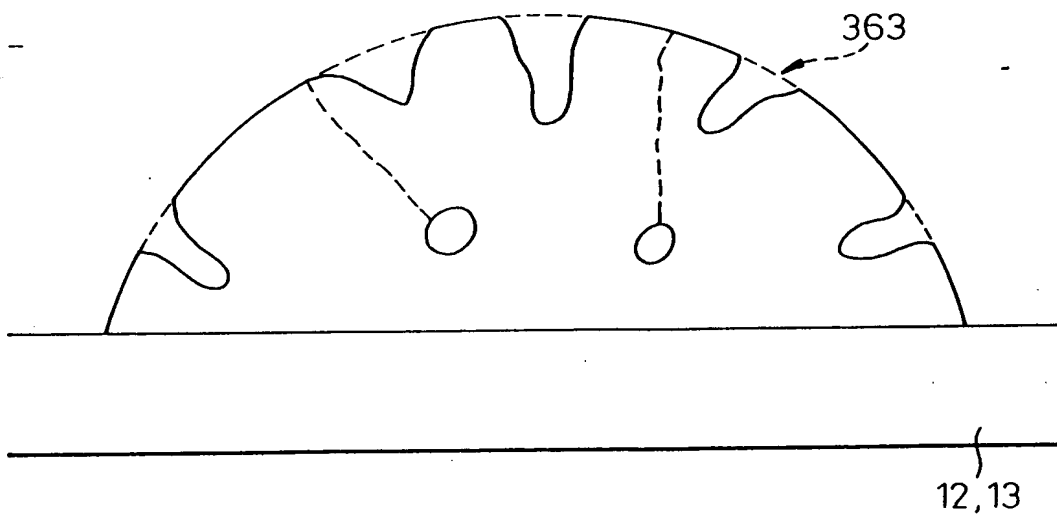
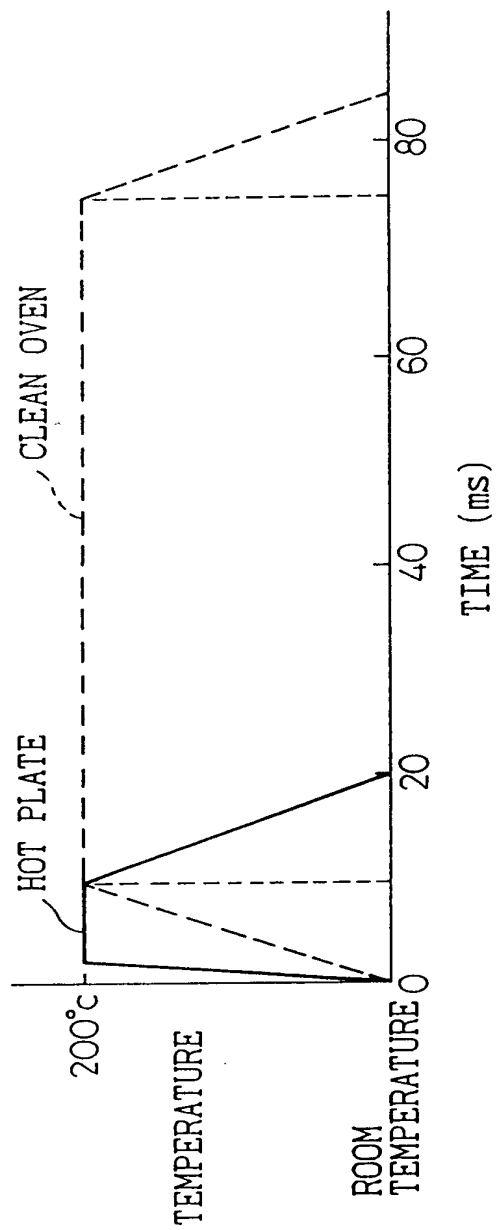


Fig. 156



152/
246

Fig.157A

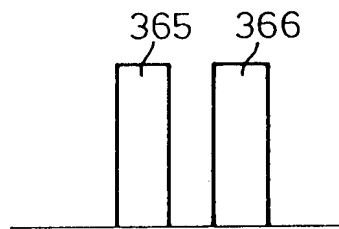


Fig.157B

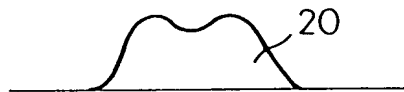


Fig.157C

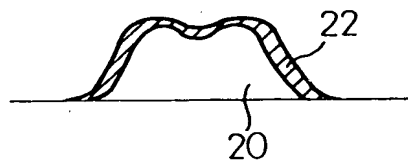
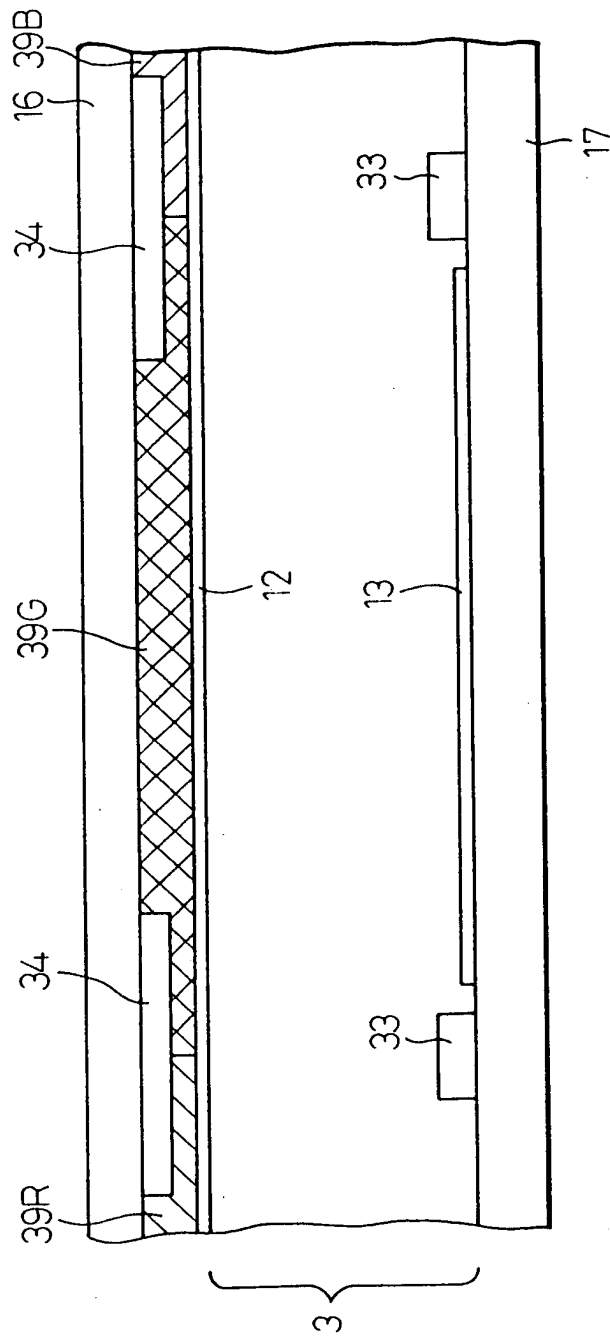
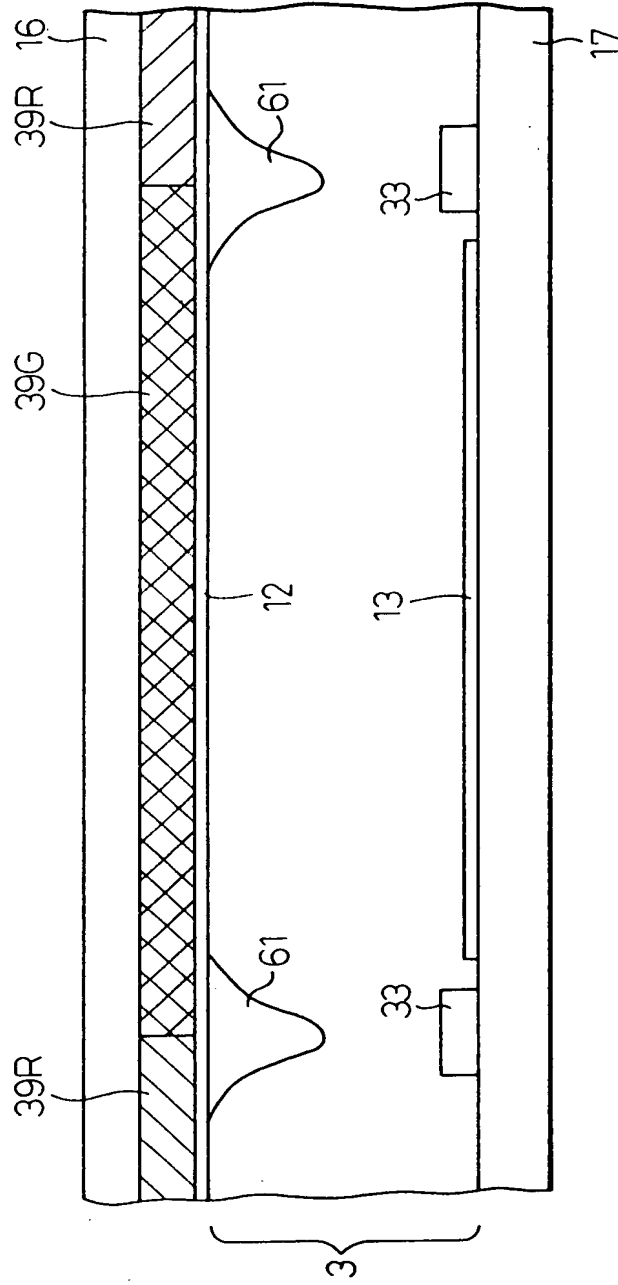


Fig.158



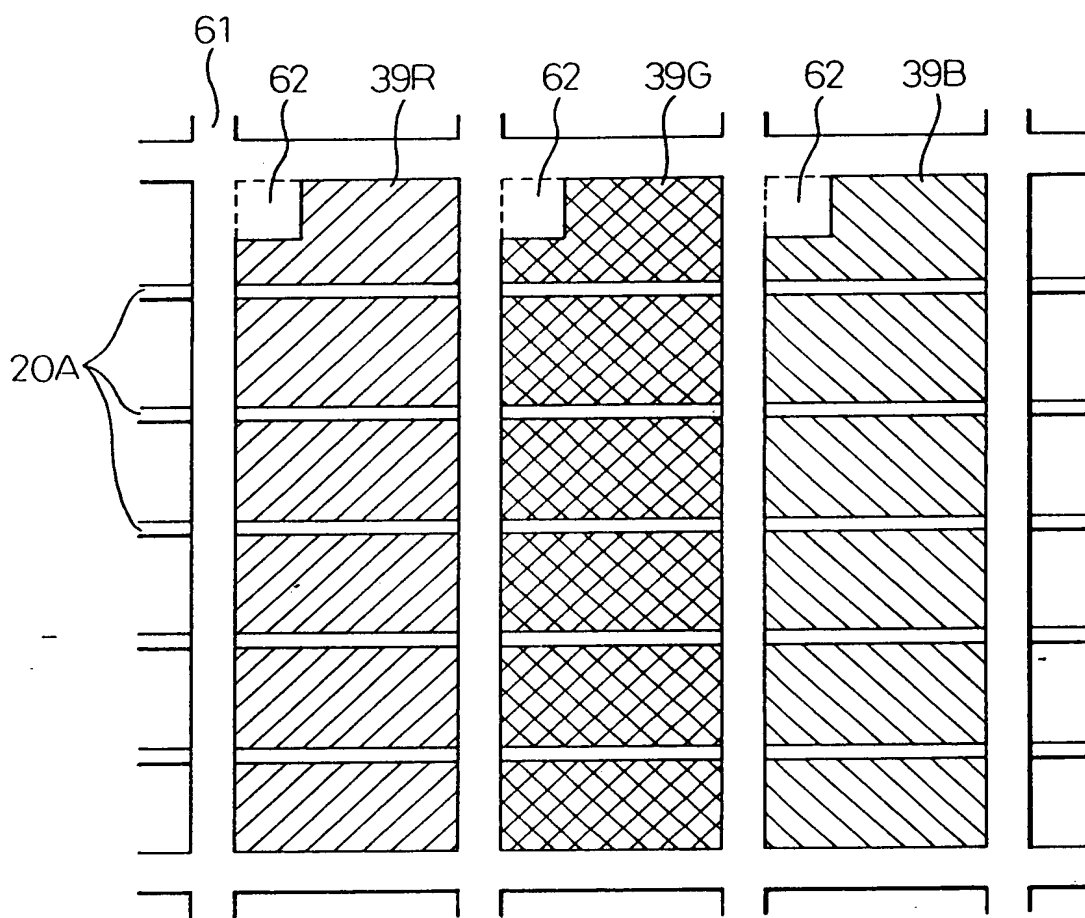
153/246

Fig.159



154/246

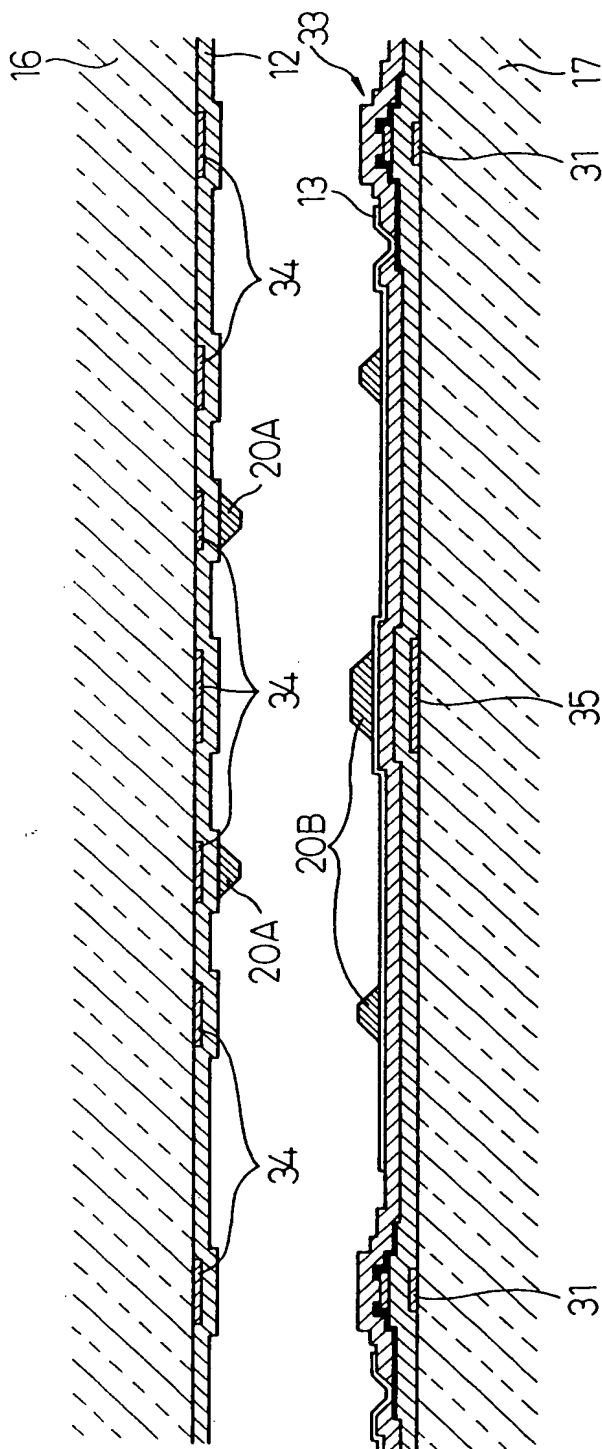
Fig. 160



1



Fig.162



157/246

158/246

Fig.163

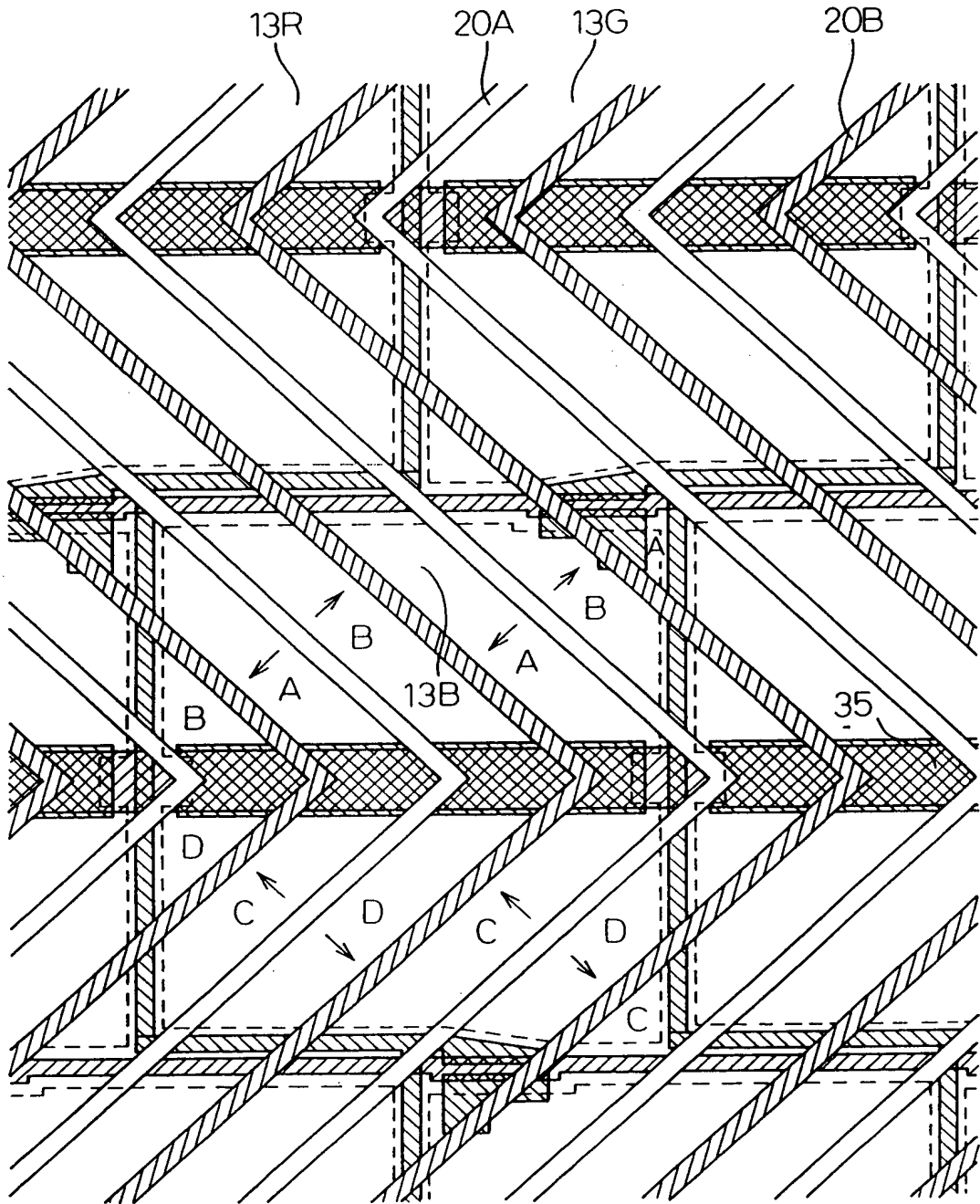


Fig. 165A

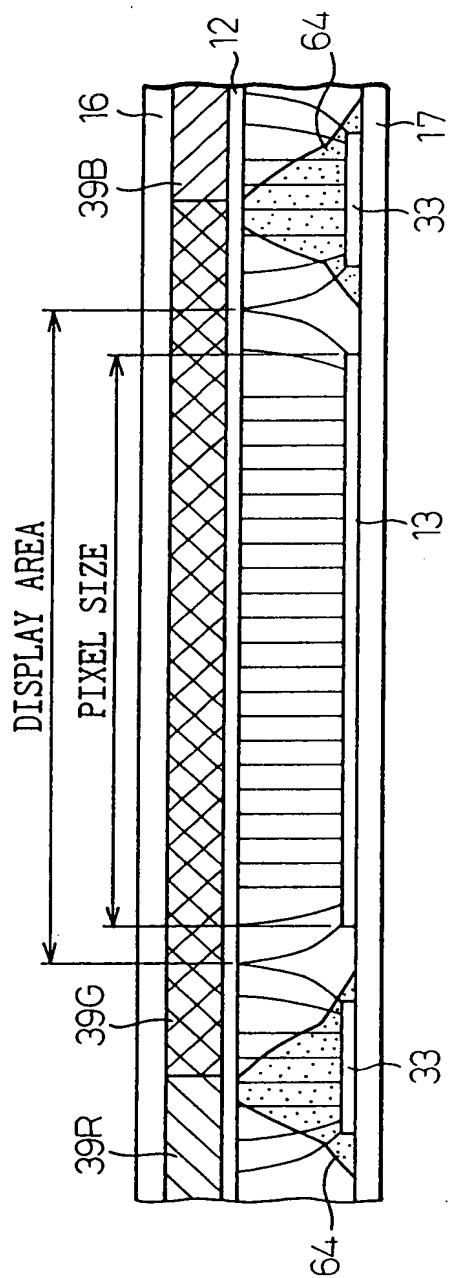


Fig. 165B

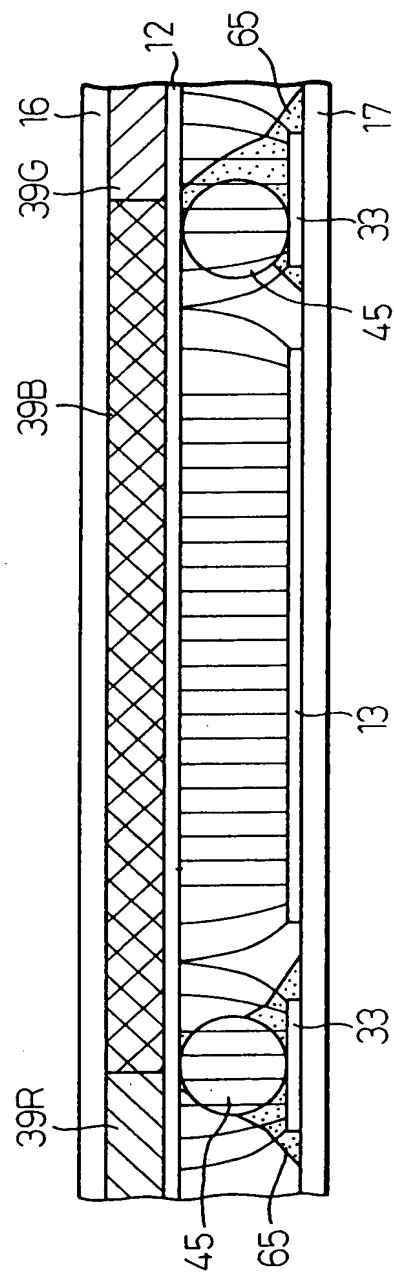


Fig. 166A

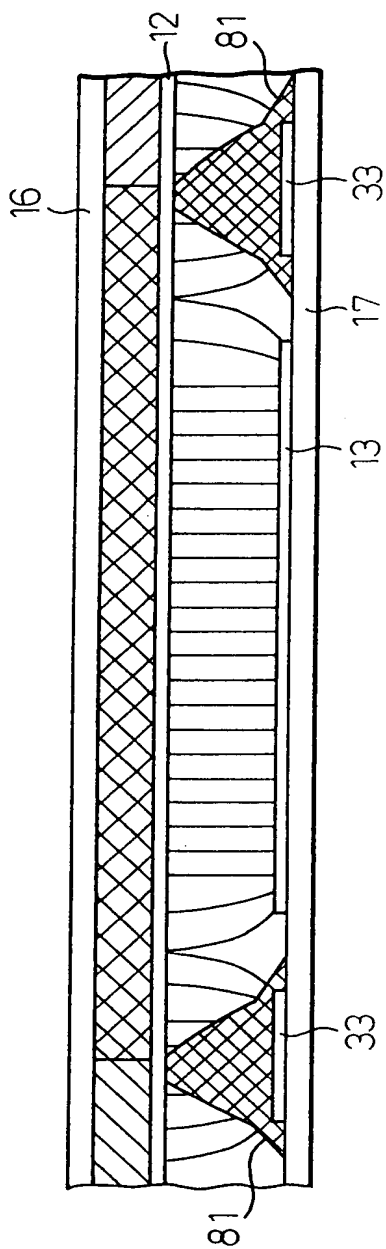


Fig. 166B

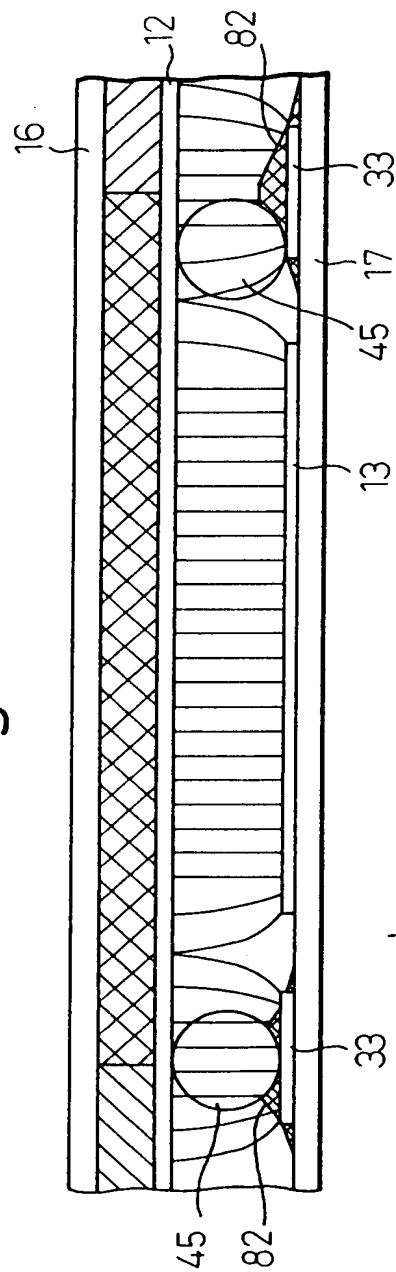
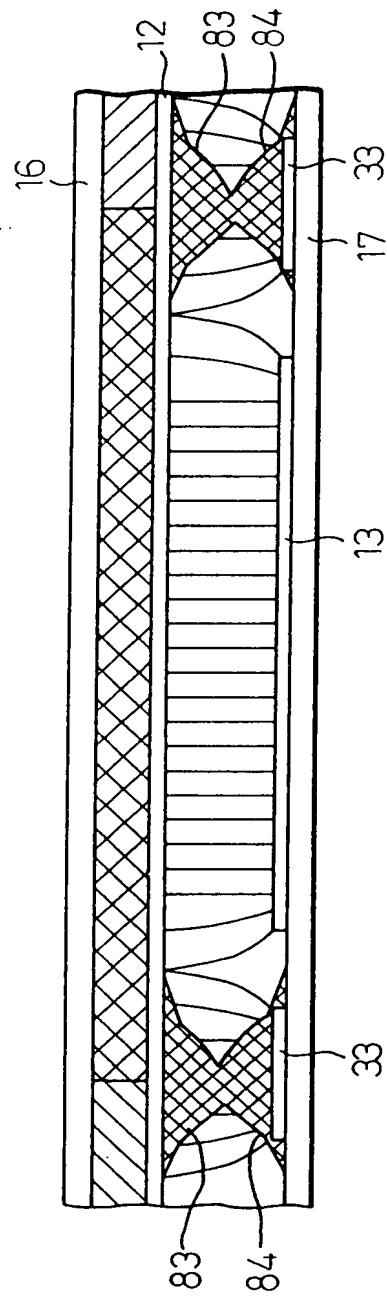


Fig.167



163/246

Fig.168A

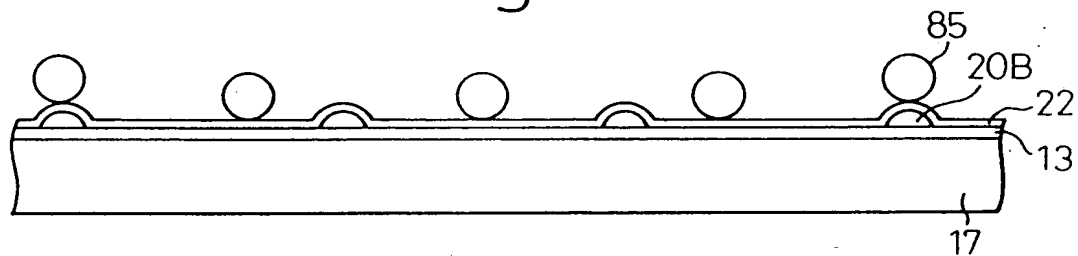


Fig.168B

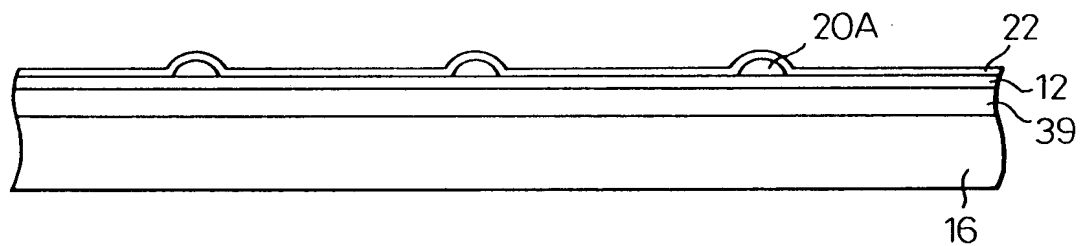
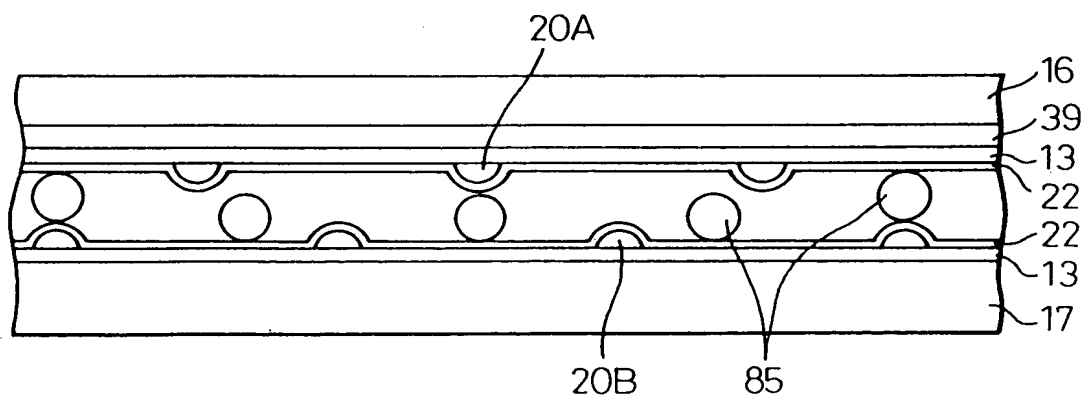


Fig.168C



164/246

Fig. 169

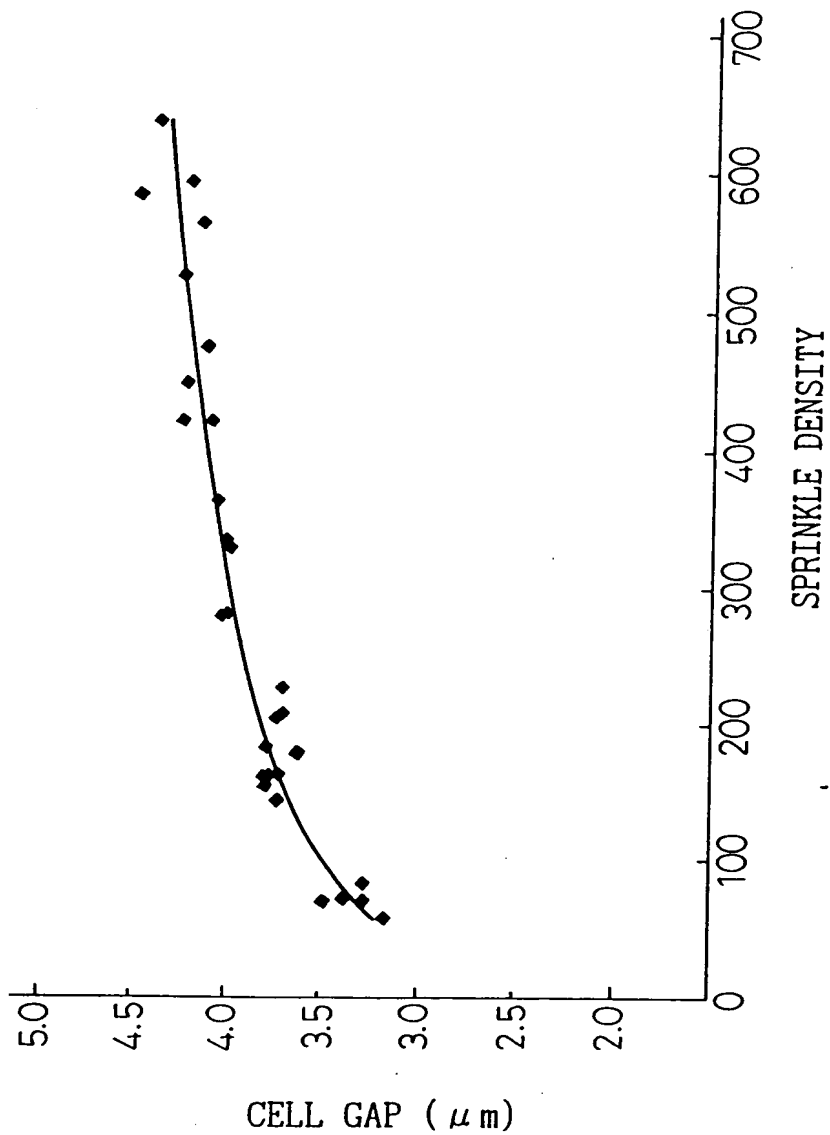
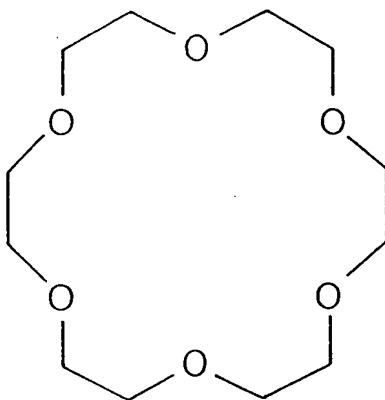


Fig.170

SPRINKLE DENSITY OF SPACERS (NUMBERS/mm ²)	50	100	150	200	250	300	350	400	450	500	550
BLEMISH OCCURRENCE DUE TO PUSHING	YES	YES	NO	NO	NO	NO	NO	NO	NO	NO	NO
BLEMISH OCCURRENCE DUE TO PULLING	NO	NO	NO	NO	NO	NO	YES	YES	YES	YES	YES

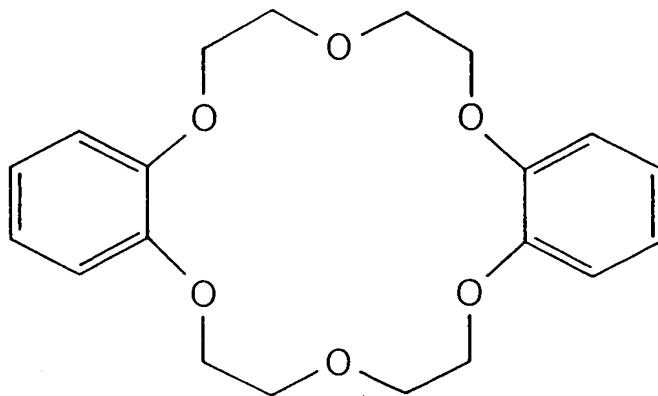
166/
246

Fig.171A



18-CROWN-6

Fig.171B

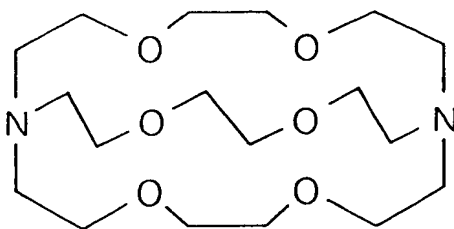


DIBENZOYL-18-CROWN-6

www.elsevier.com

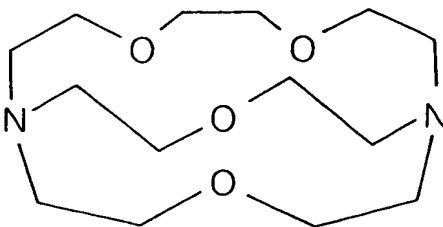
167/246

Fig.172A



CRYPTAND [2.2.2]

Fig.172B



CRYPTAND [2.1.1]

168/
246

Fig.173A

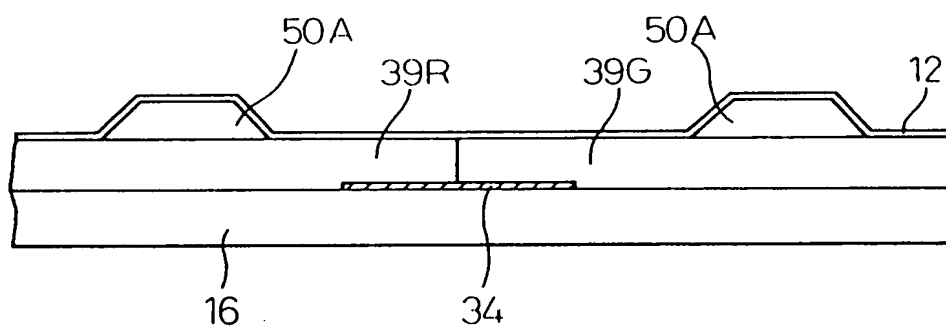
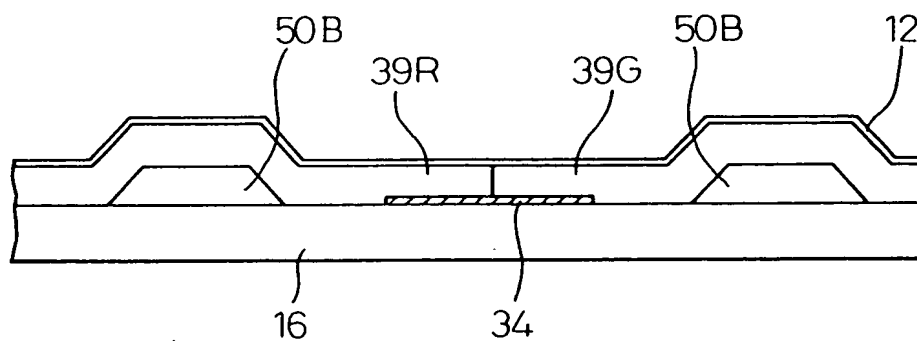


Fig.173B



169/246

Fig.174

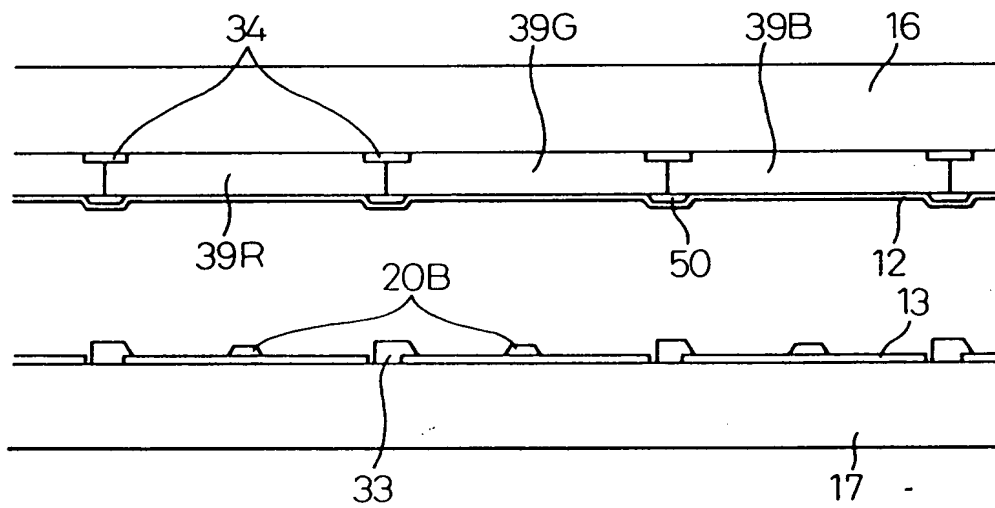


Fig.175A

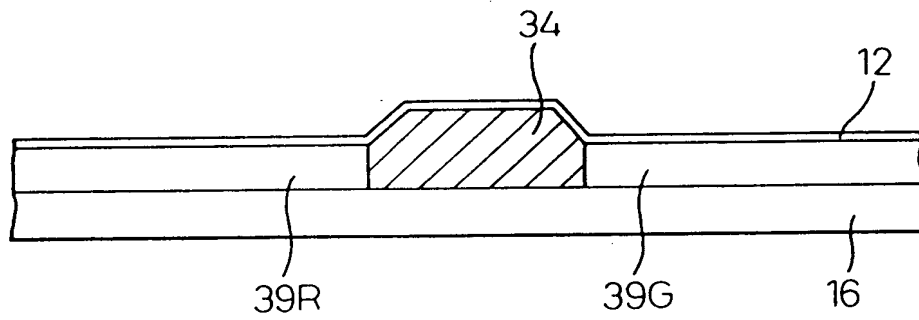
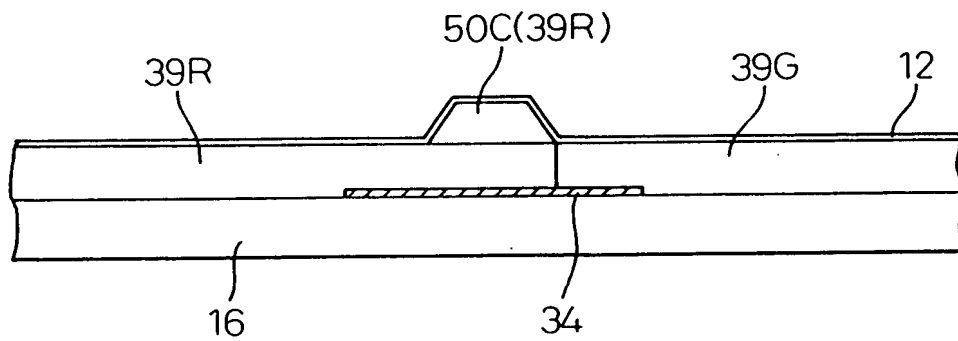


Fig.175B



171/246

Fig.176A

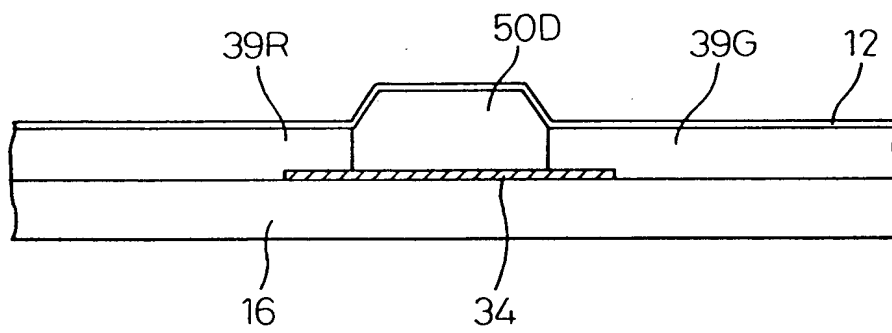
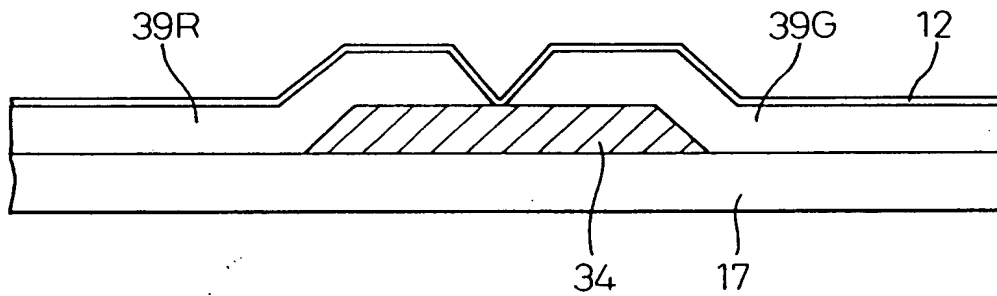


Fig.176B



172/246

Fig.177A

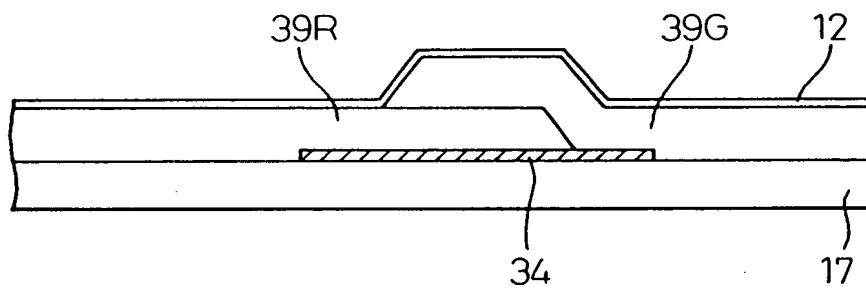
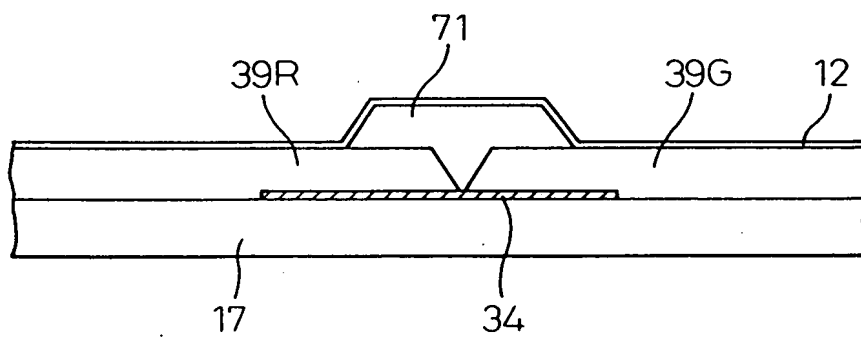
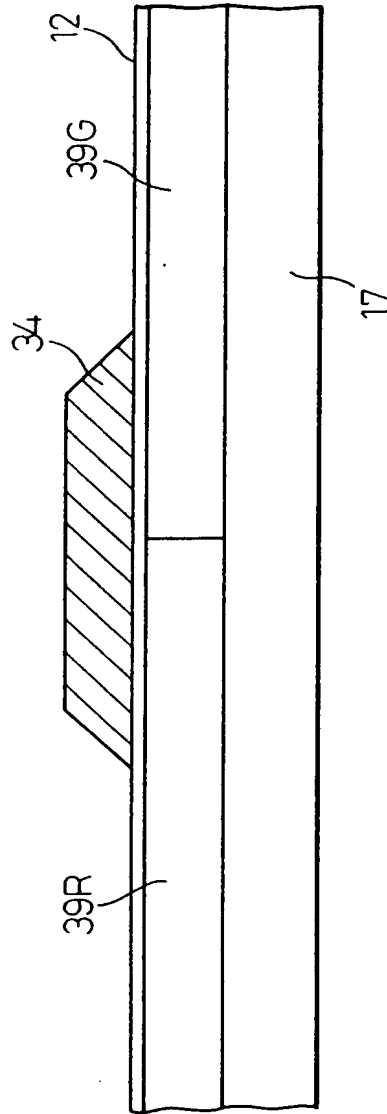


Fig.177B



[illegible]

174/246

Fig.179A

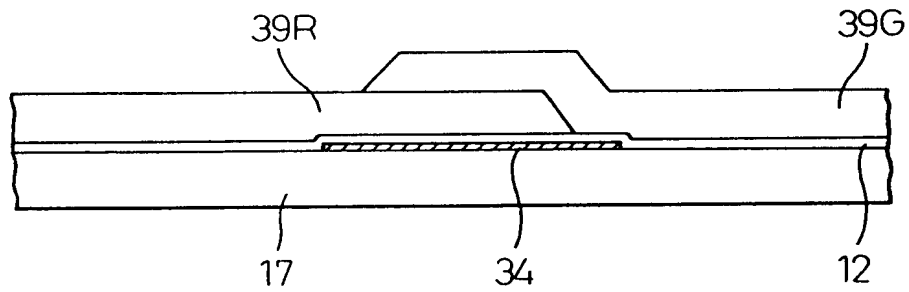
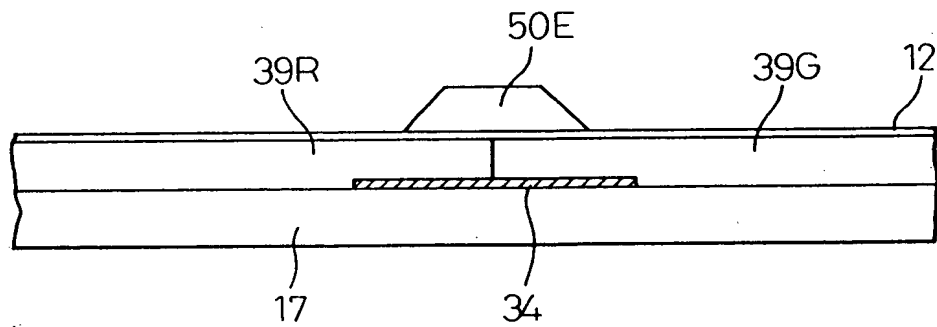


Fig.179B



175/246

Fig.180A

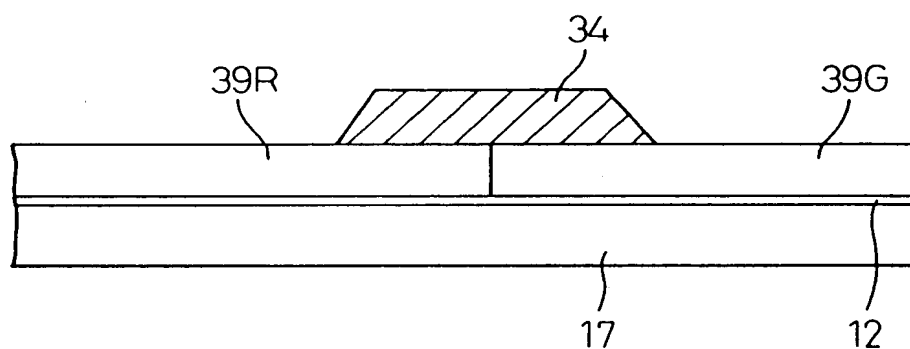


Fig.180B

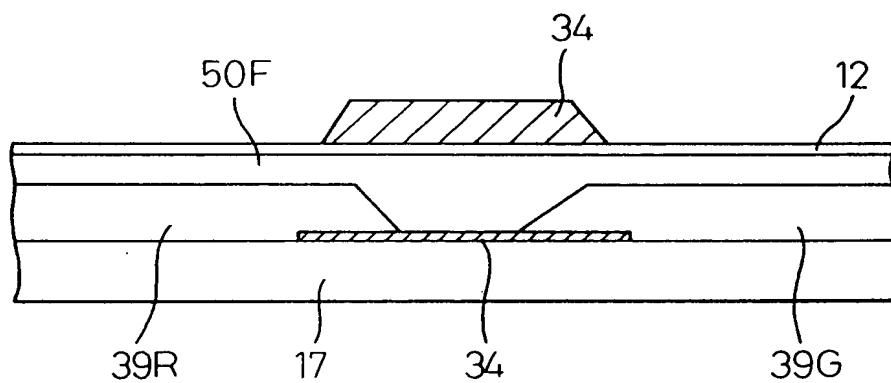


Fig.181A

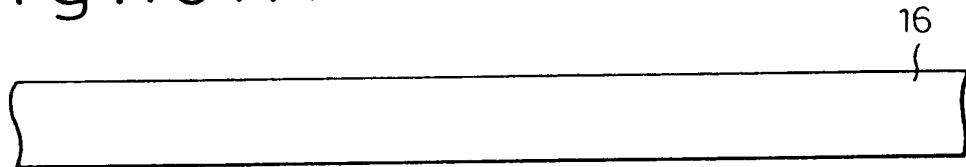


Fig.181B

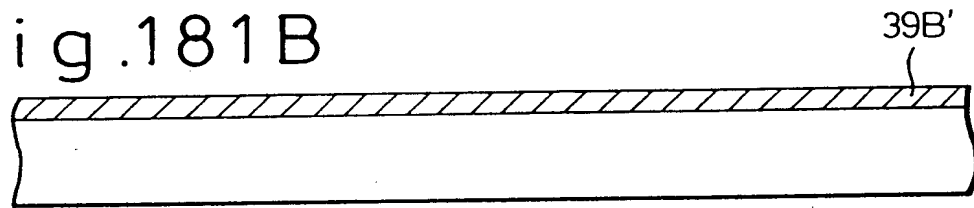


Fig.181C

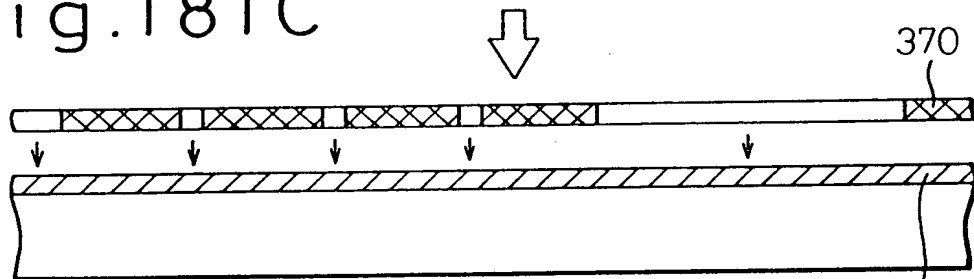
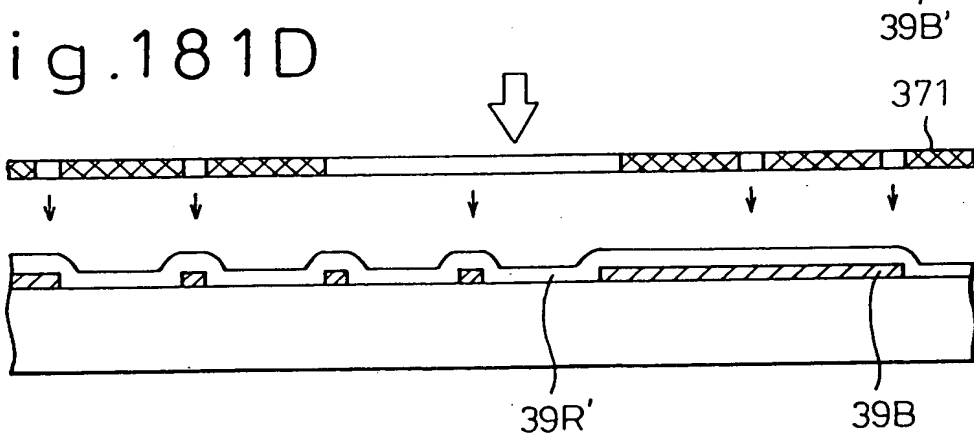


Fig.181D



177/246

Fig.181E

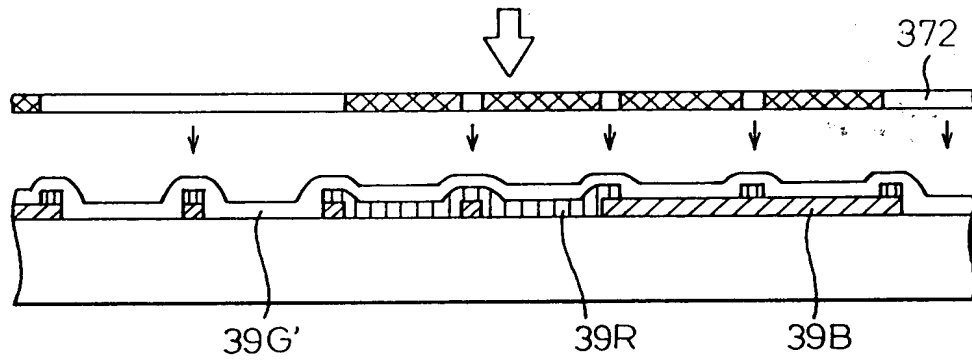


Fig.181F

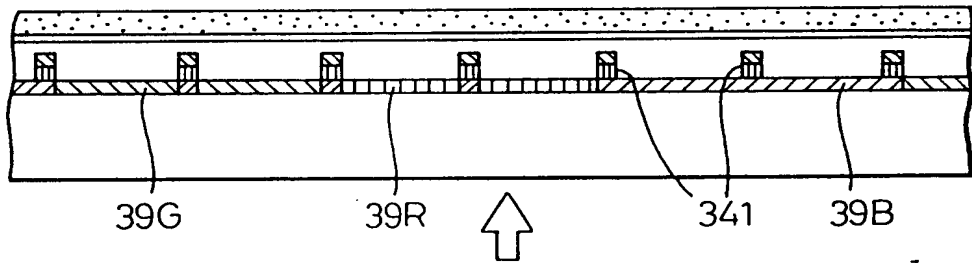
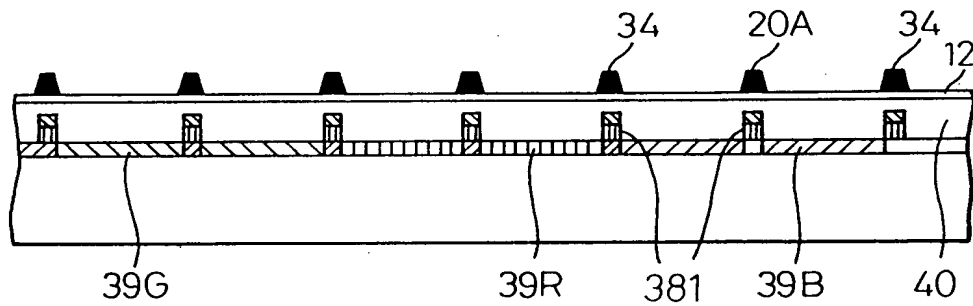


Fig.181G



178/
246

Fig. 182

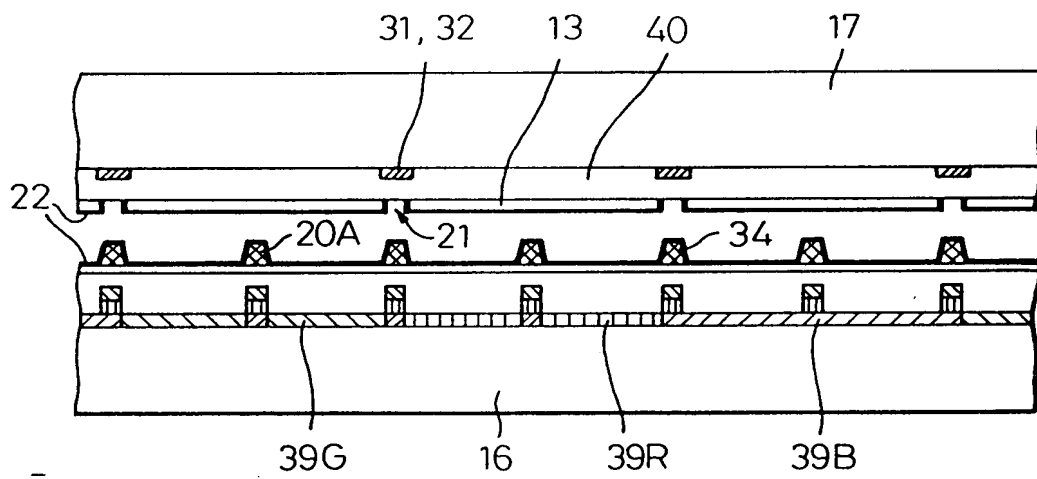


Fig.183A

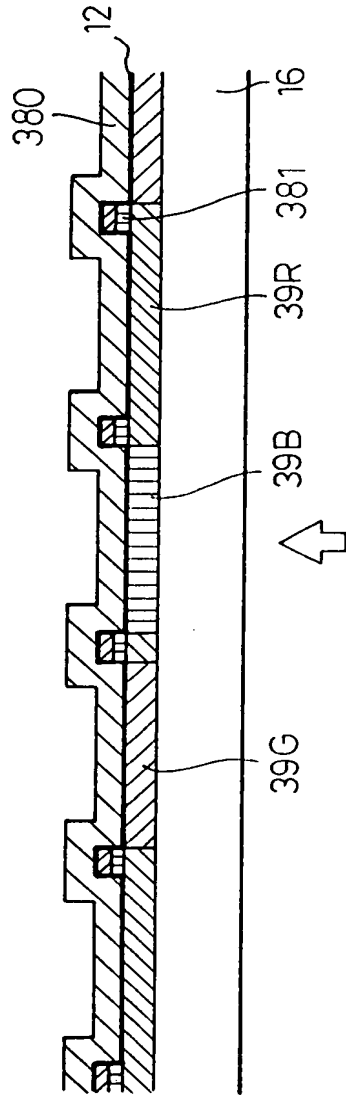
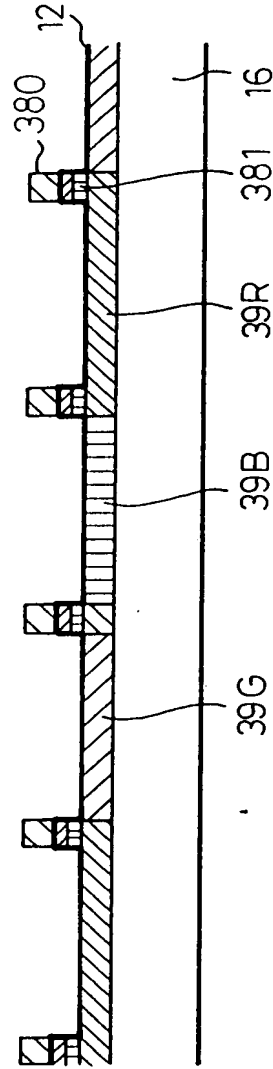


Fig.183B



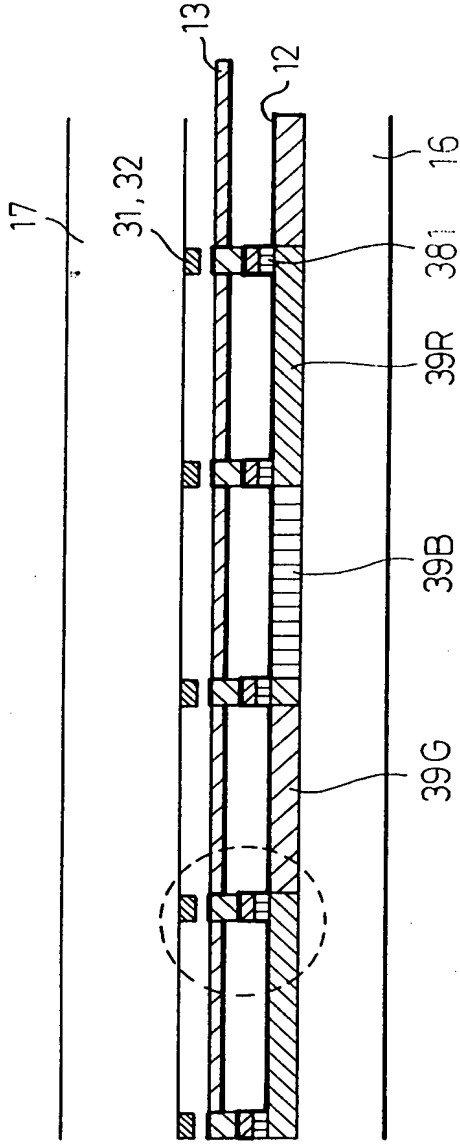


Fig. 184A

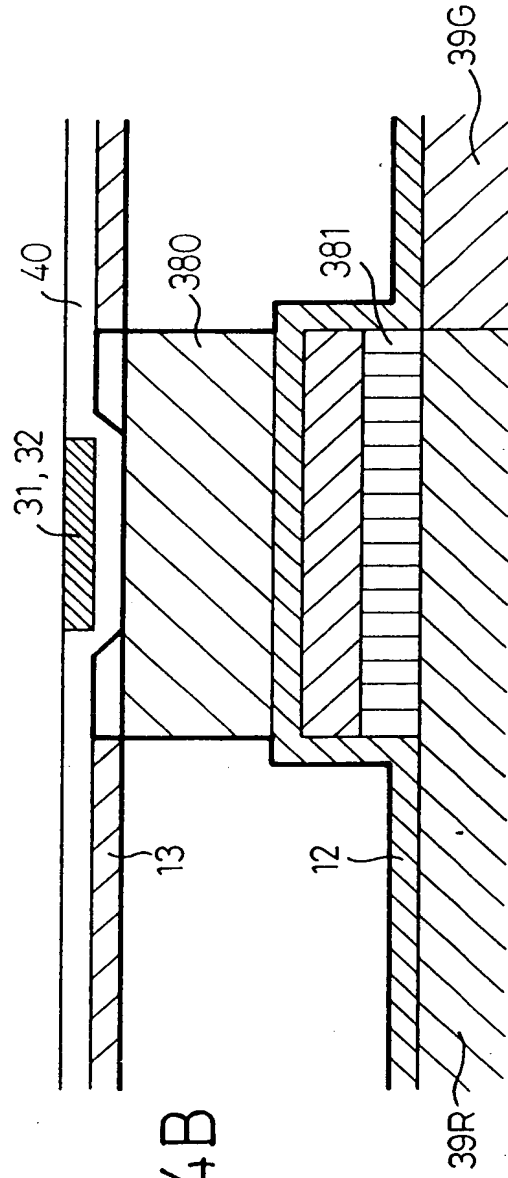


Fig. 184B

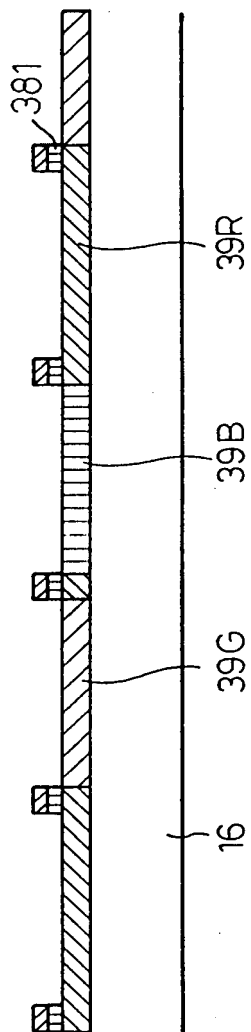


Fig. 185A

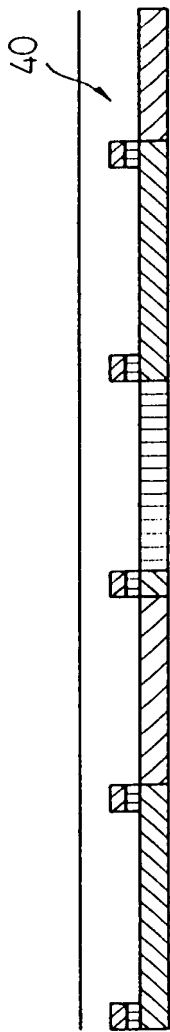


Fig. 185B

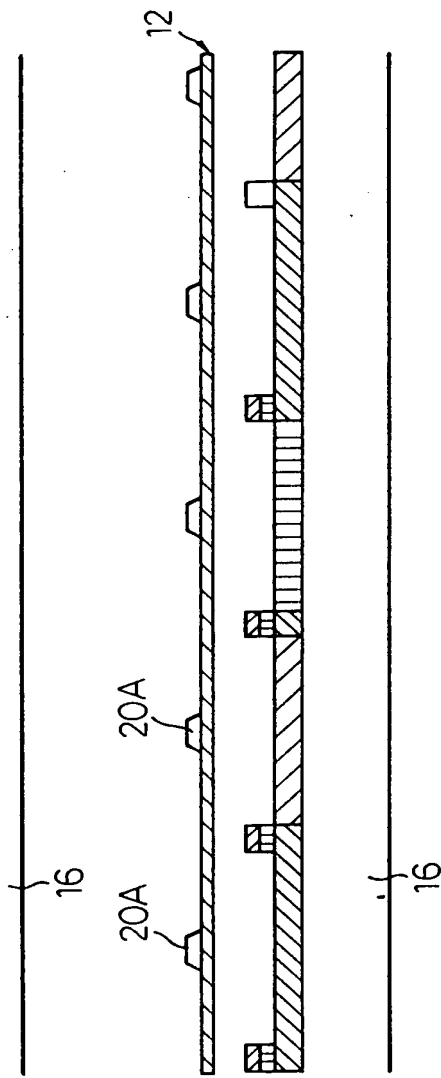
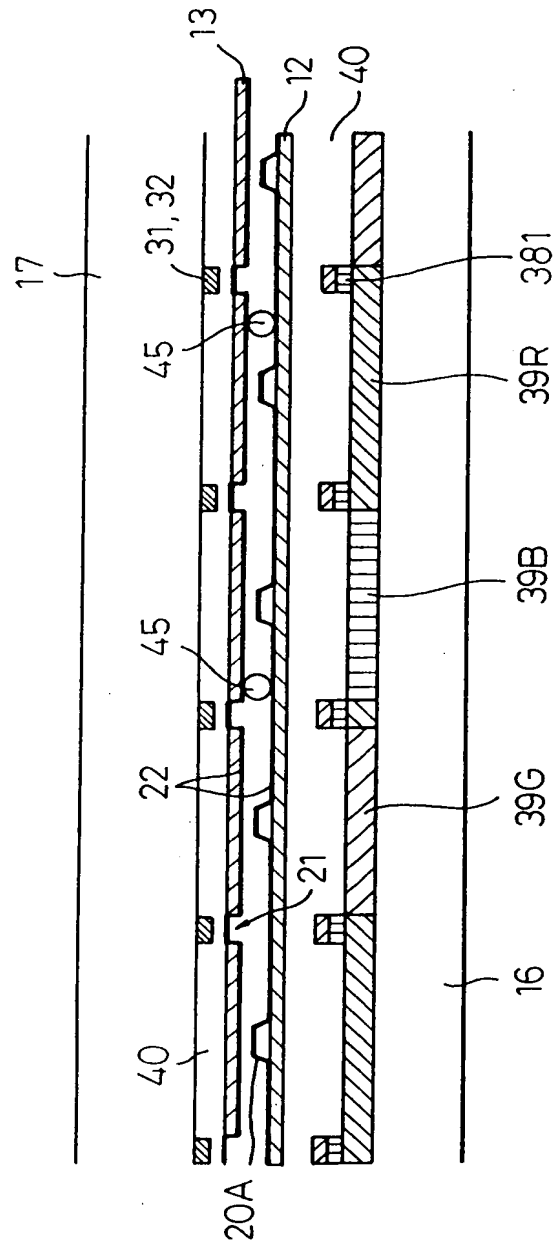


Fig. 185C

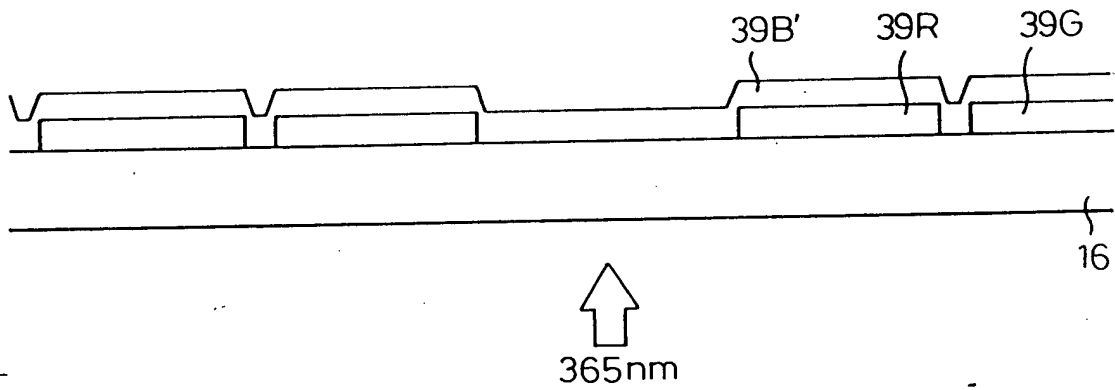
Fig. 186



182/246

183/246

Fig.187



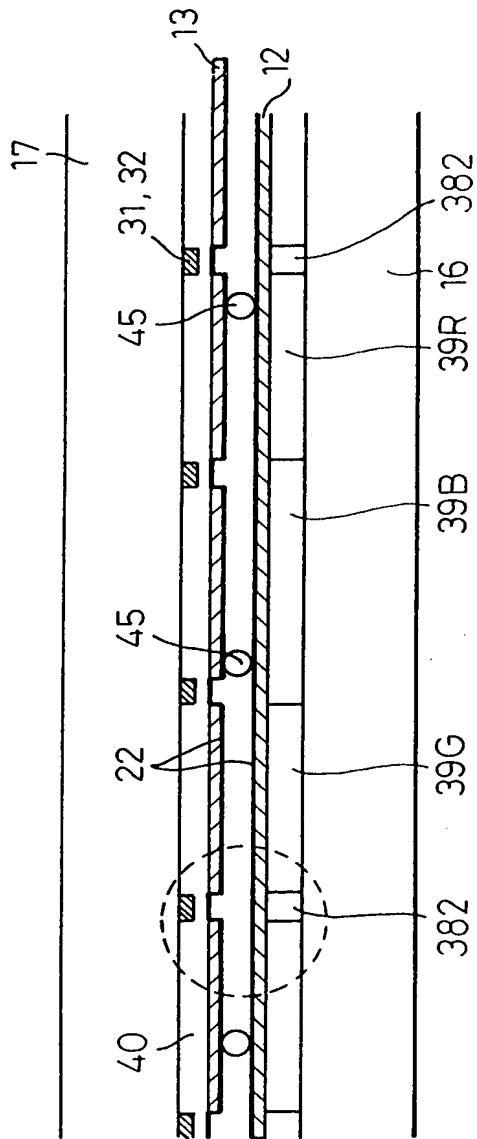


Fig. 188A

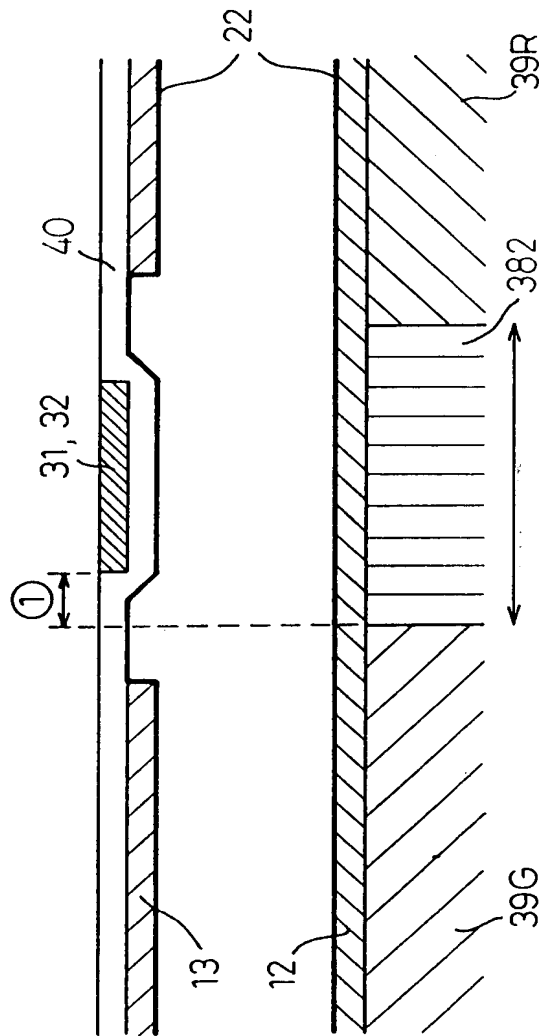


Fig. 188B

185/
246

Fig.189

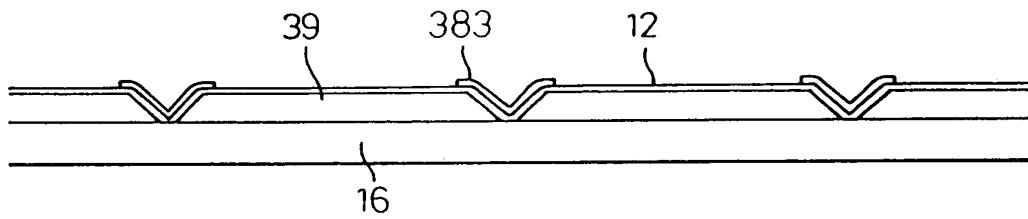


Fig.190A

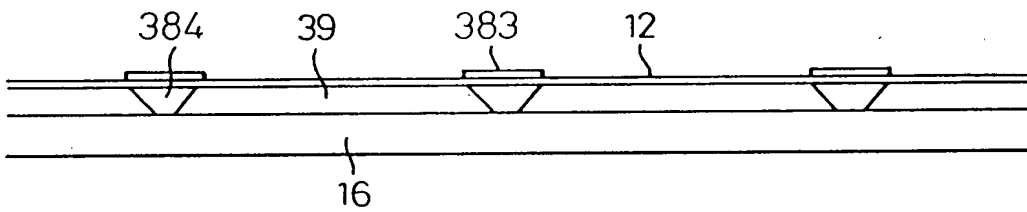
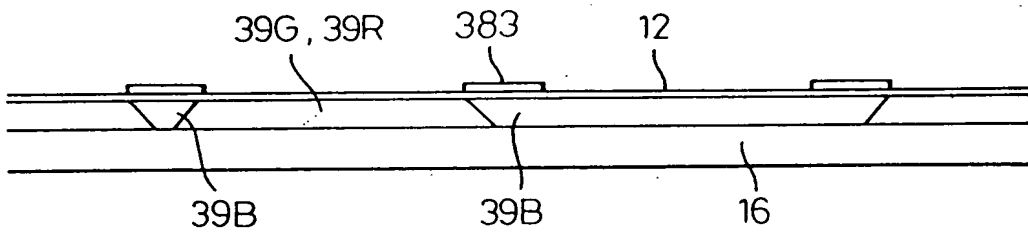


Fig.190B



186/246

Fig.191

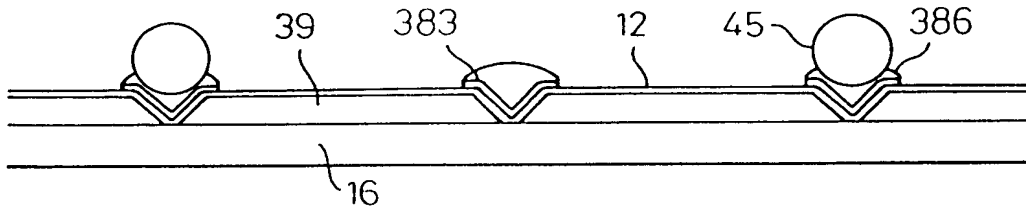


Fig.192

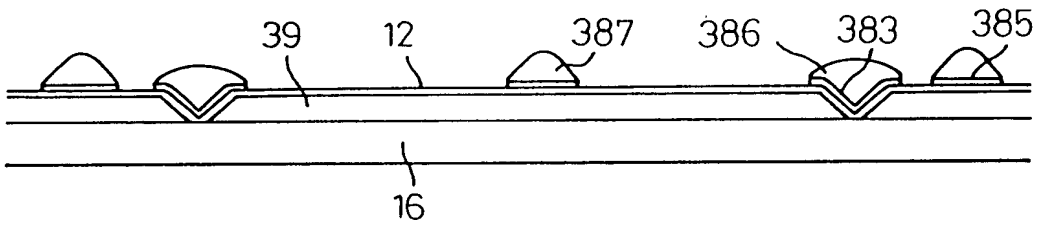
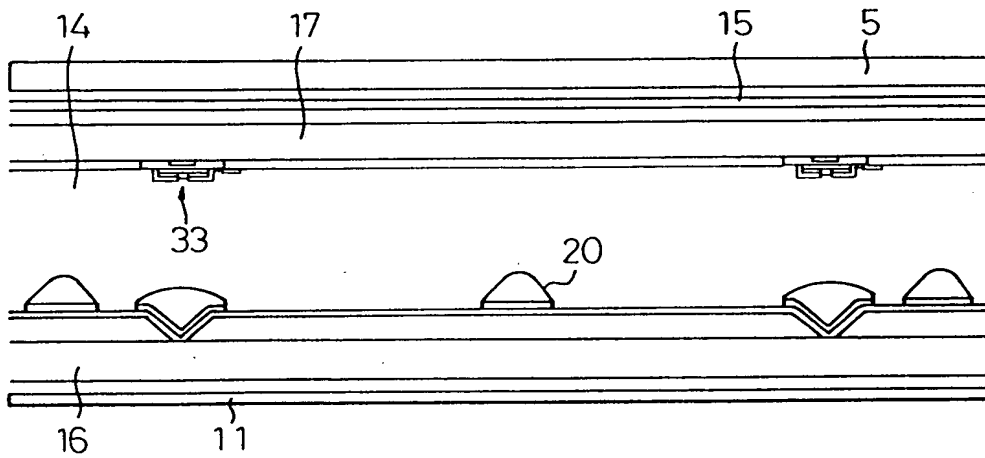


Fig.193



187/
246

Fig. 194

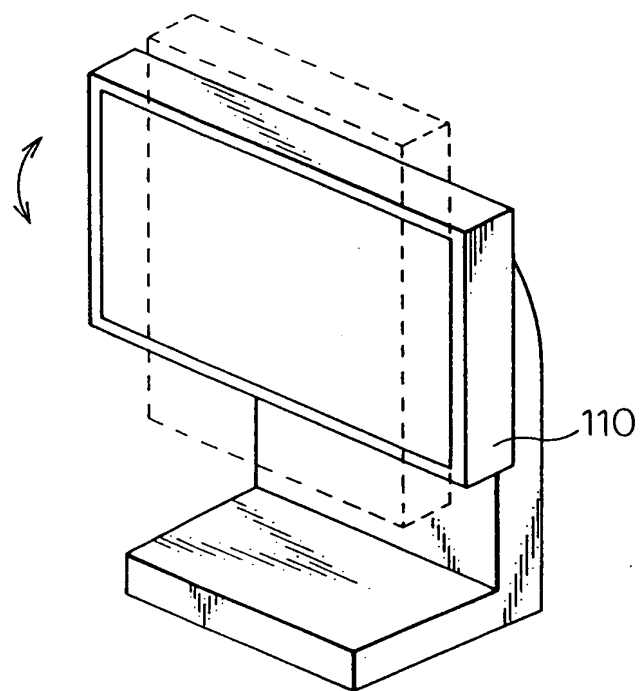
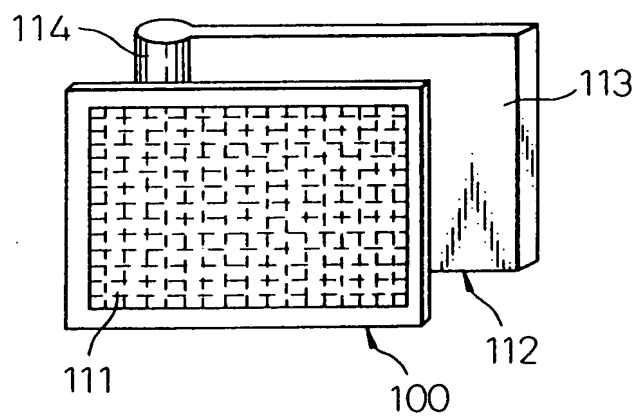


Fig. 195



ROTATION
→

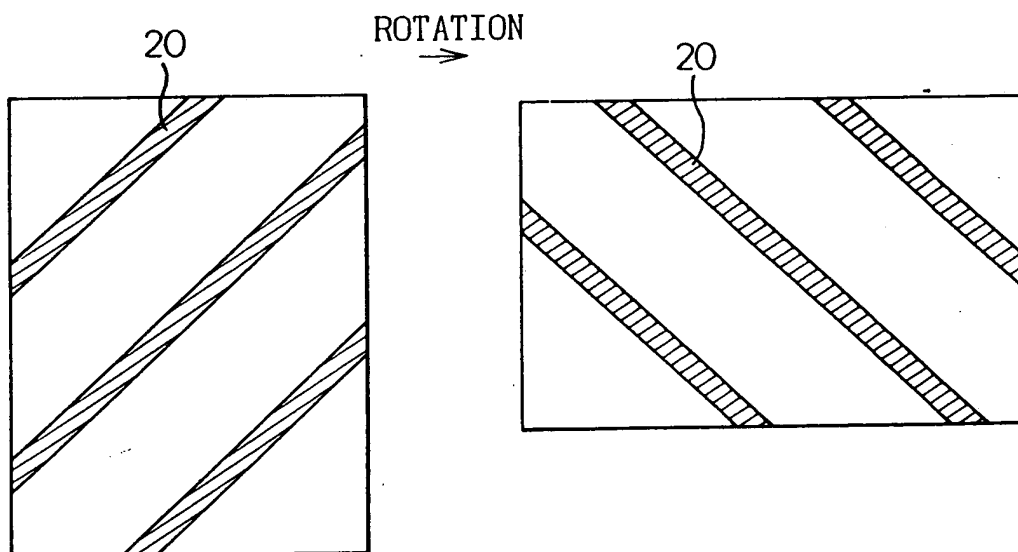
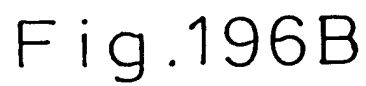
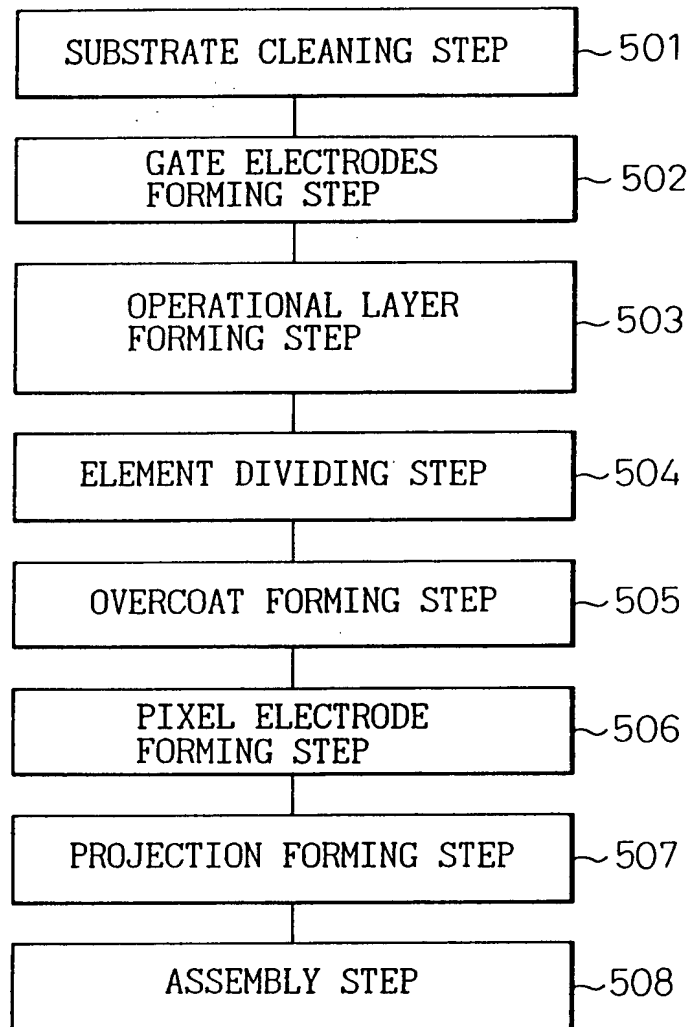


Fig.197



190/246

Fig.198

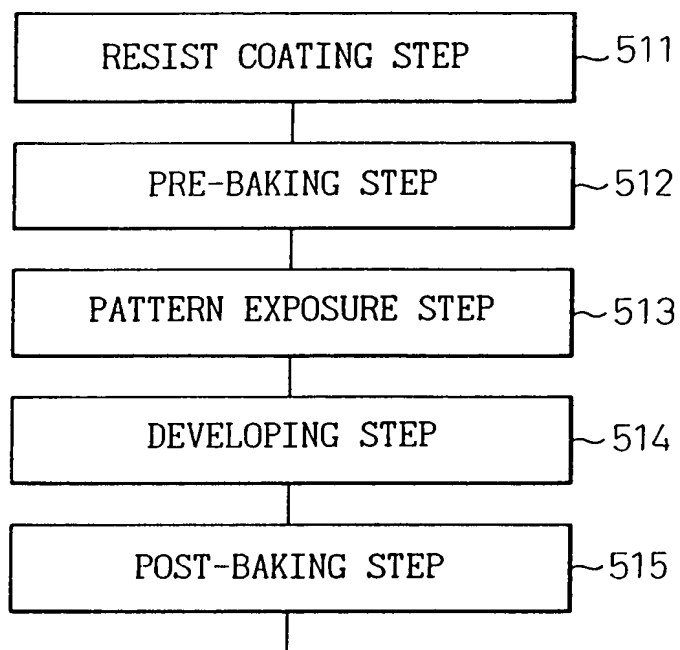


Fig.199

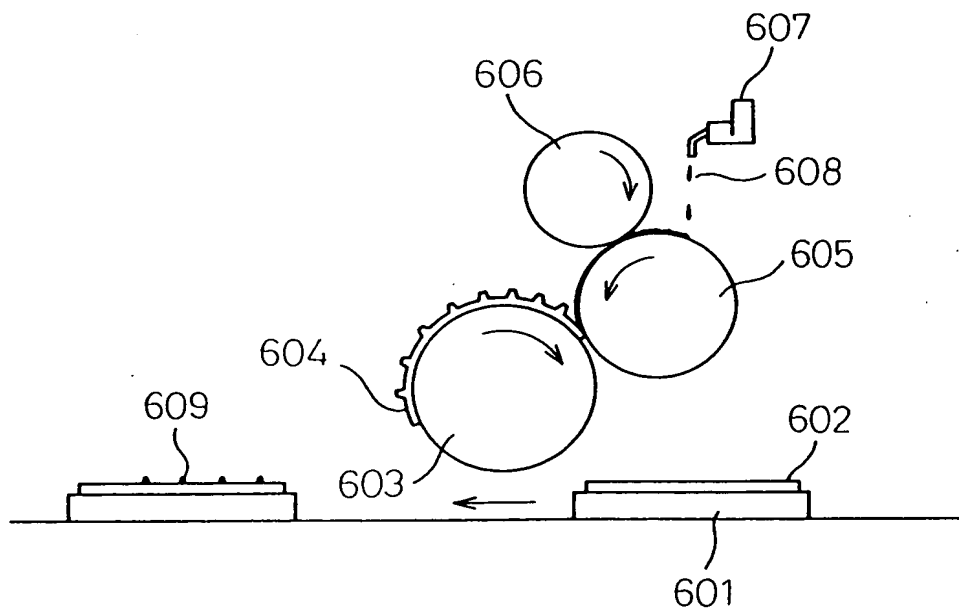


Fig. 200

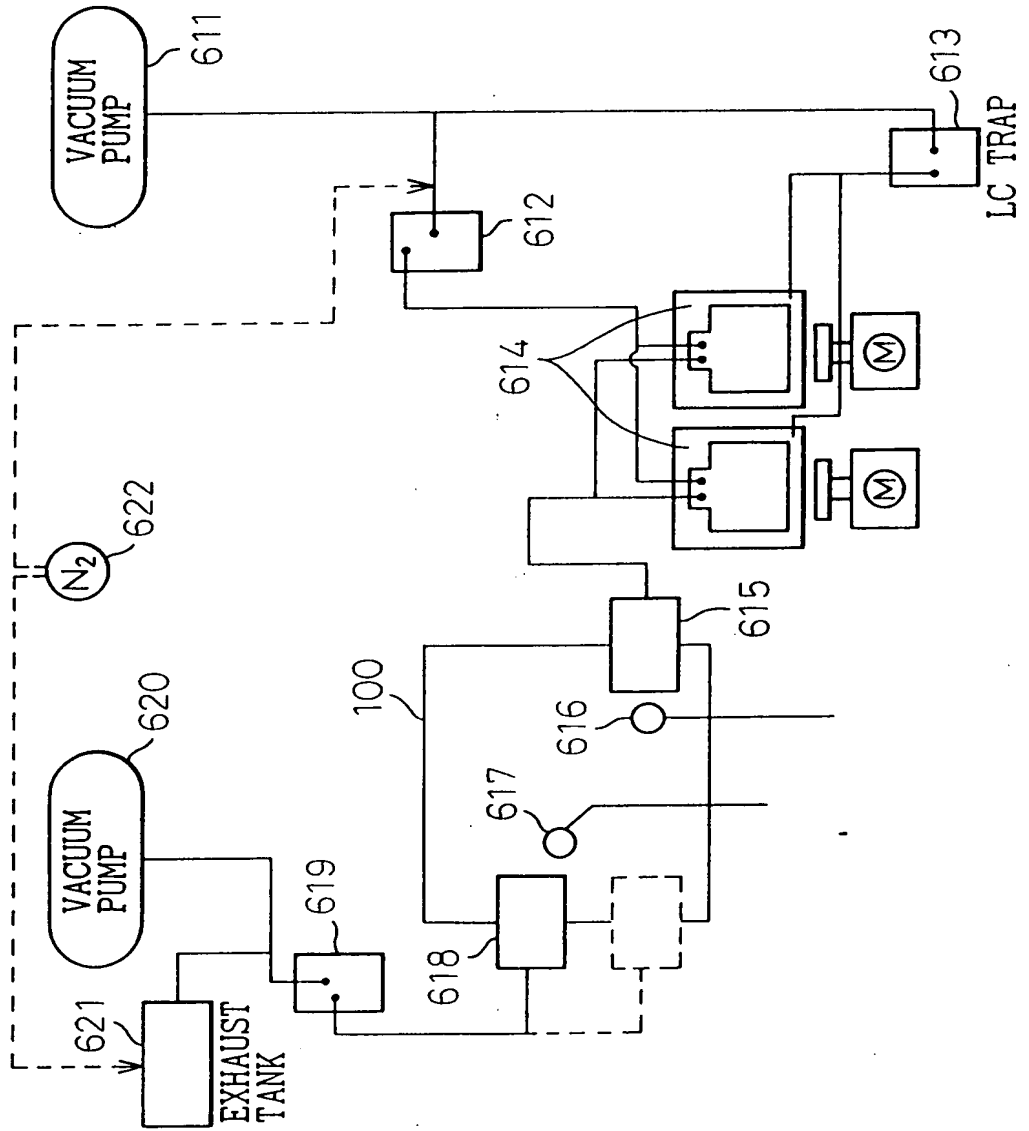


Fig. 201A

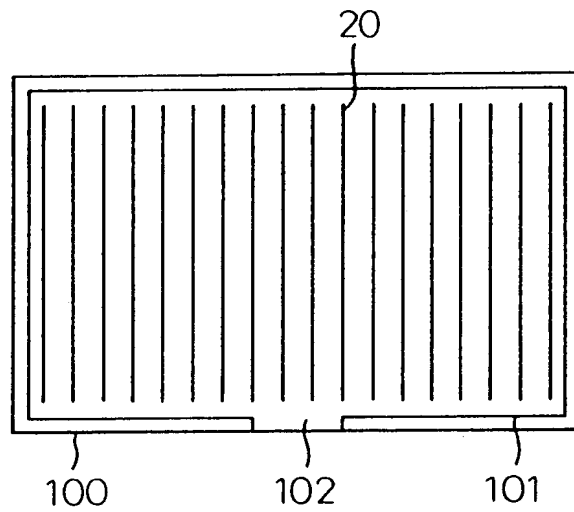


Fig. 201B

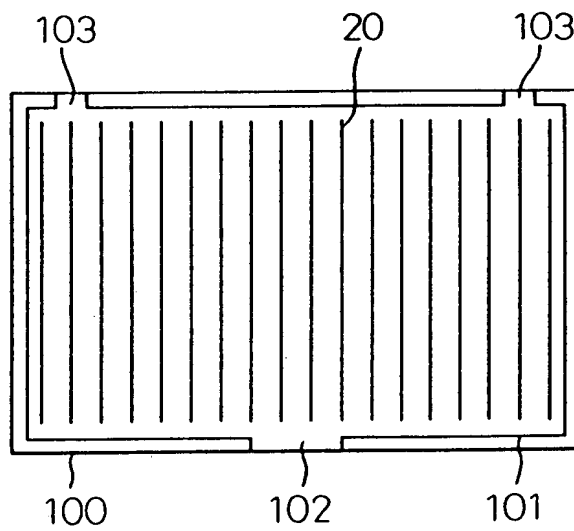


Fig. 202A

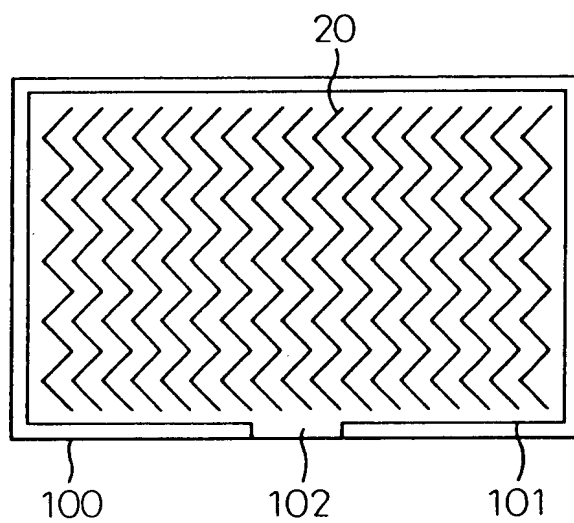


Fig. 202B

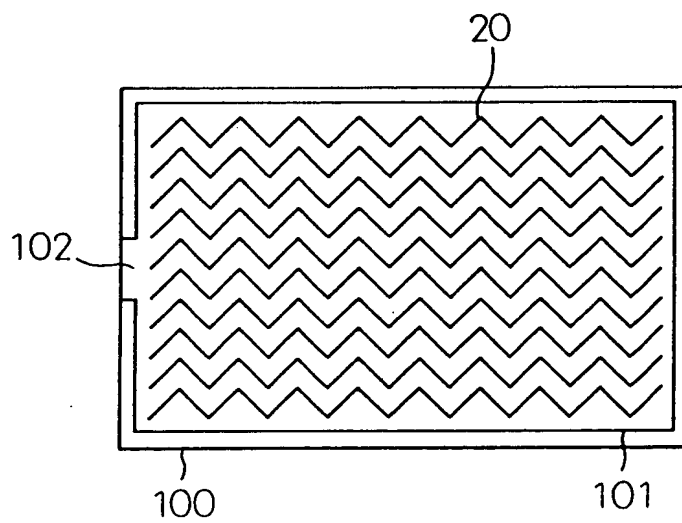


Fig. 203A

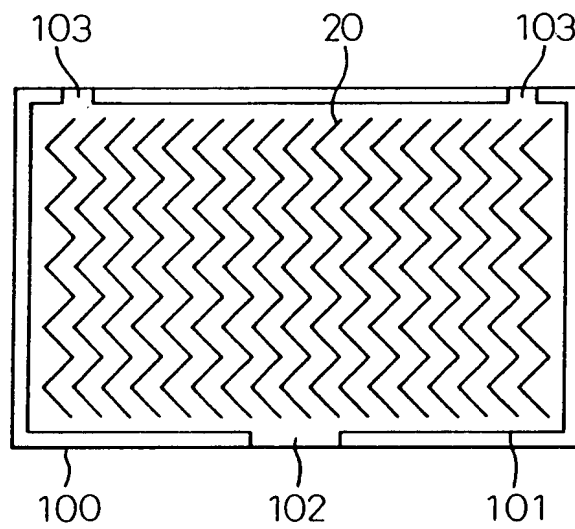
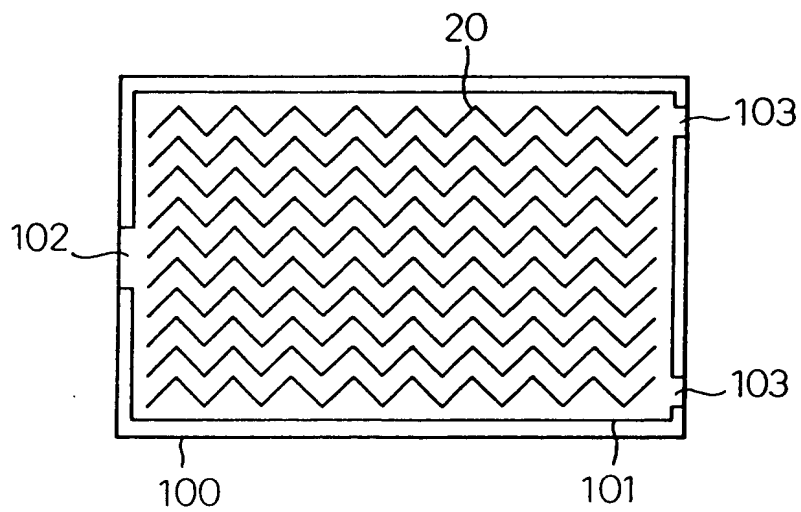


Fig. 203B



195/246

Fig. 204

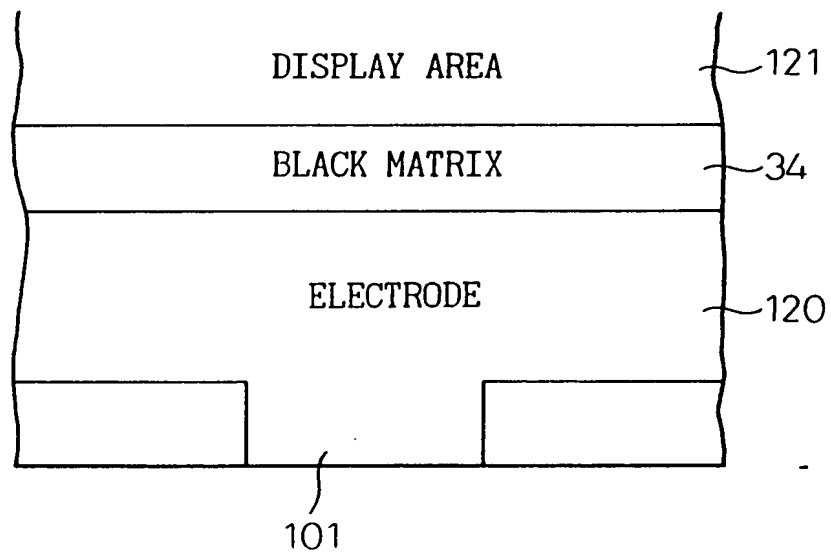


Fig. 205A

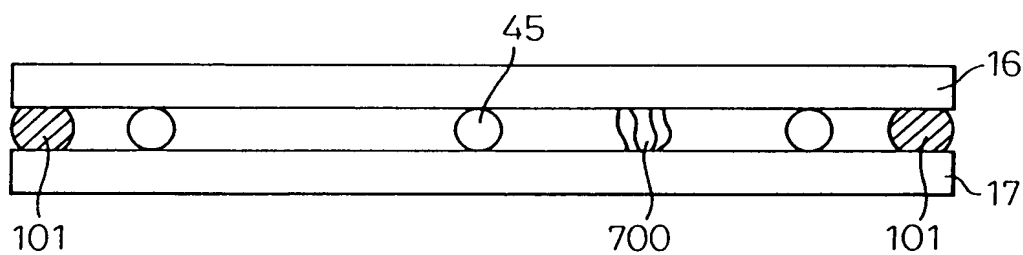


Fig. 205B

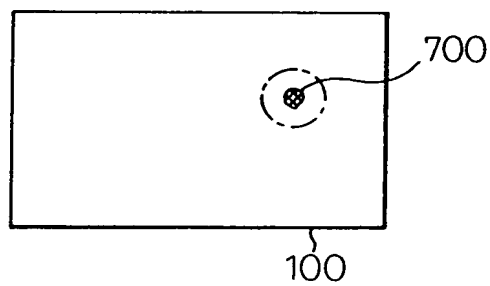
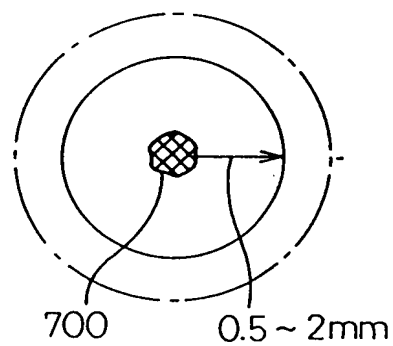


Fig. 205C



197/246

Fig. 206

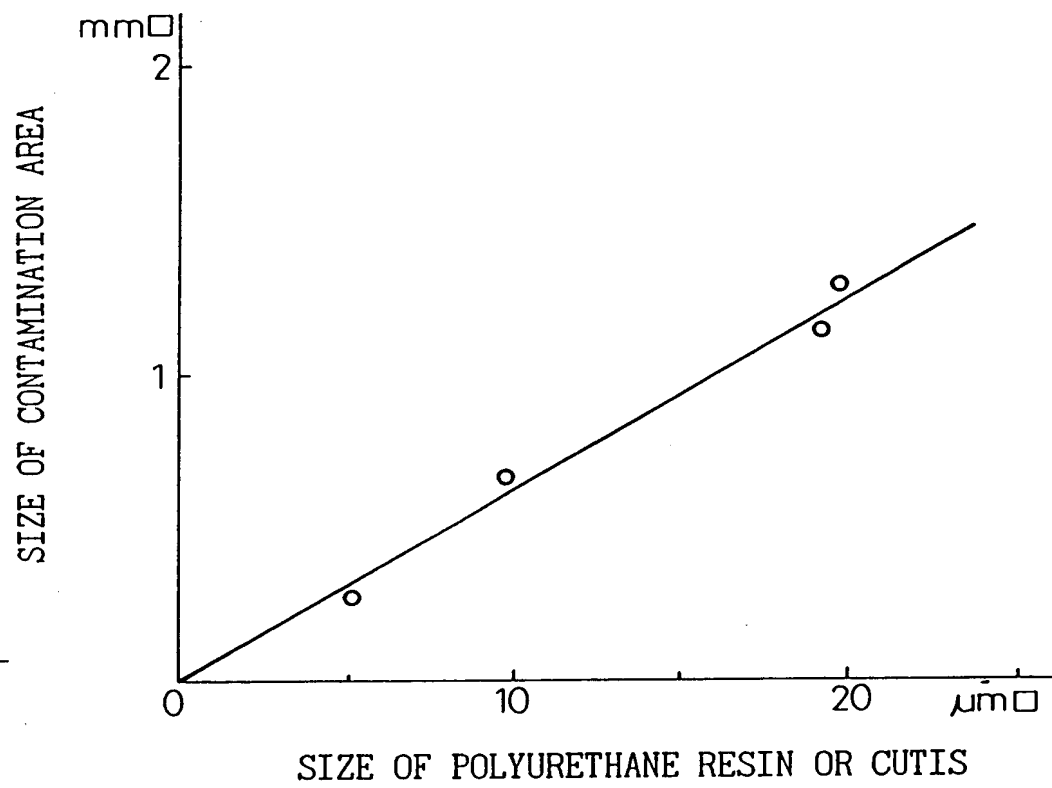


Fig. 207

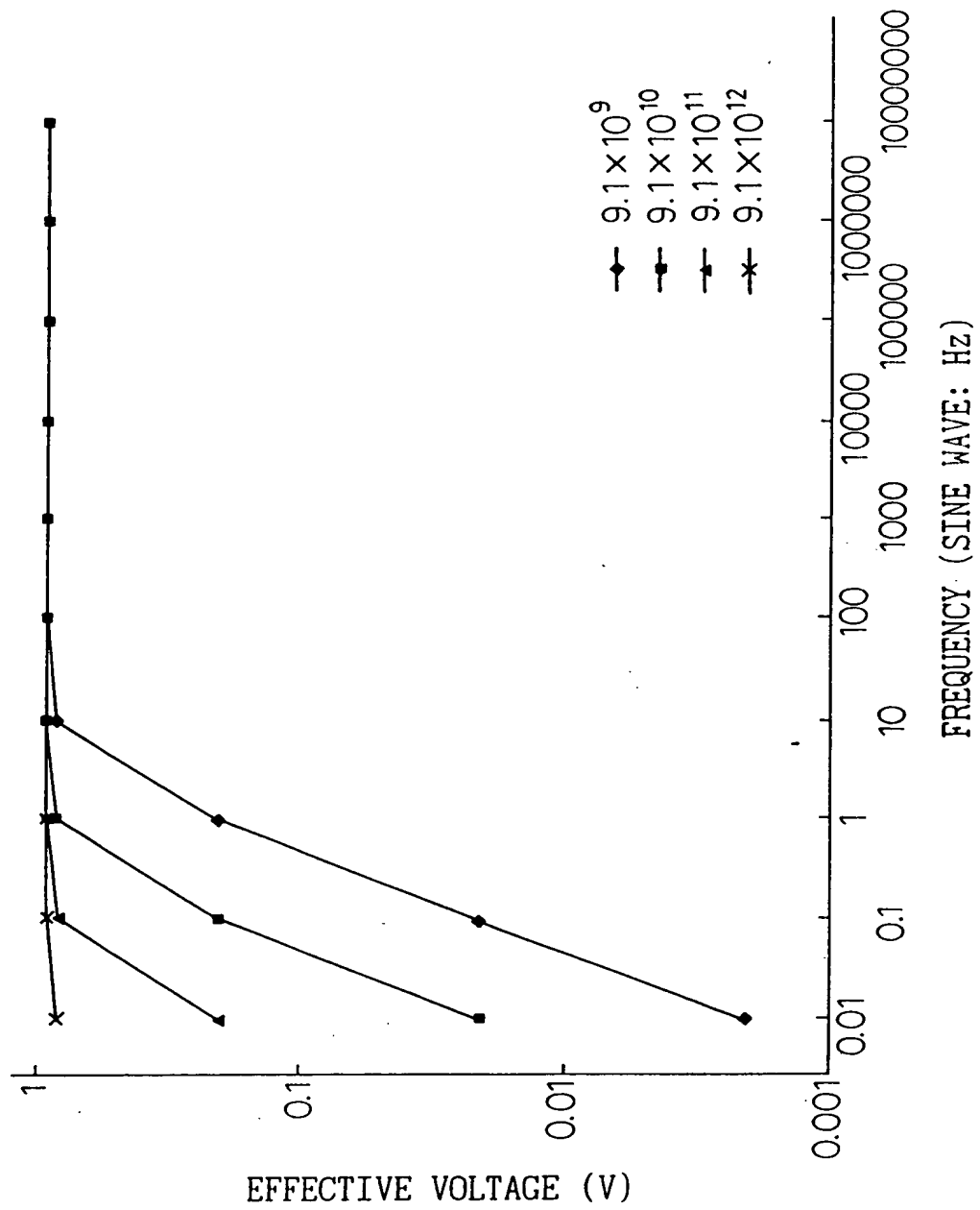


Fig. 208

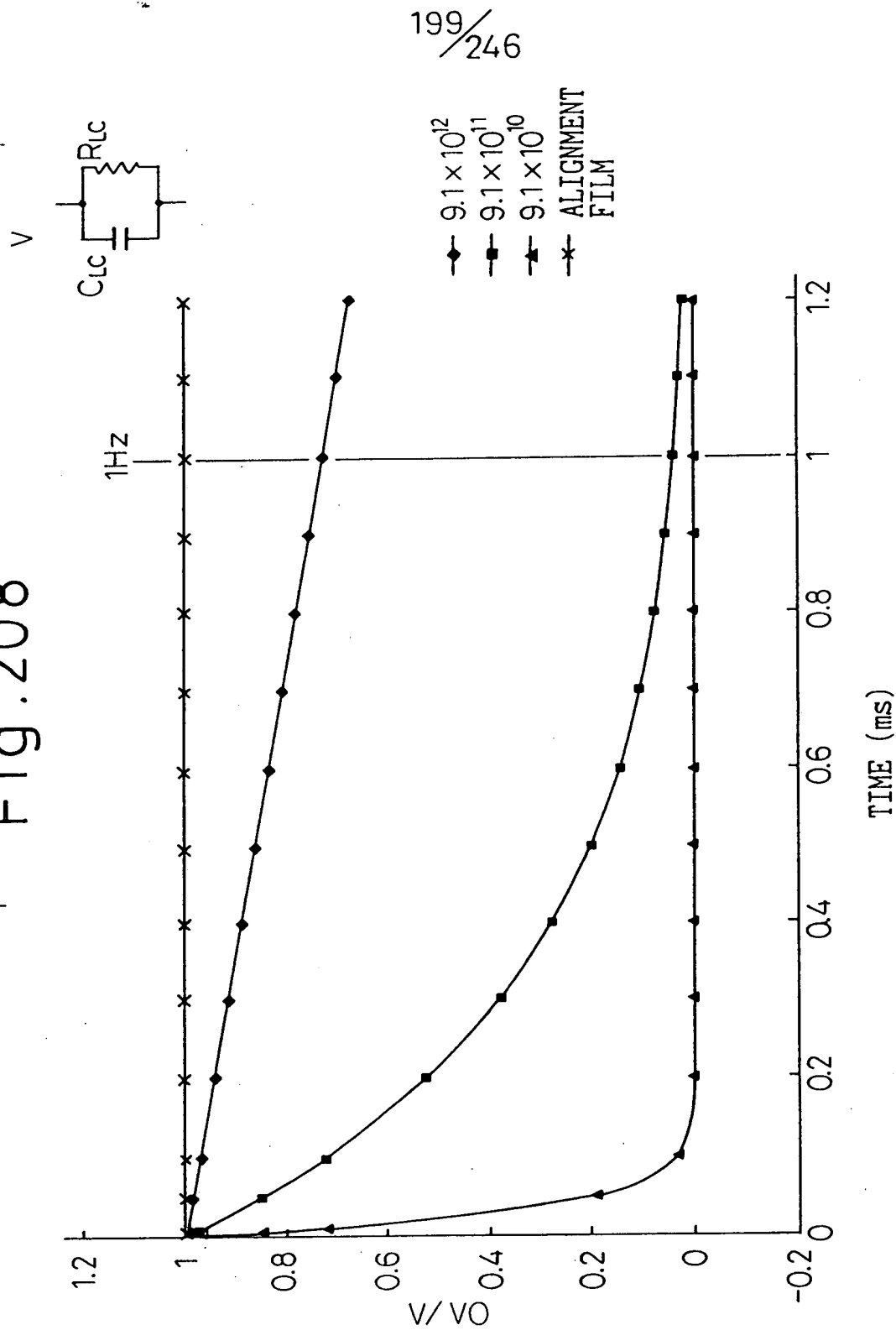
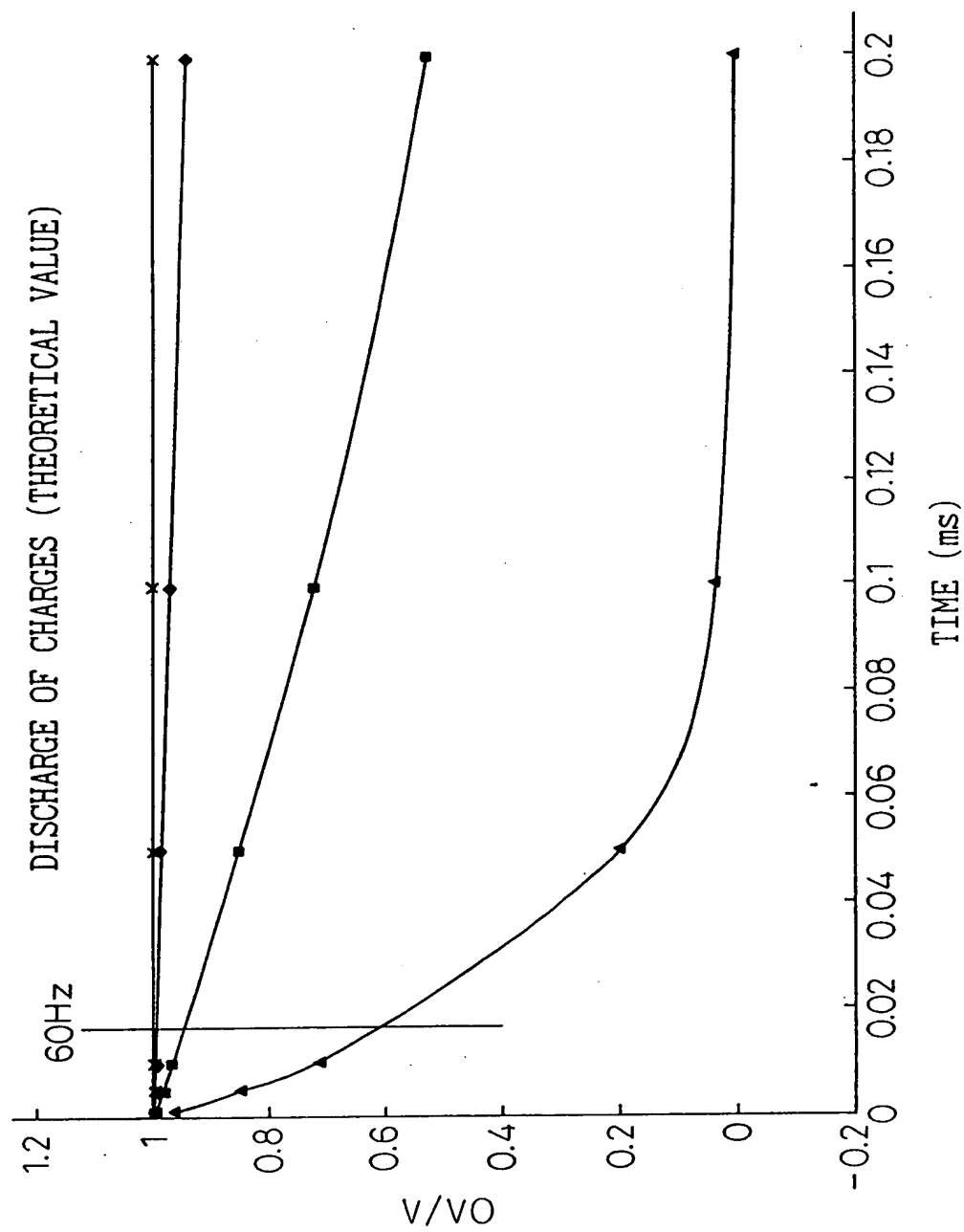
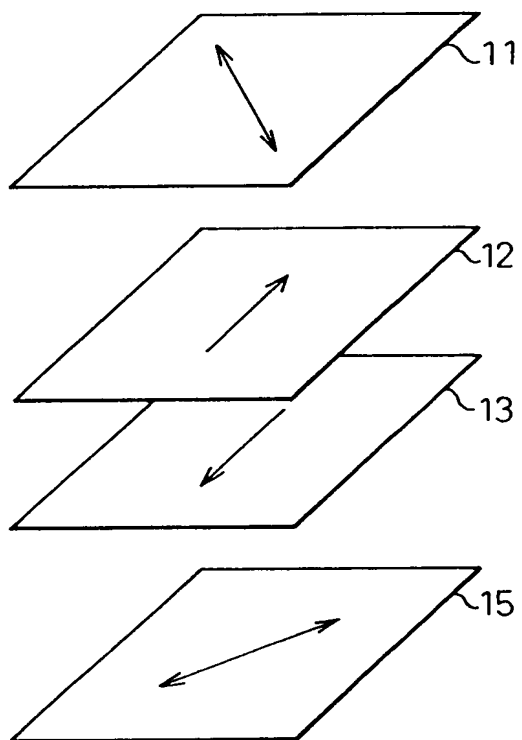


Fig. 209

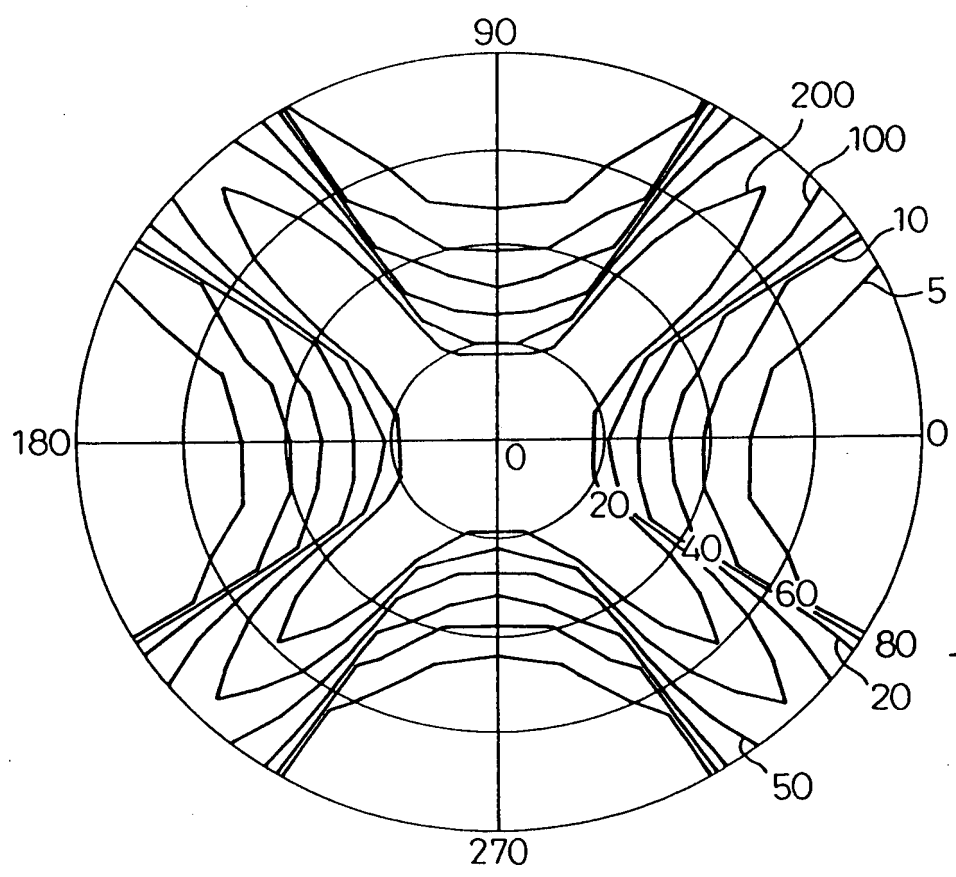


200/246

[illegible]

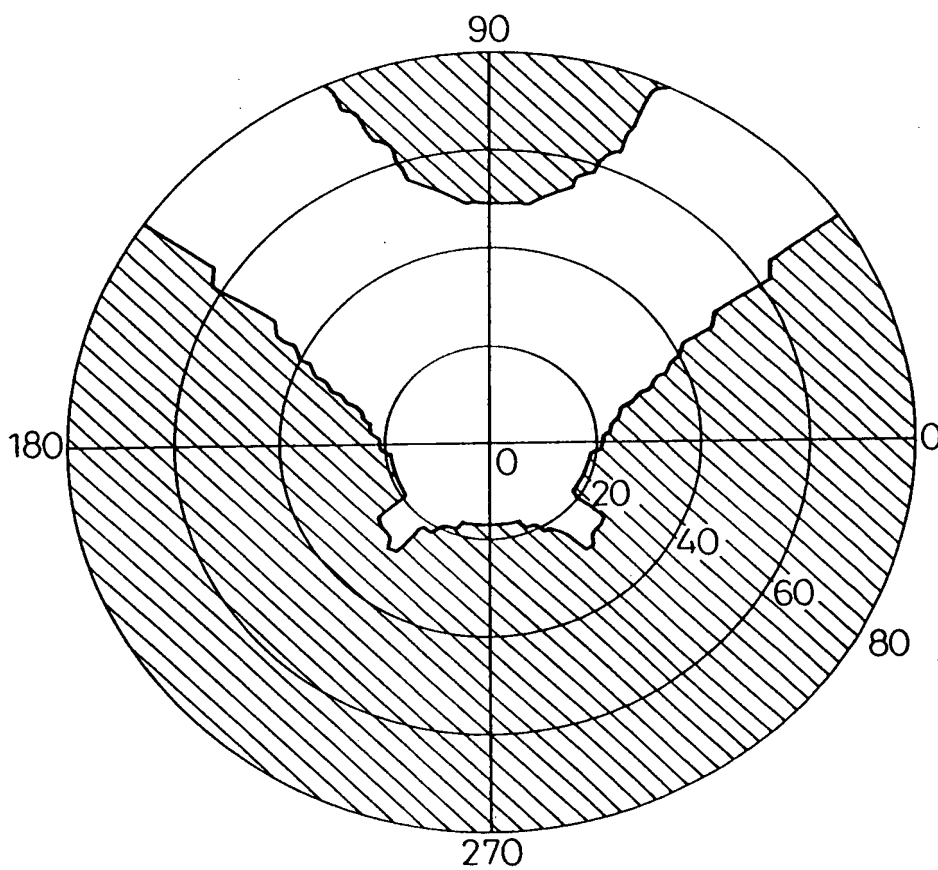
202/246

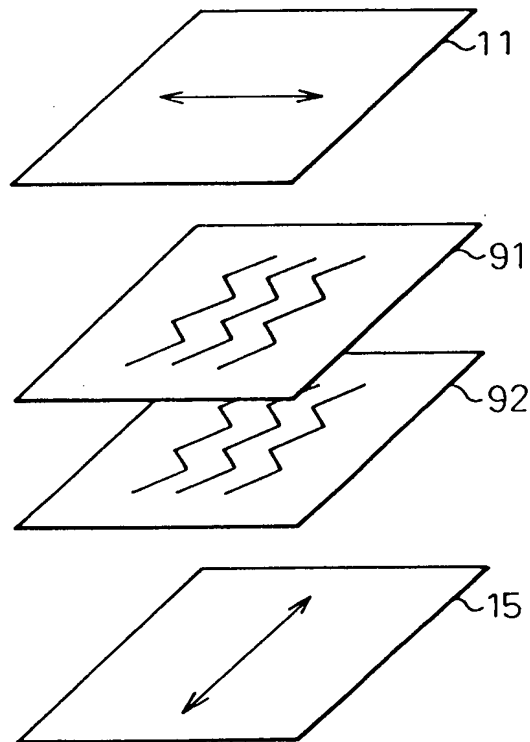
Fig. 211



203/246

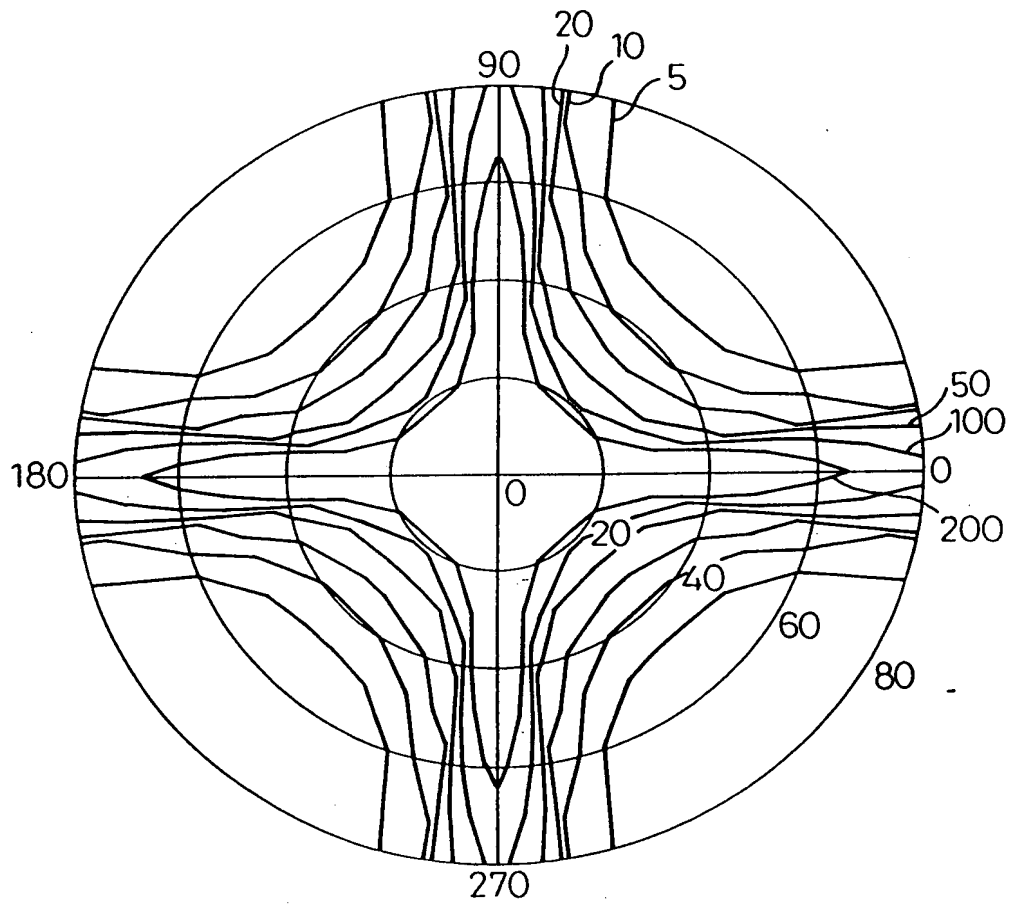
Fig. 212



[illegible]

205/
246

Fig. 214



206/246

Fig. 215

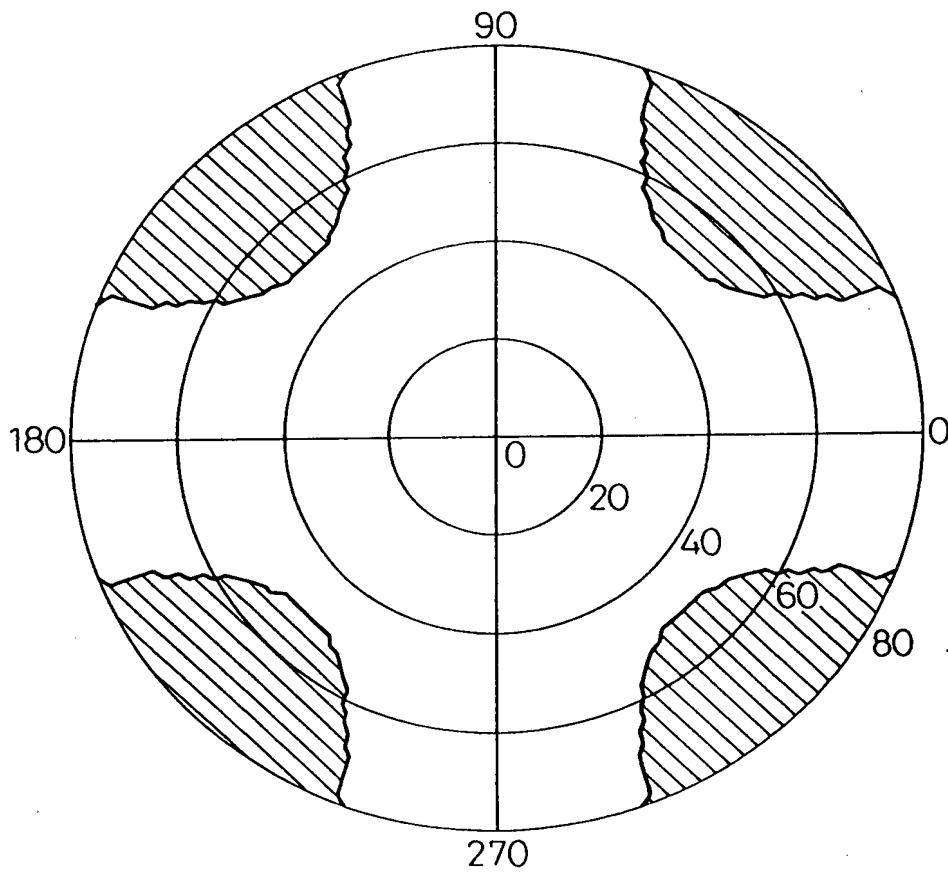
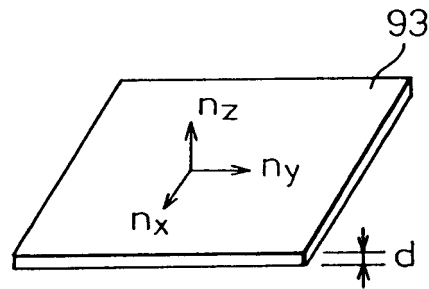


Fig.216



GENERAL CONDITION

$$n_x, n_y \geq n_z$$

POSITIVE UNIAXIAL FILM

$$n_x > n_y = n_z$$

NEGATIVE UNIAXIAL FILM

$$n_x = n_y > n_z$$

BIAXIAL FILM
(A PHASE LAG AXIS IS X DIRECTION.)

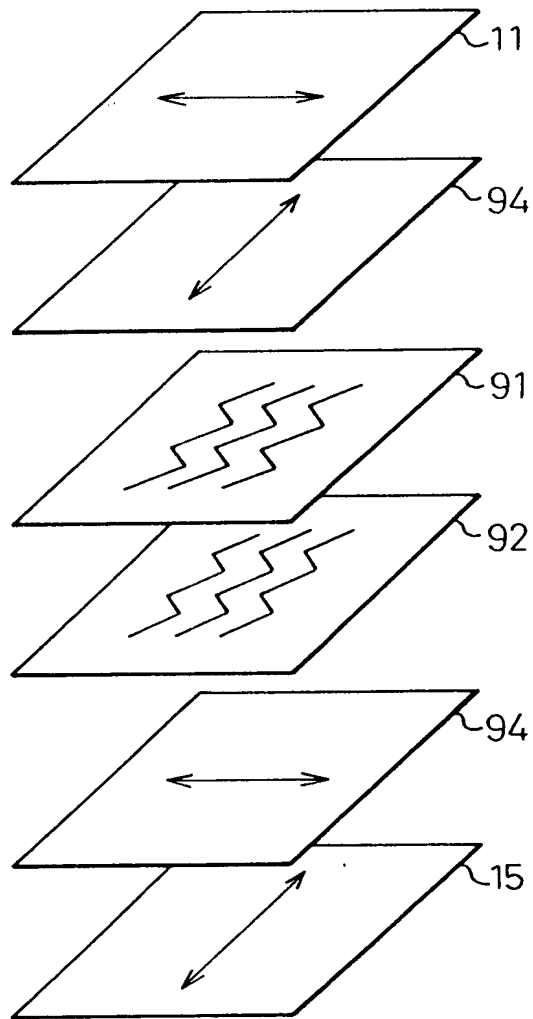
$$n_x > n_y > n_z$$

RETARDATION IN
INPLANE DIRECTIONS

$$R = (n_x - n_y)d$$

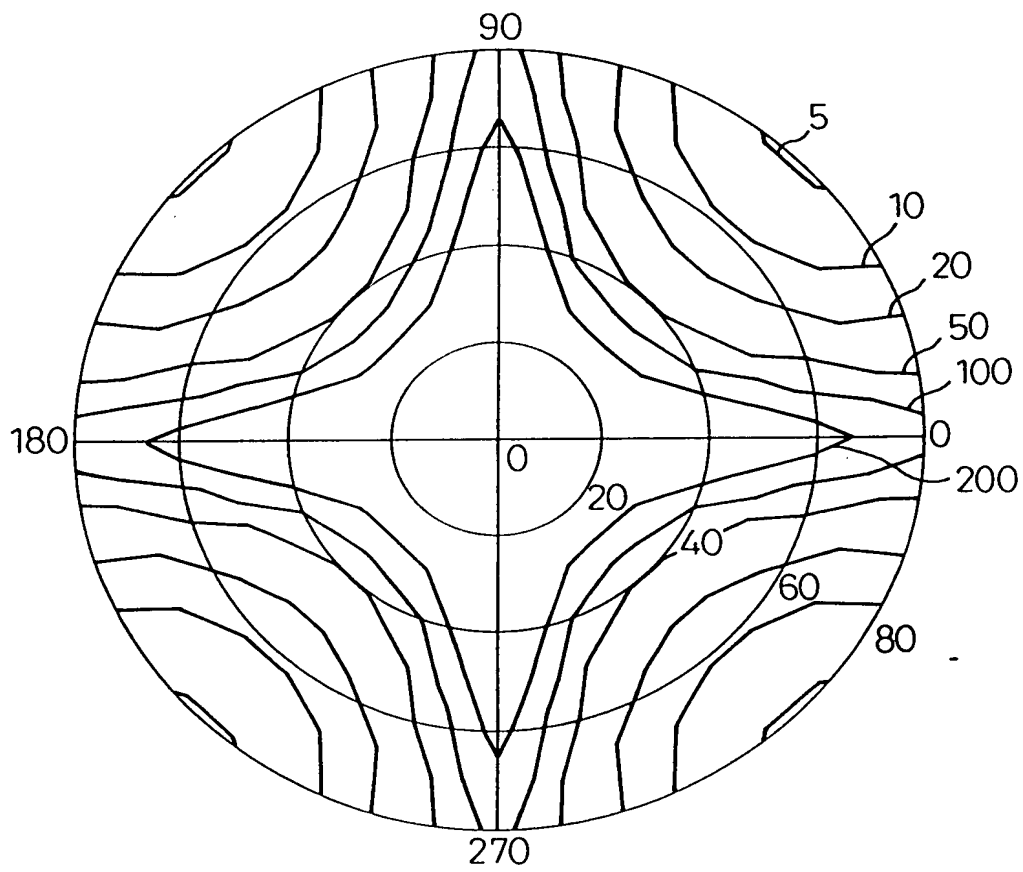
RETARDATION OF
THICKNESS DIRECTION

$$R = \left(\frac{n_x + n_y}{2} - n_z \right) d$$

[illegible]

209/246

Fig.218



210/246

Fig. 219

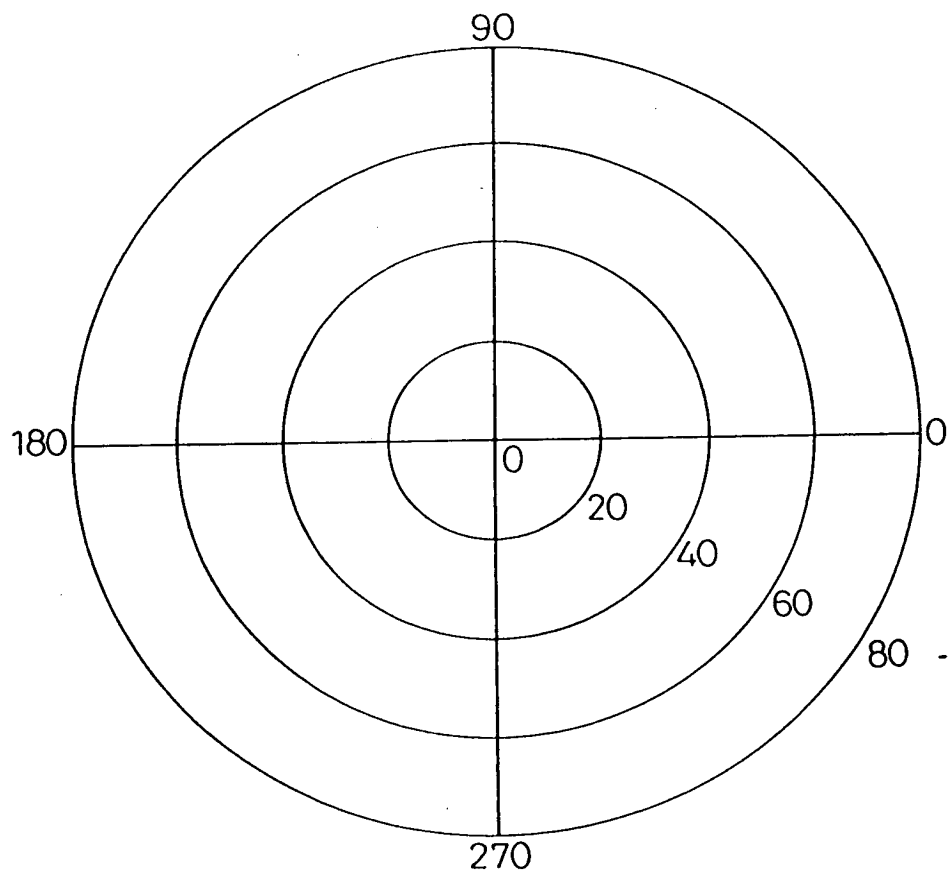
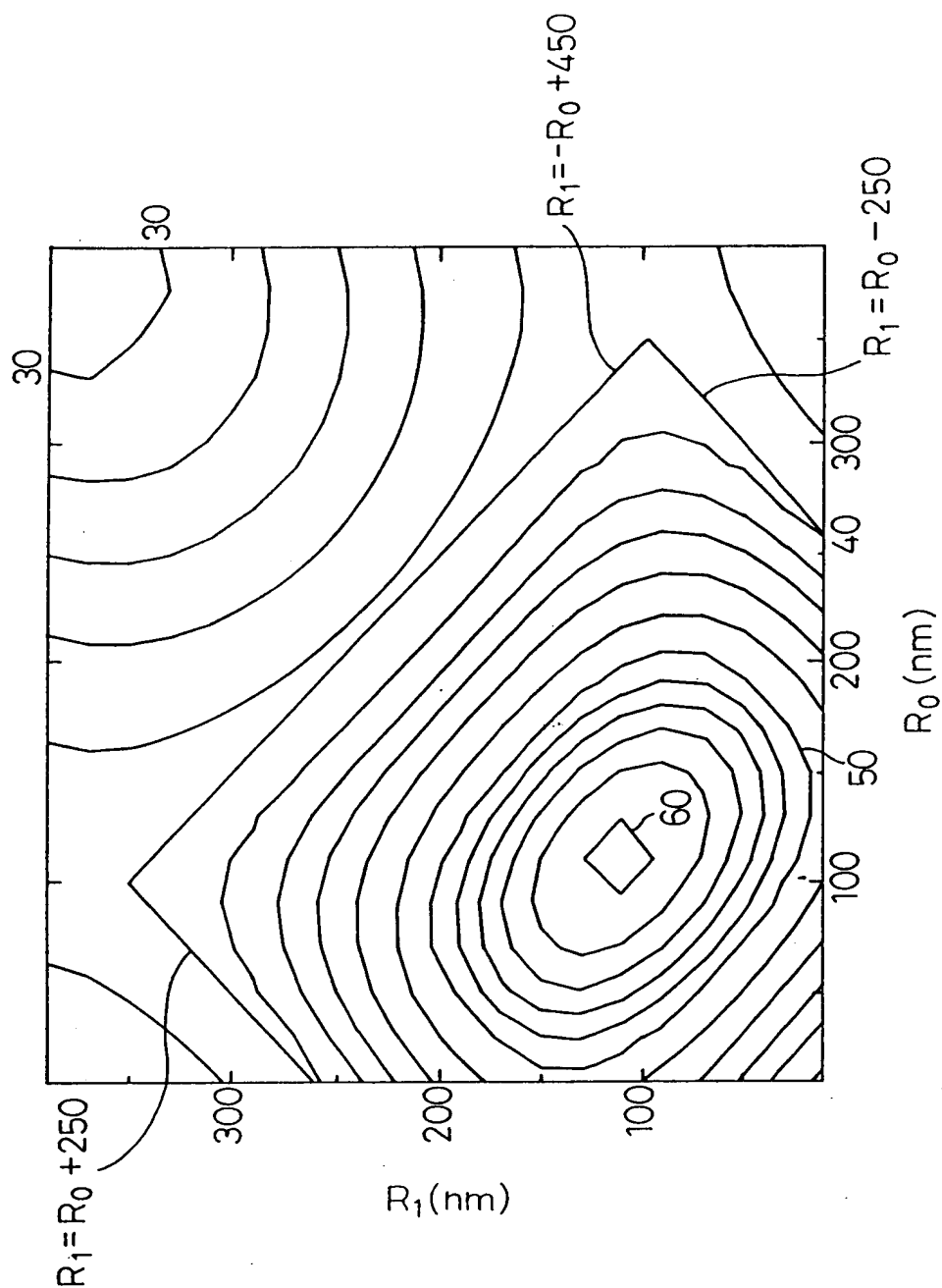


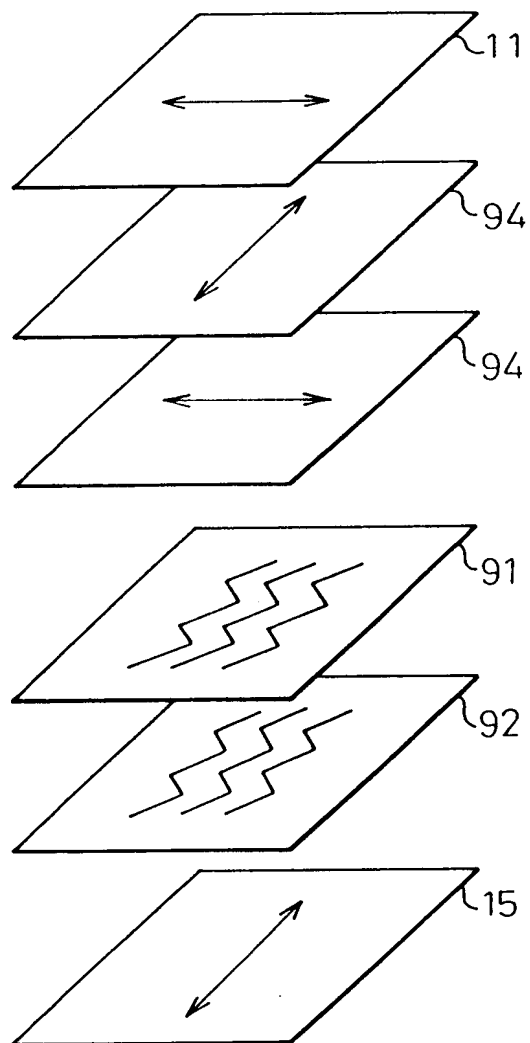
Fig. 220



$\frac{211}{246}$

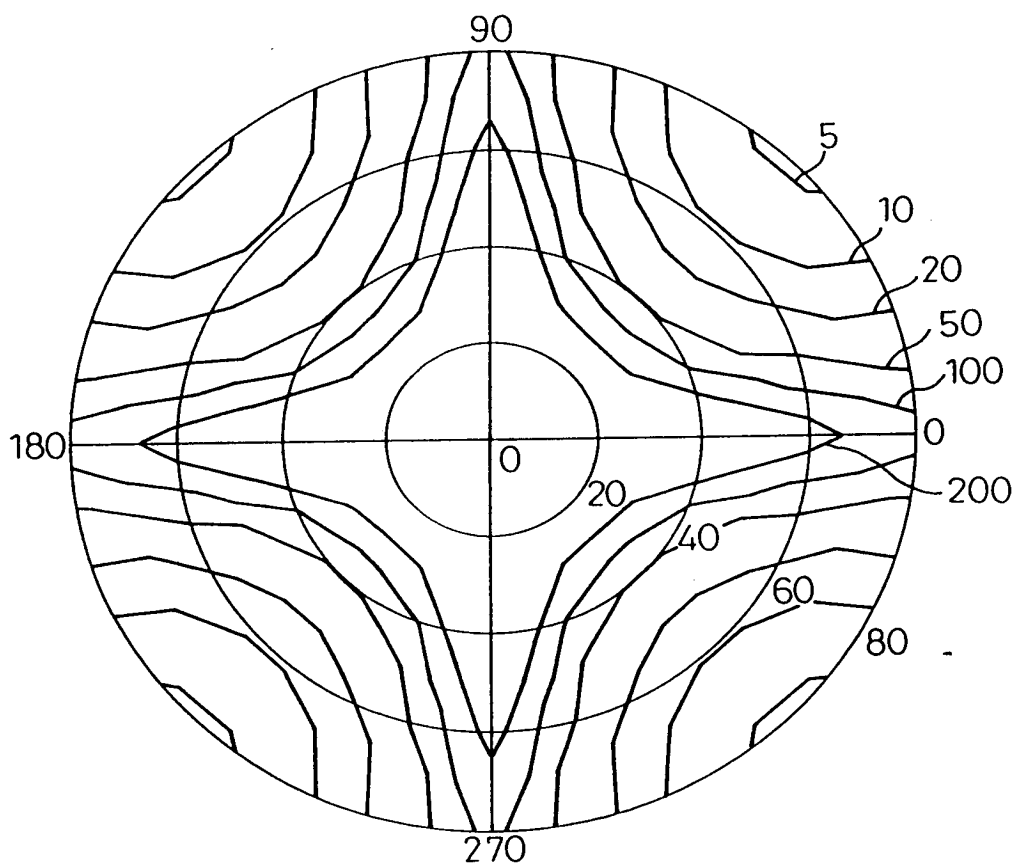
212/246

Fig. 221



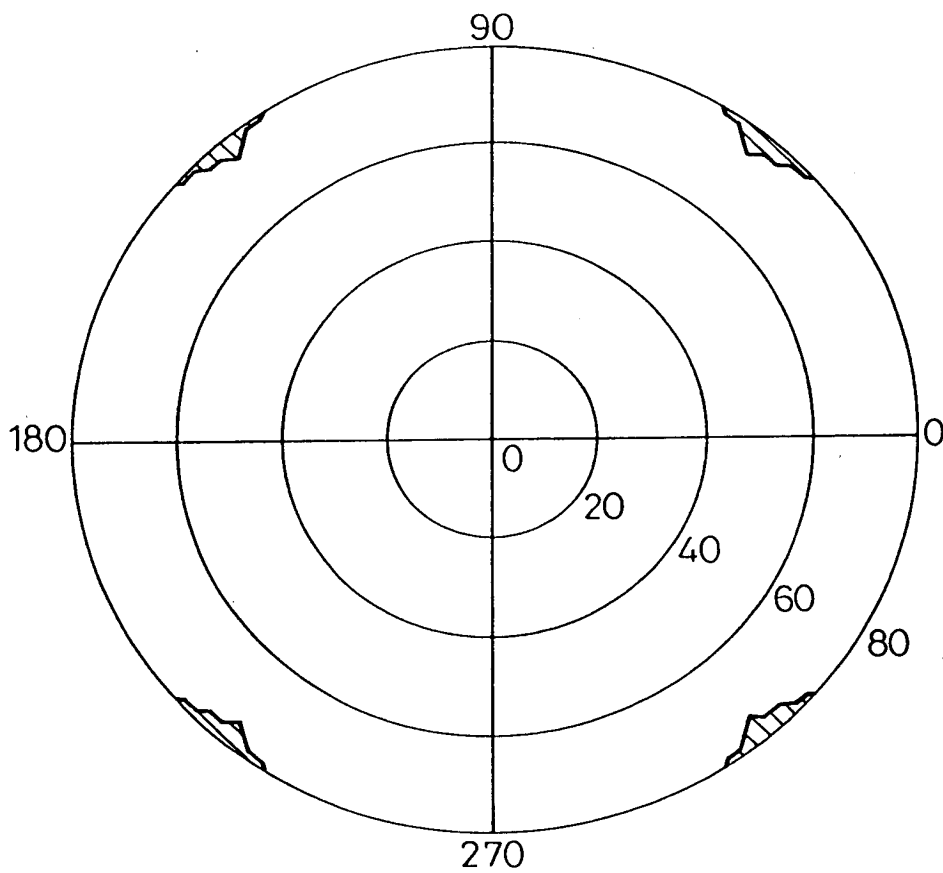
213/246

Fig. 222



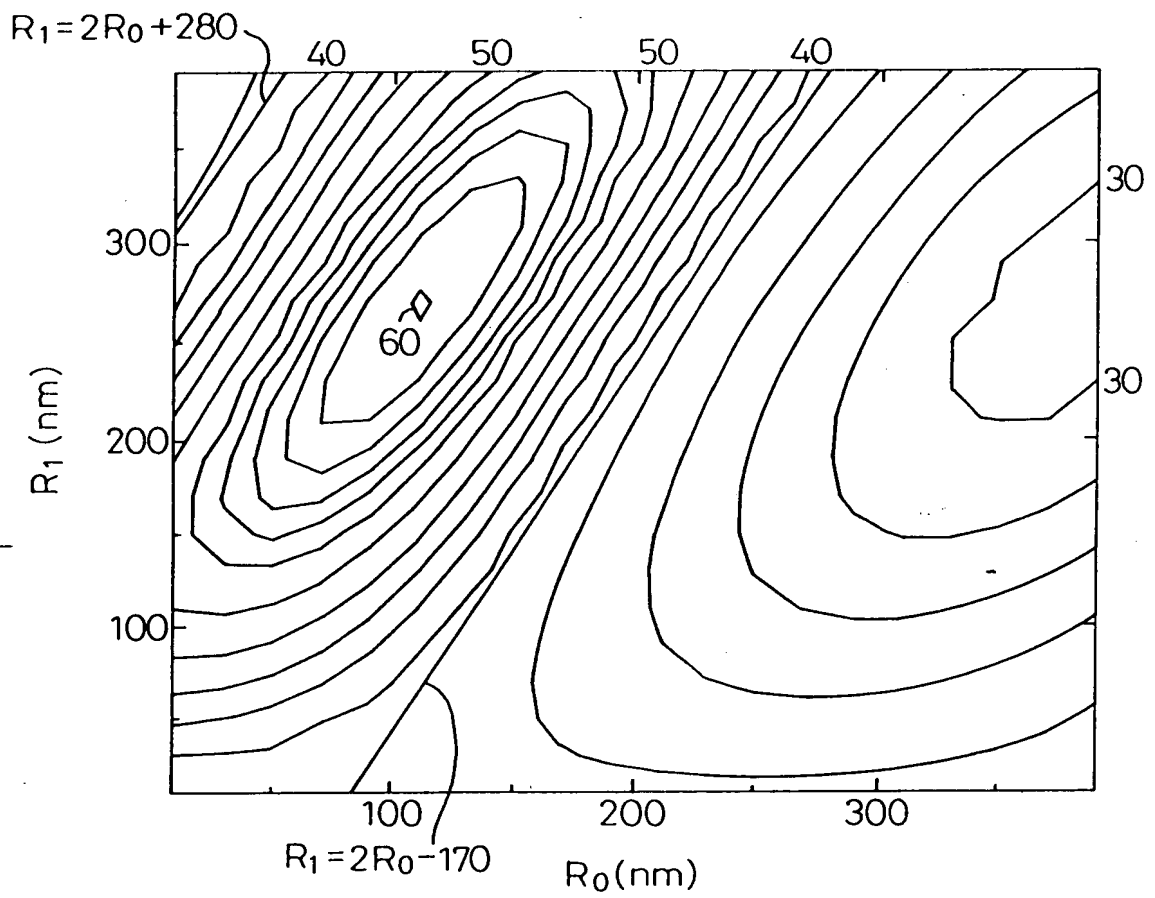
214/246

Fig. 223



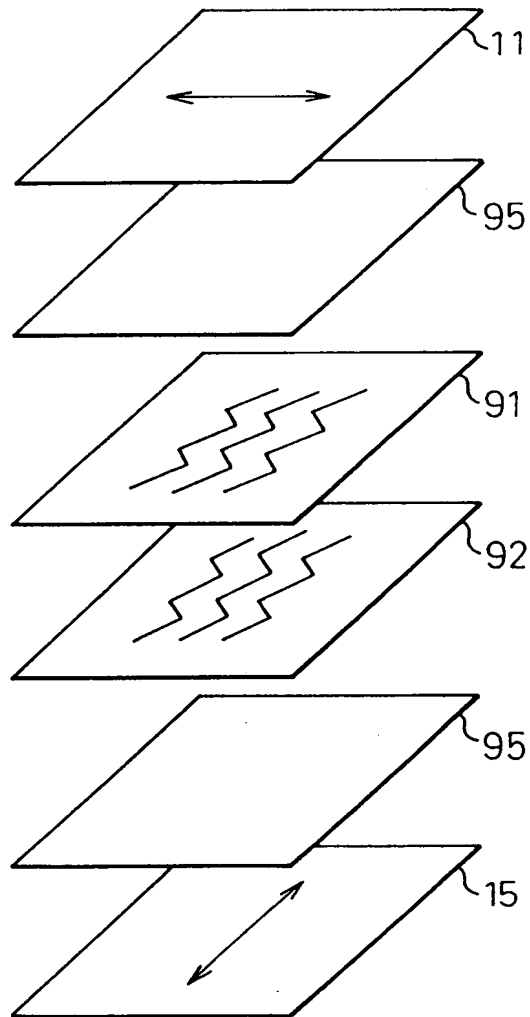
215/246

Fig. 224



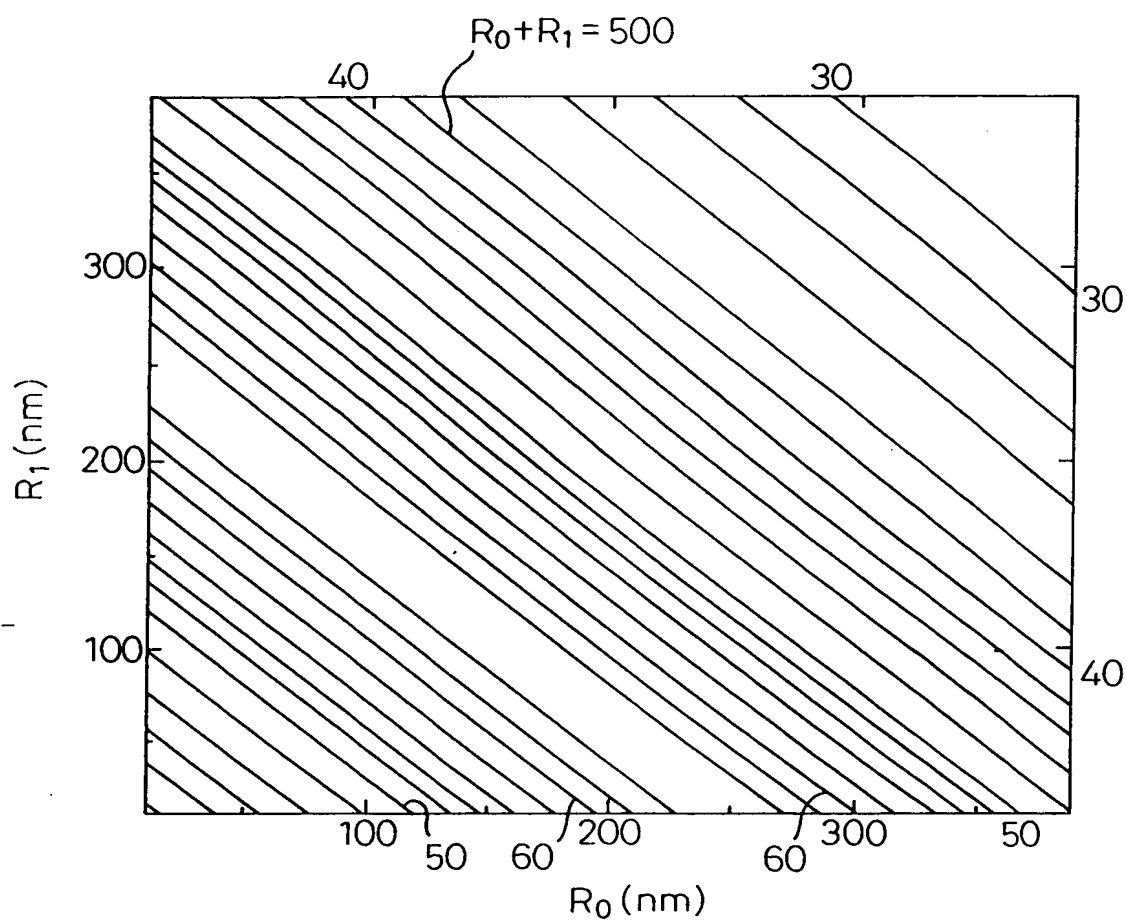
216/246

Fig. 225



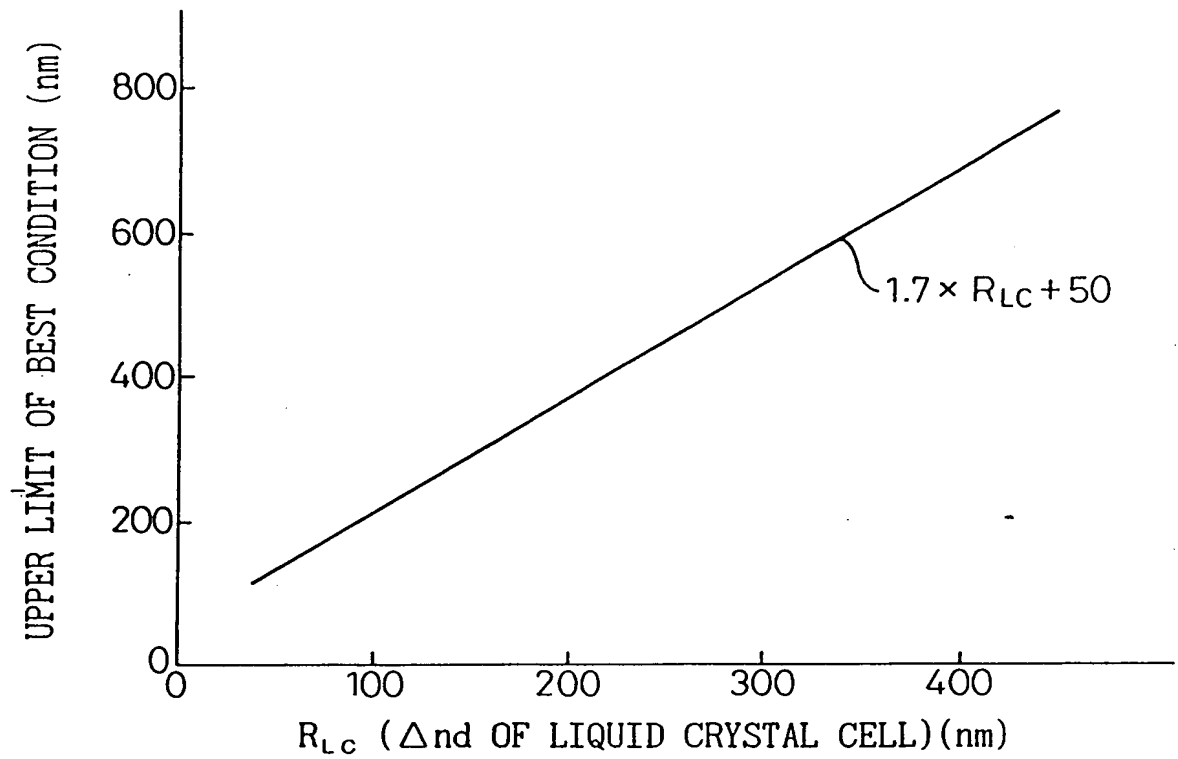
217/246

Fig. 226



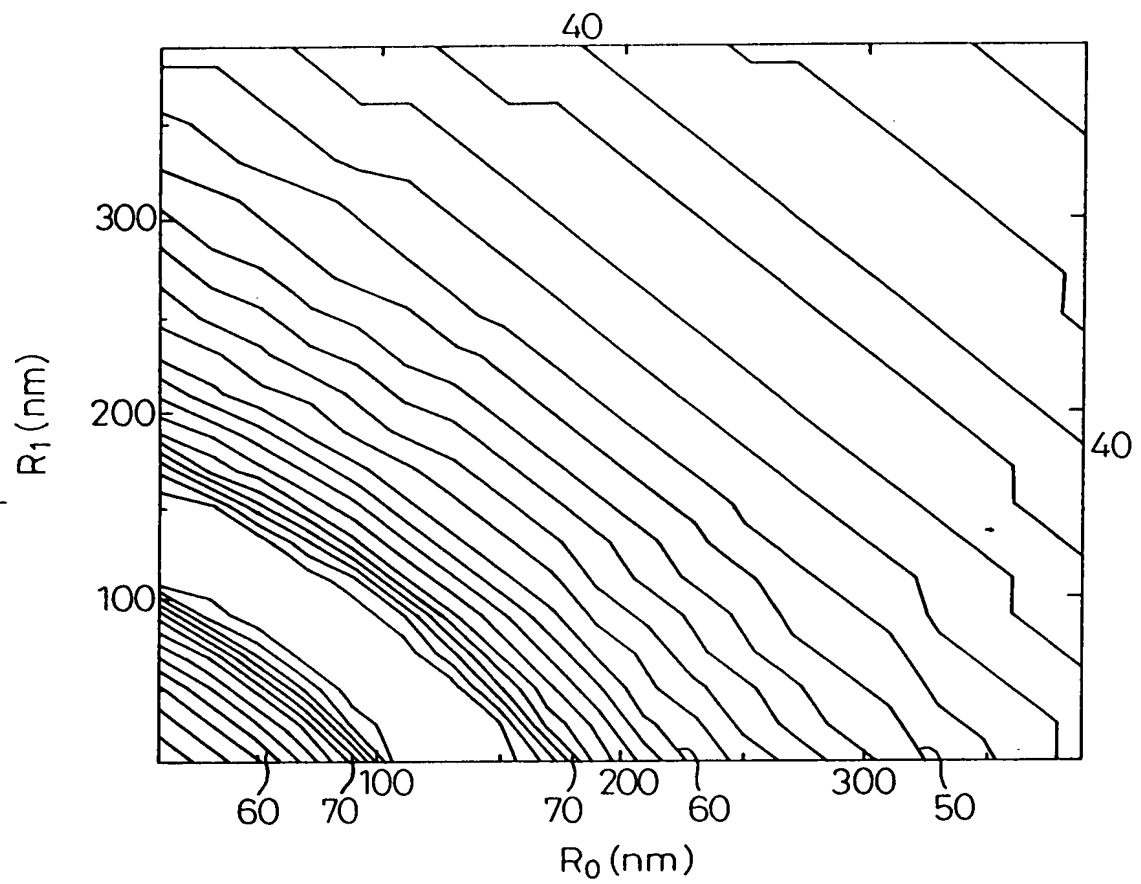
218/
246

Fig .227



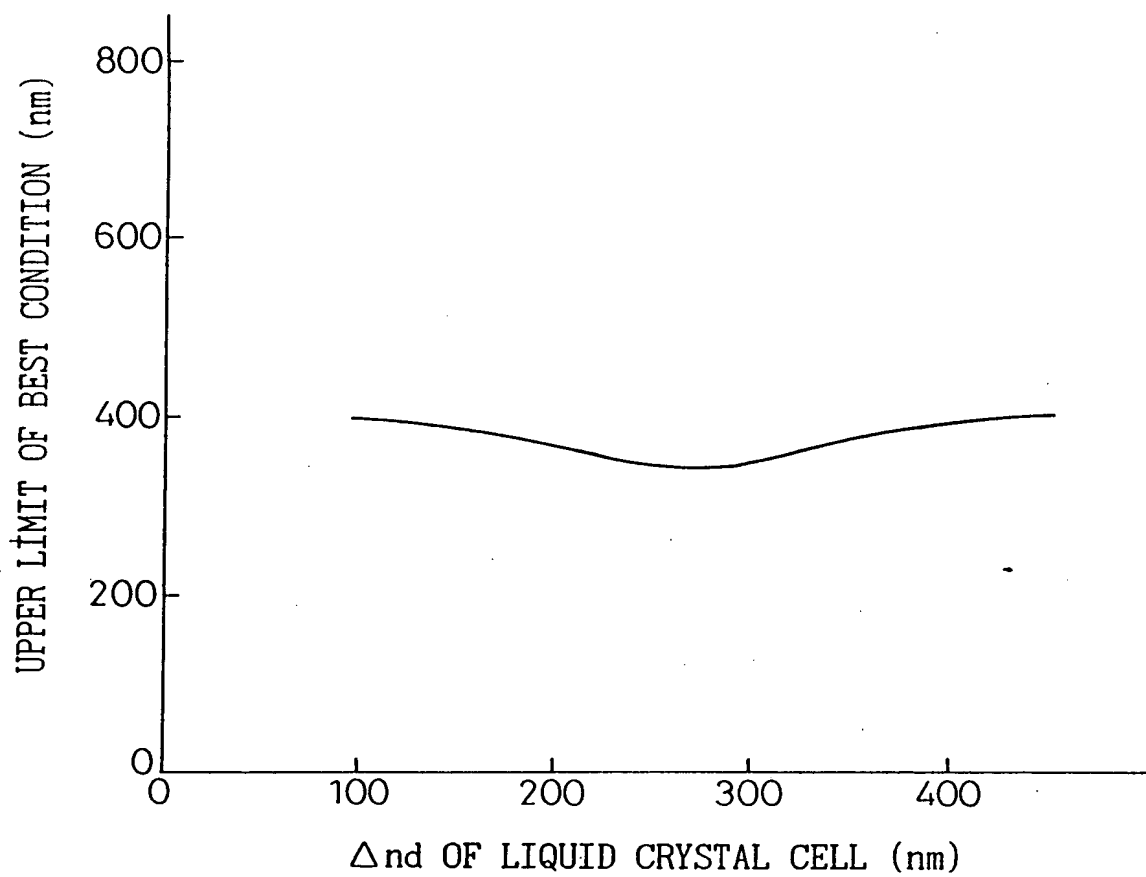
219/246

Fig.228



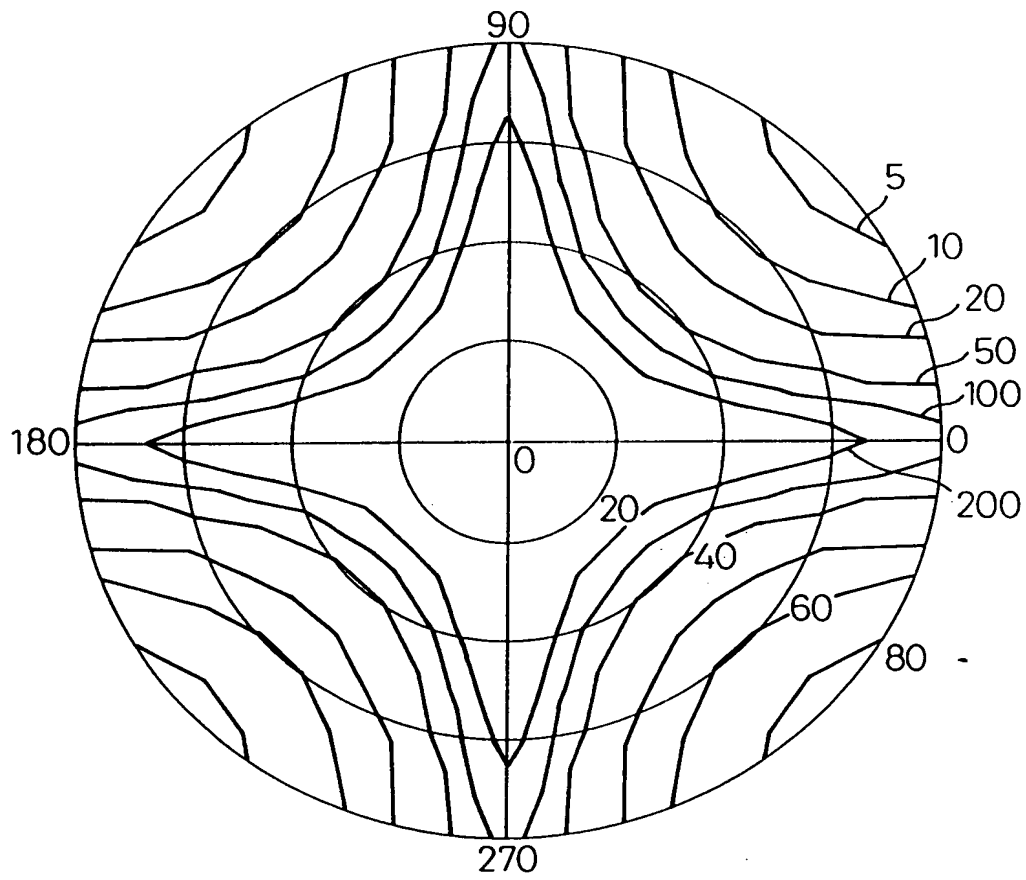
$\frac{220}{246}$

Fig. 229



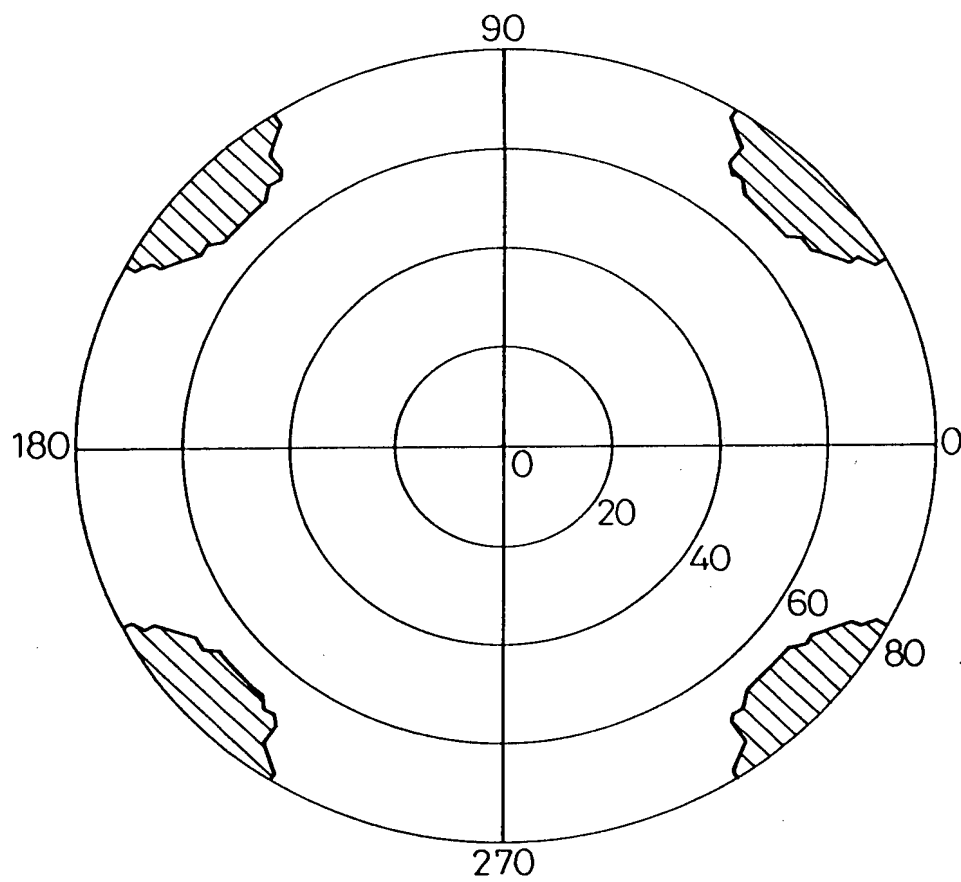
221/246

Fig. 230



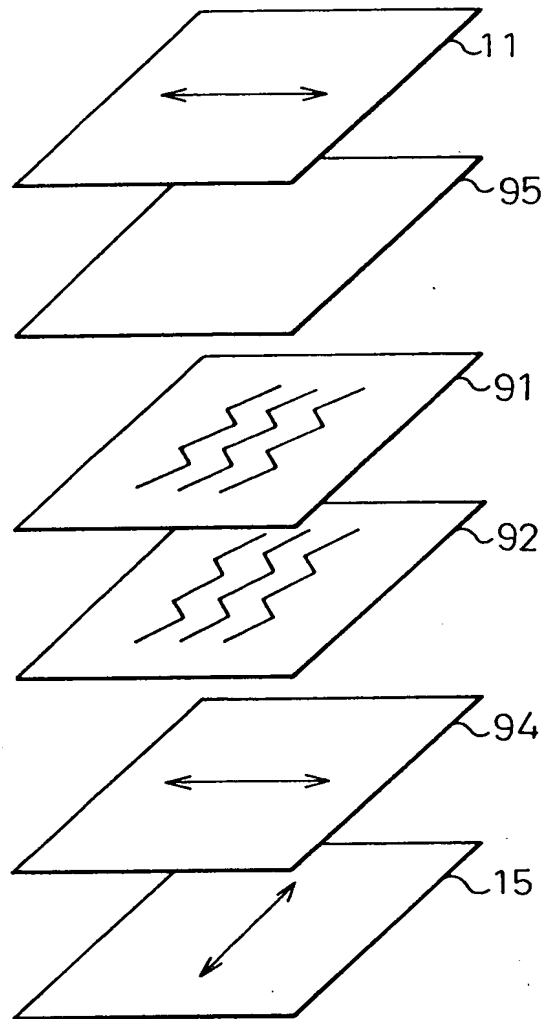
222/246

Fig. 231



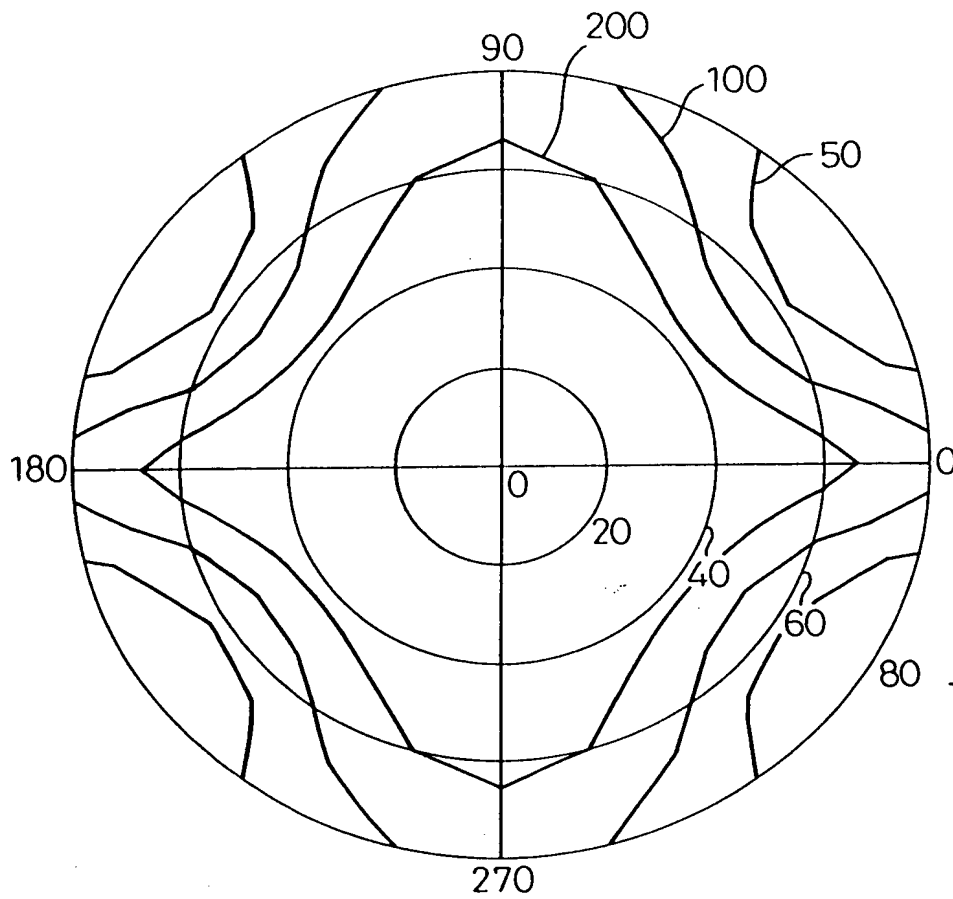
223/246

Fig. 232



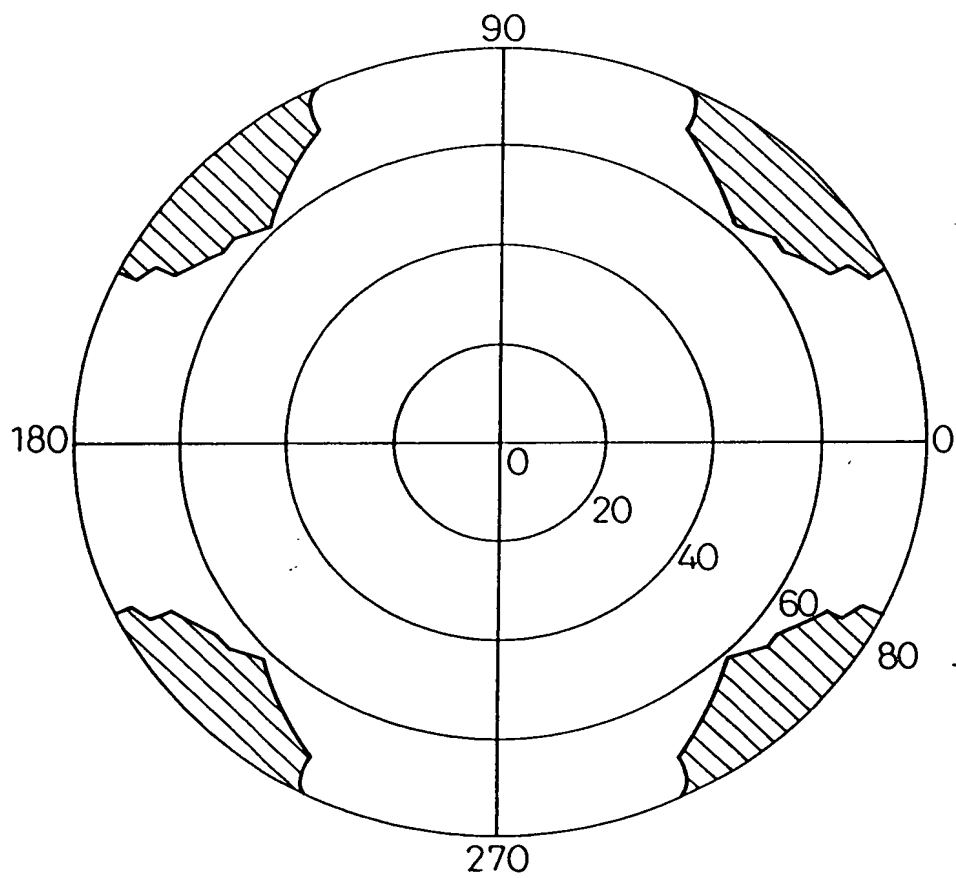
224/246

Fig. 233



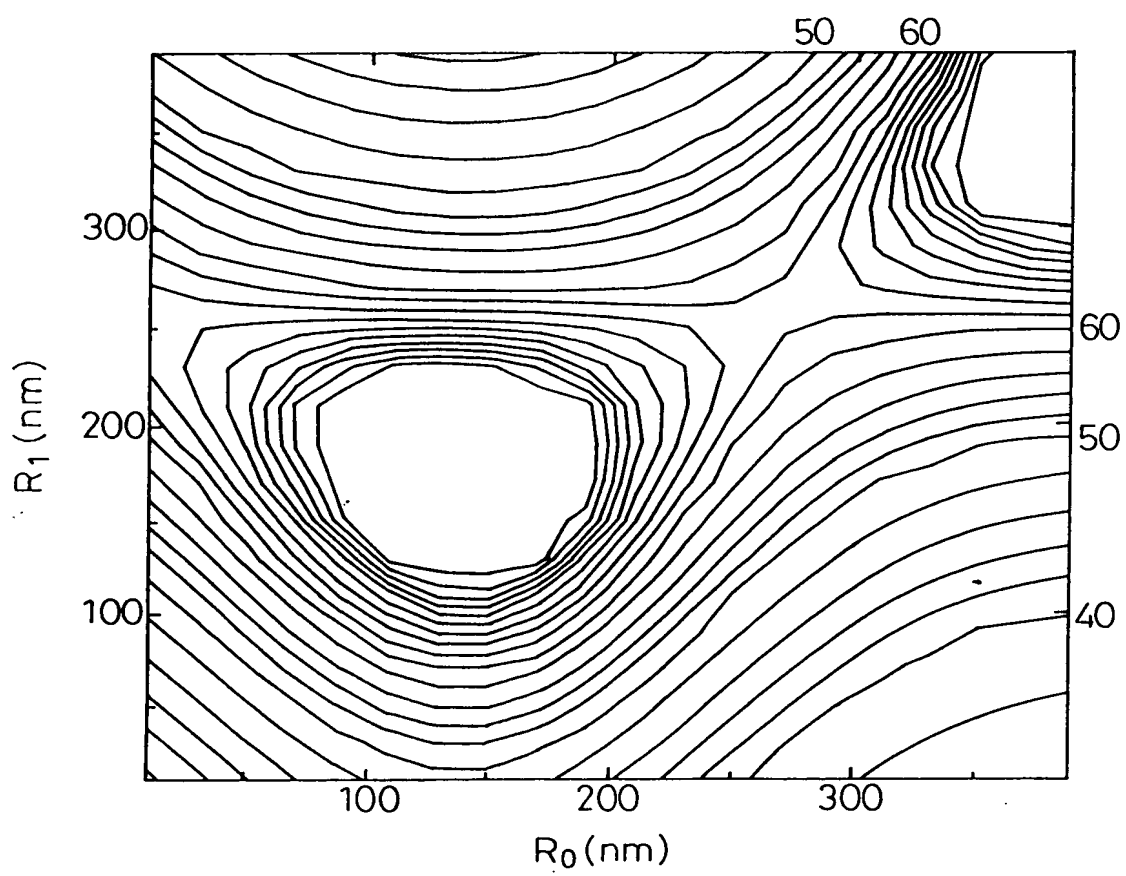
$$\frac{225}{246}$$

Fig. 234



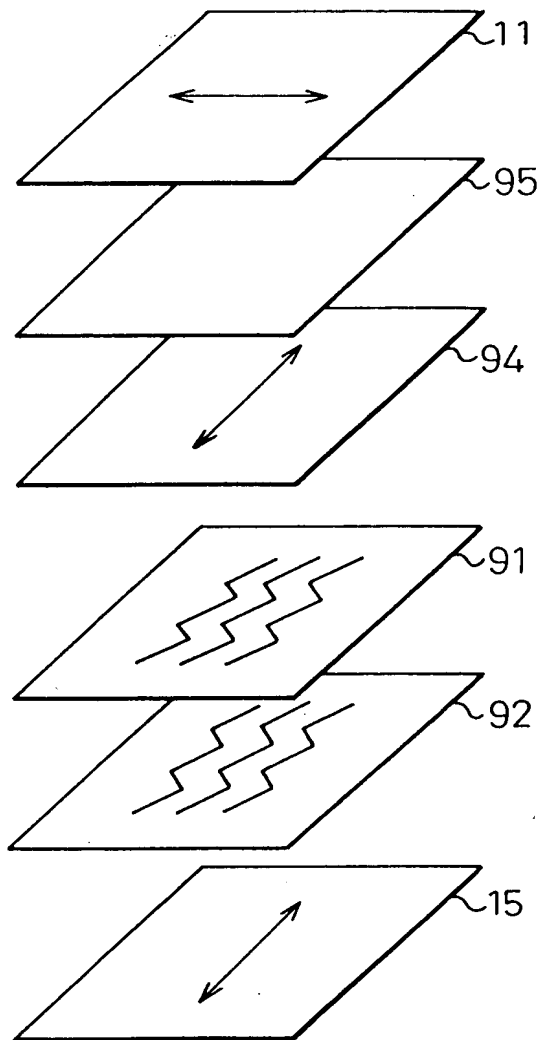
$\frac{226}{246}$

Fig. 235



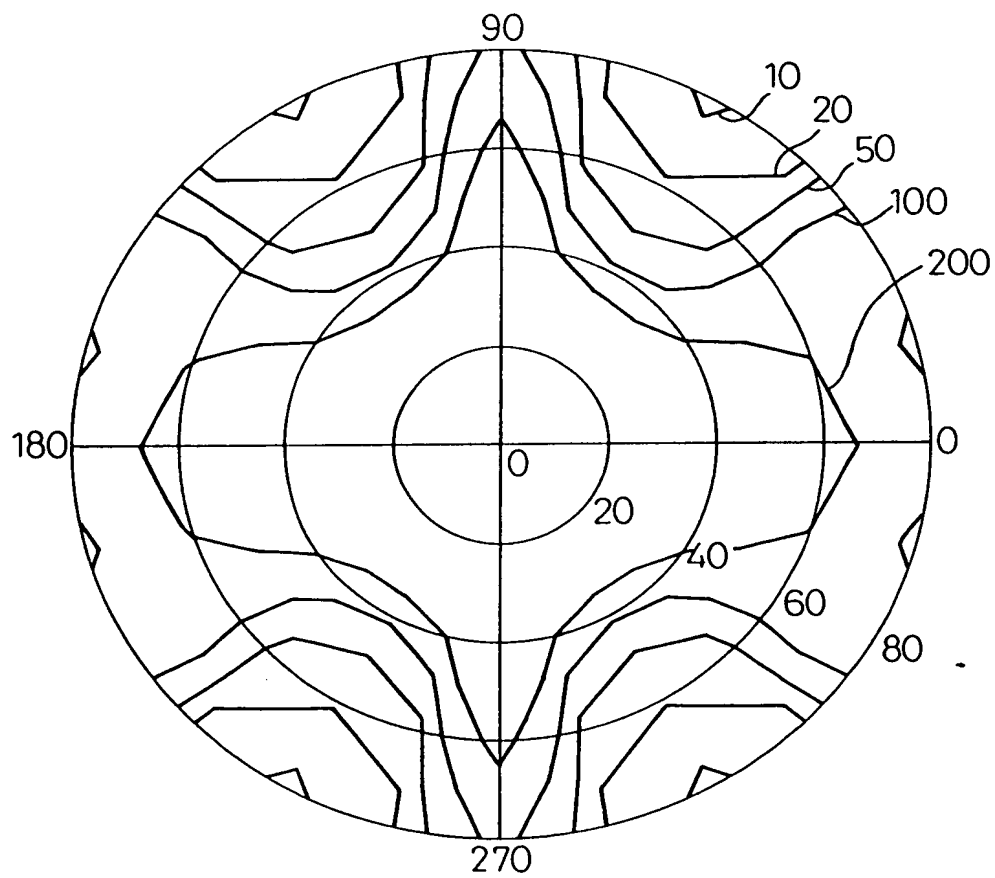
227/246

Fig. 236



228/246

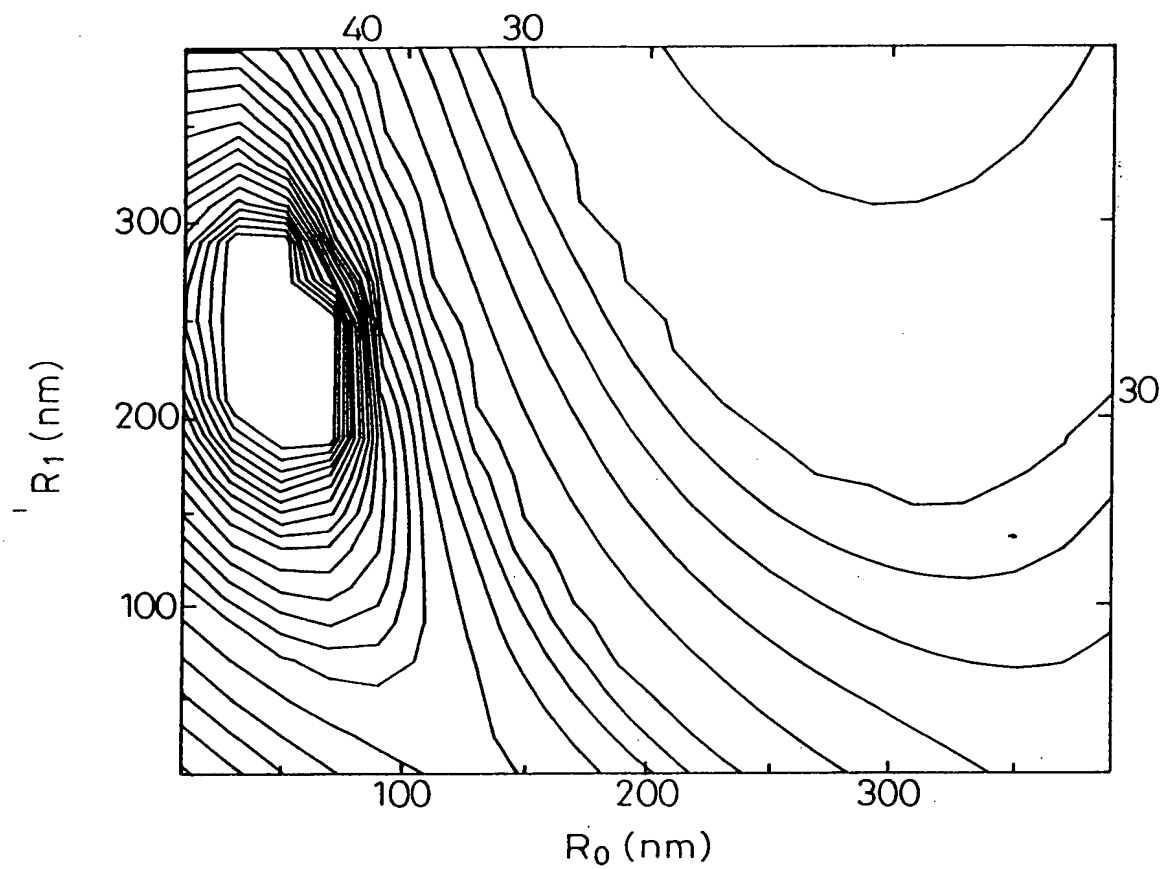
Fig. 237



[illegible]

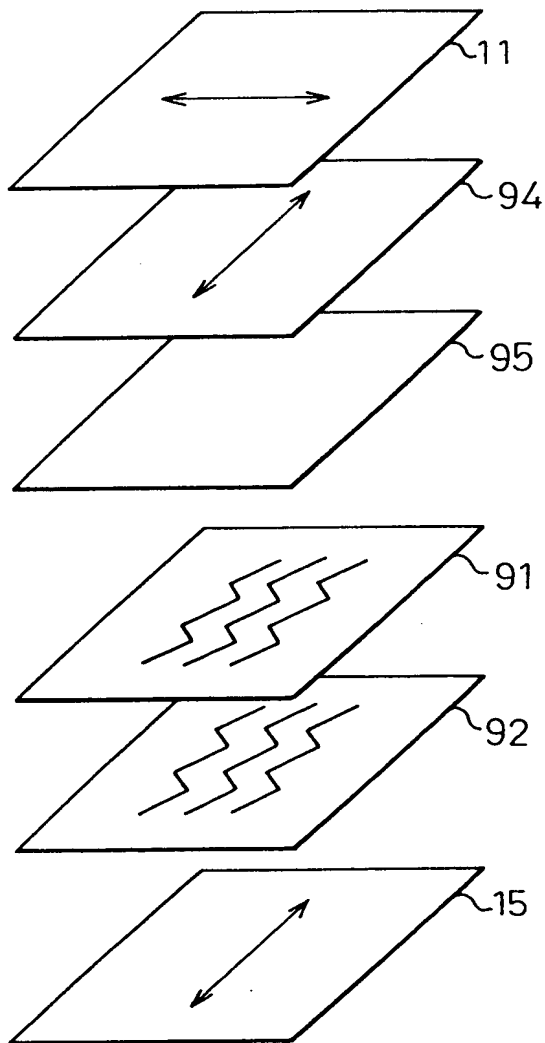
230/246

Fig. 239



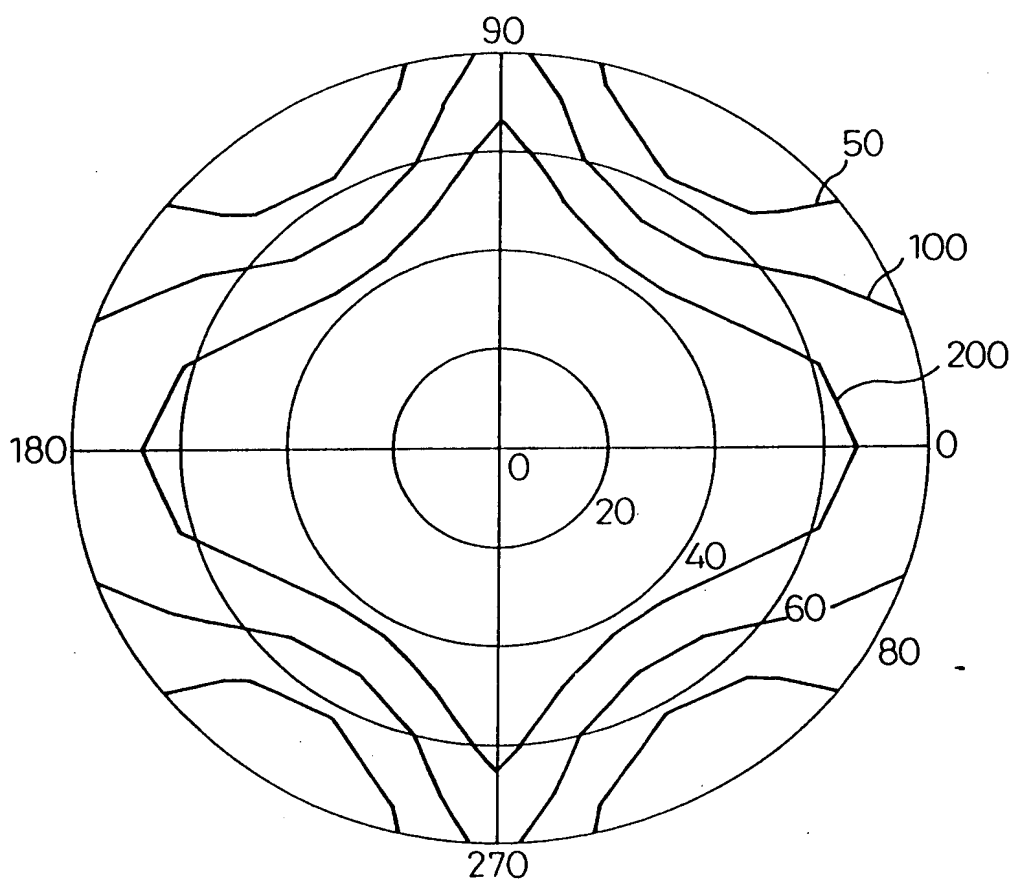
231/246

Fig. 240



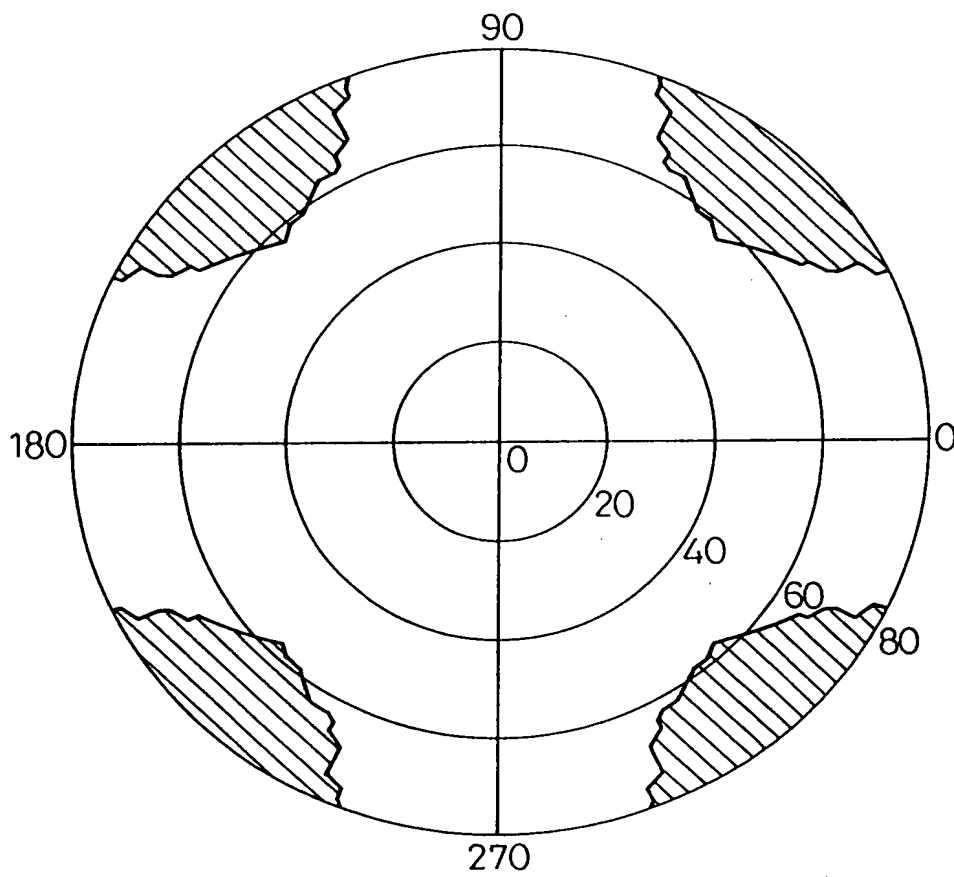
232/246

Fig .241



233/246

Fig. 242



234/246

Fig .243

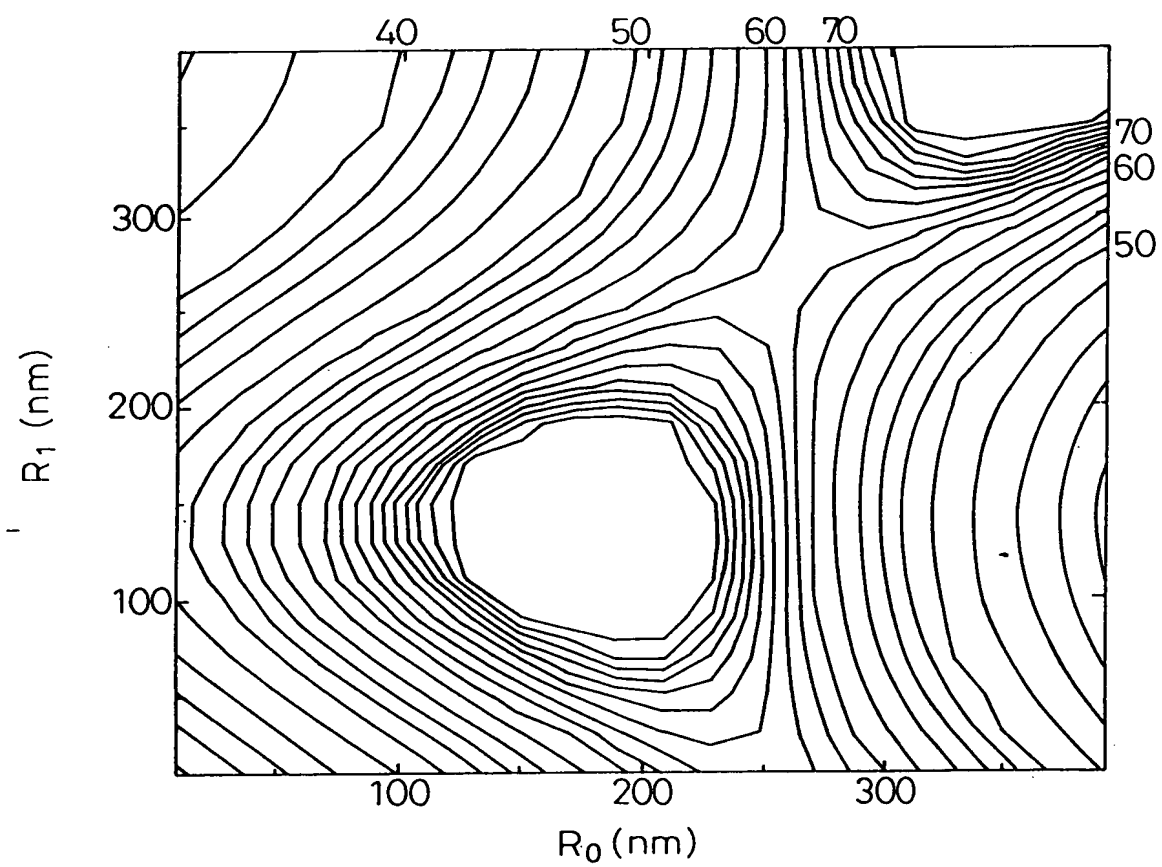
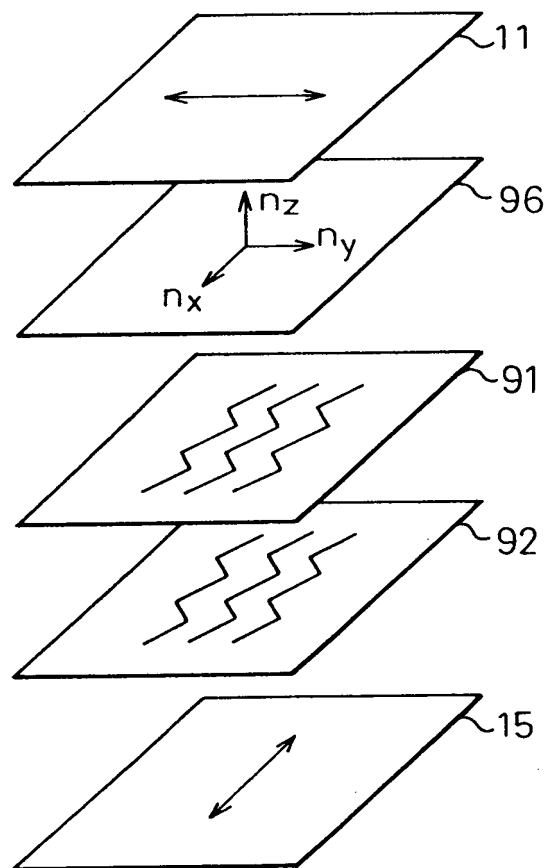
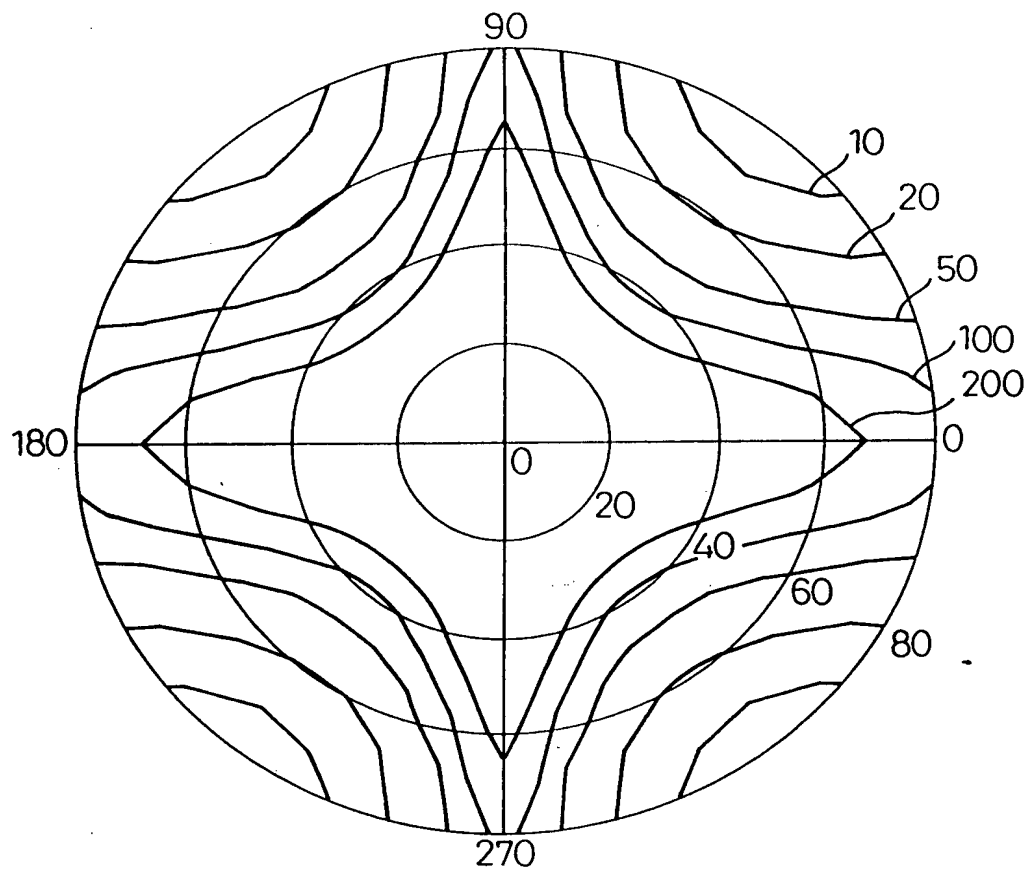


Fig. 244



236/246

Fig. 245



237/246

Fig. 246

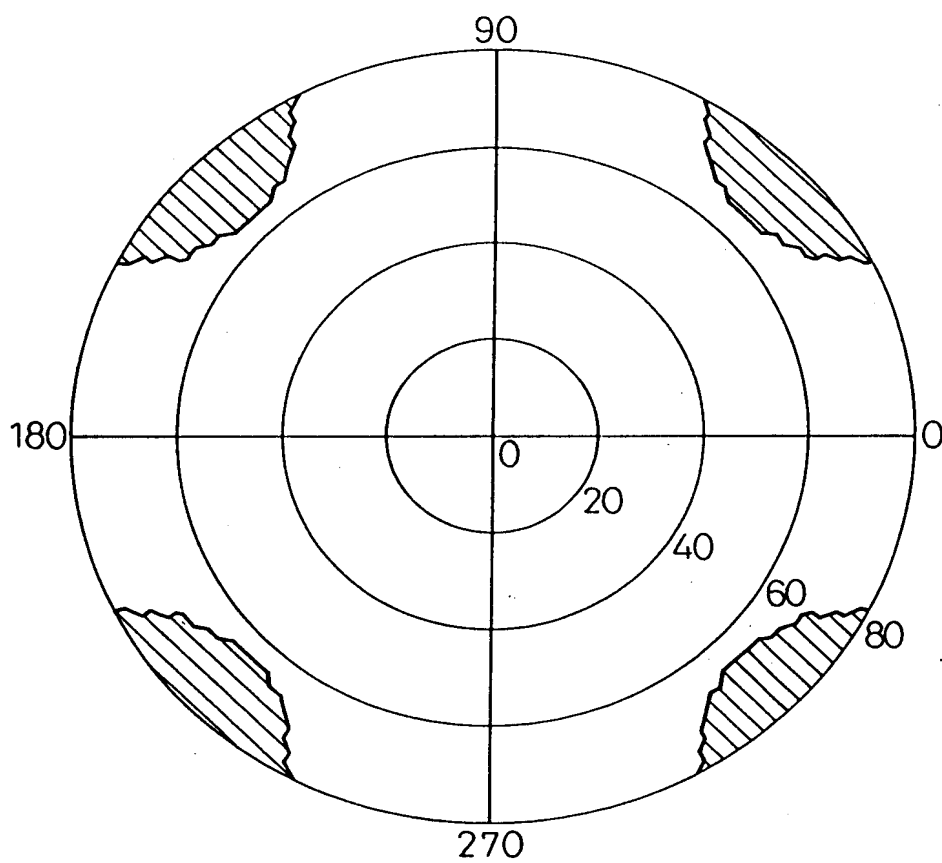
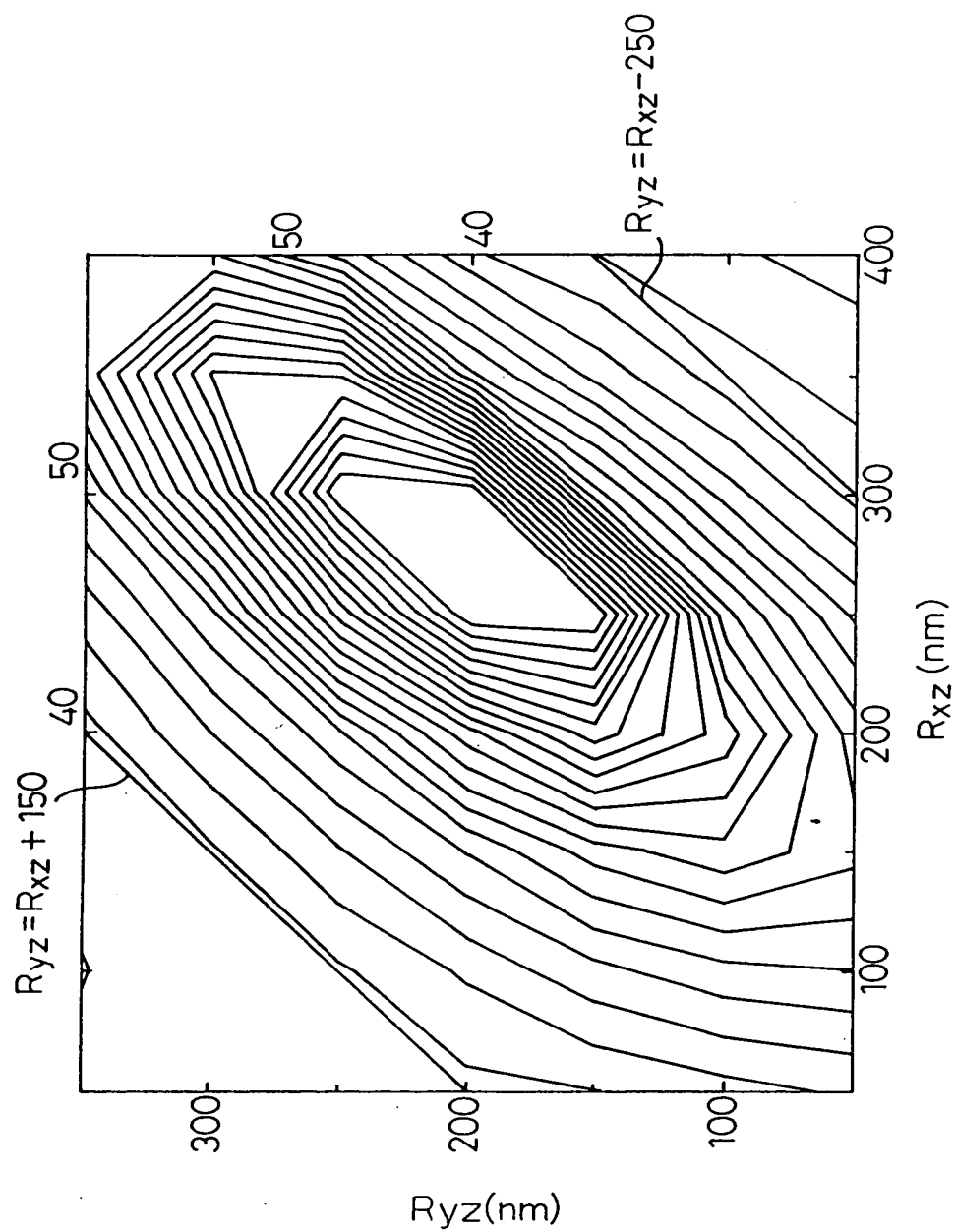


Fig. 247



238/246

239/
246

Fig .248

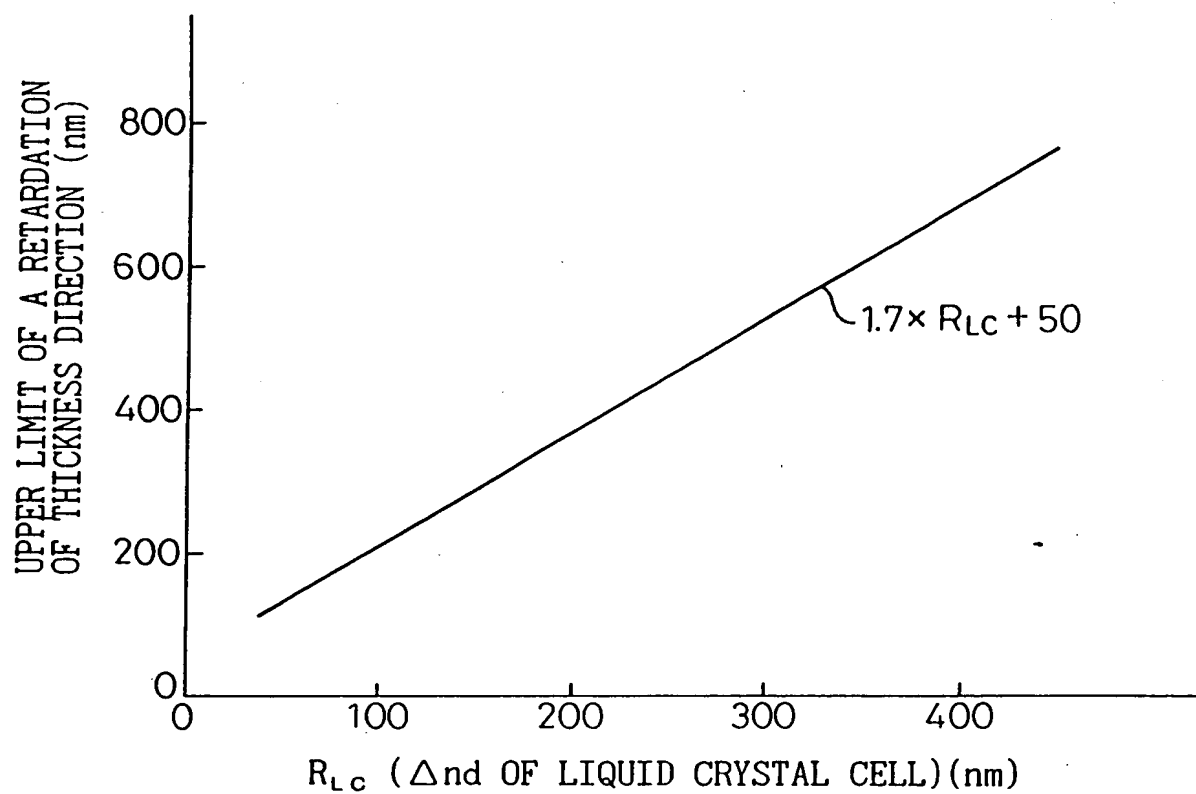


Fig. 249

SAMPLE	THICKNESS OF A PANEL (μm) R G B	GAP BETWEEN PROJECTIONS (μm) R G B	PHASE DIFFERENCE FILM Rd VALUE (nm)	TRANS- MITTANCE % (5v)	VIEW ANGLE : CR > 10 LEFT-RIGHT DIRECTION	COLOR DIFFERENCE (5v: LEFT -RIGHT) $\Delta u(x)$ $\Delta v(y)$
EMBODIMENT A	5.7, 4.6, 3.6	20, 25, 30	320	5.60	$\pm 80^\circ$	0.03 0.03
EMBODIMENT B	5.7, 4.6, 3.6	20, 25, 30	320	5.60	$\pm 80^\circ$	0.03 0.05
PRIOR ART 1	R, G, B = 3.6	R, G, B = 30	240	4.50	$\pm 80^\circ$	0.06 0.05
PRIOR ART 2	R, G, B = 4.6	R, G, B = 30	320	5.80	$\pm 80^\circ$	0.14 0.12

240/
246

241/
246

Fig. 250

EXAMPLES	INITIAL VALUES	AFTER 200 HOURS
EMBODIMENT C	25	42
EMBODIMENT D	33	51
EMBODIMENT E	26	45
EMBODIMENT F	30	48
REFERENCE	32	70

242/
246

Fig. 251A

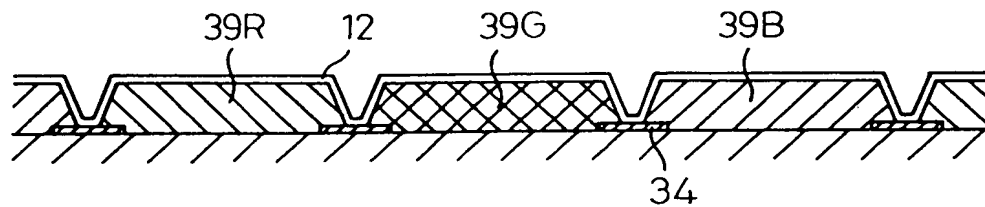


Fig. 251B

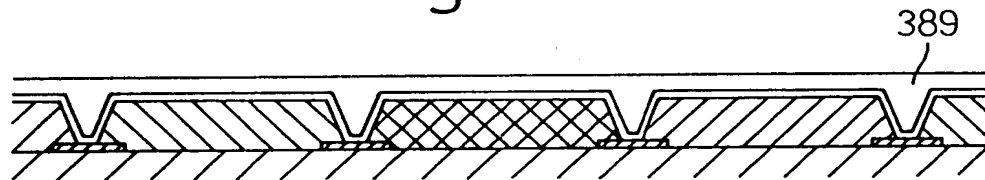


Fig. 251C

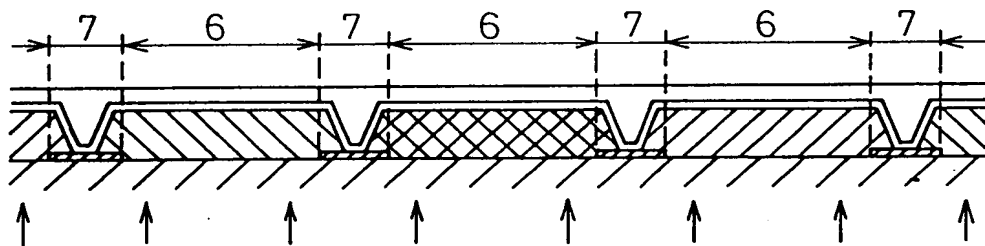
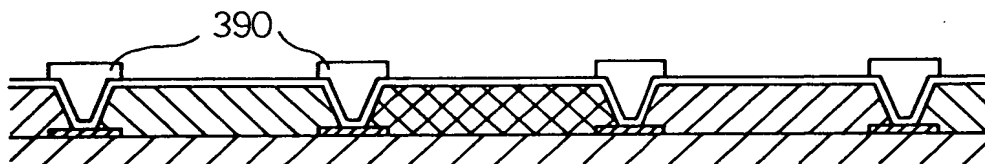


Fig. 251D



243/246

Fig.252A

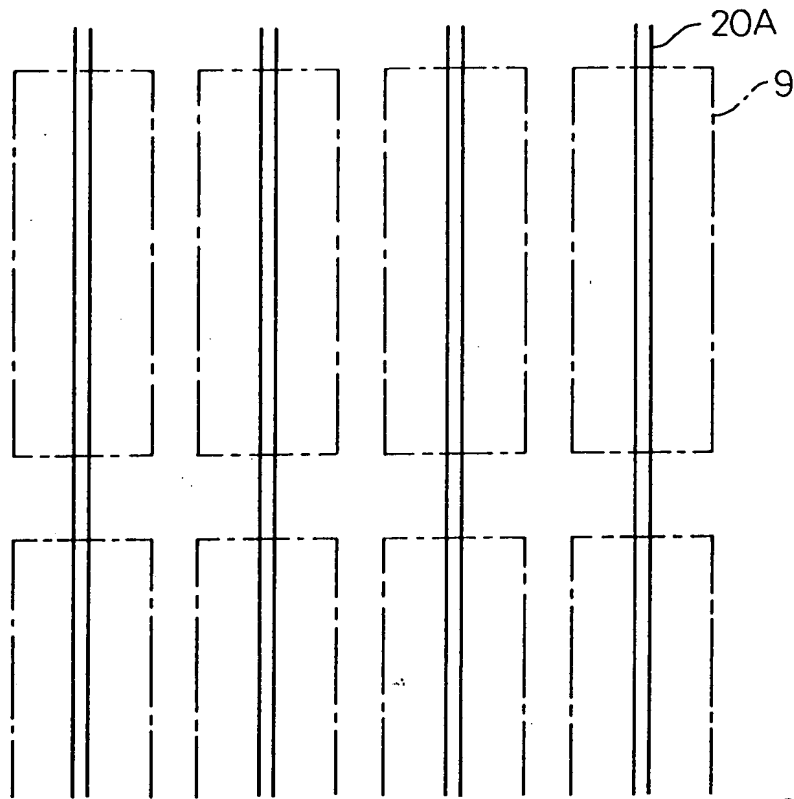
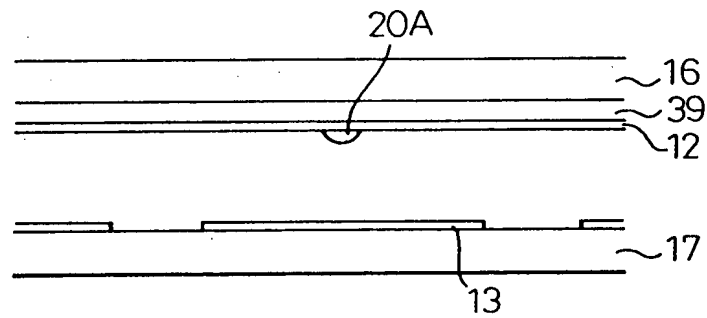
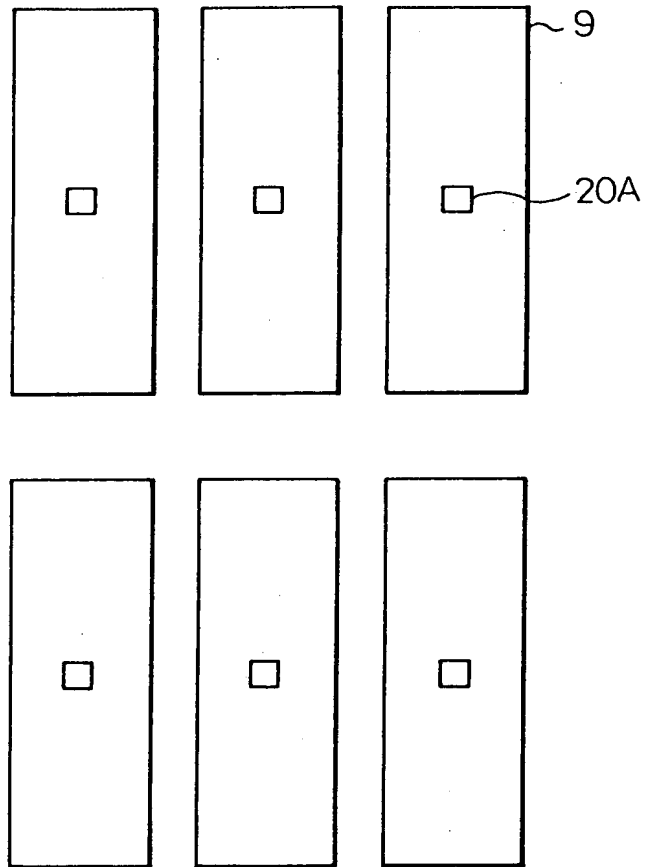


Fig.252B



244/
246

Fig. 253



245/
246

Fig. 254 A

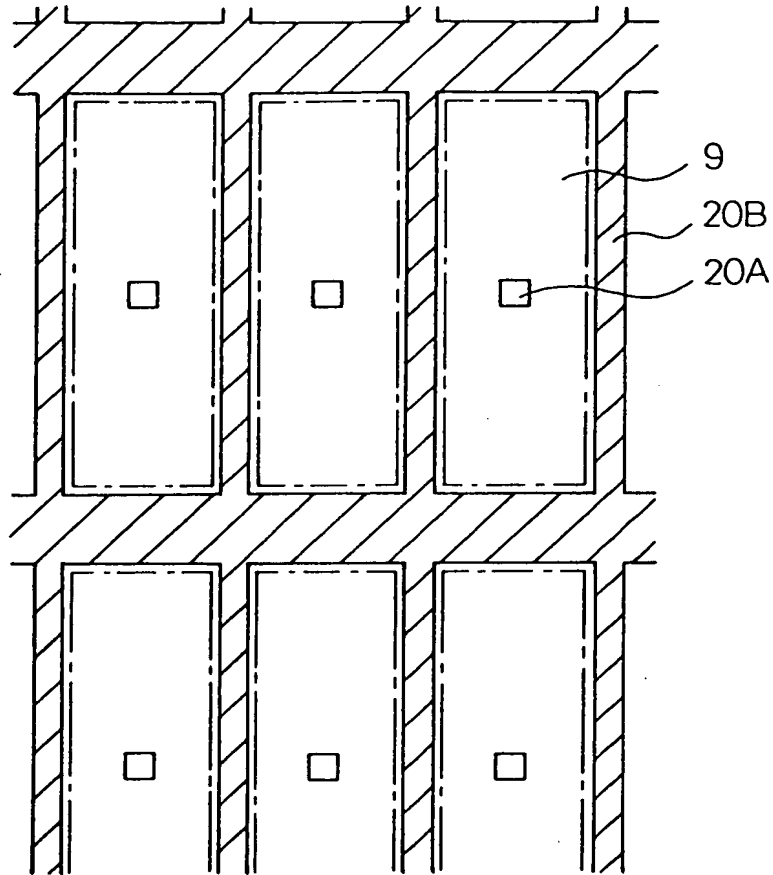
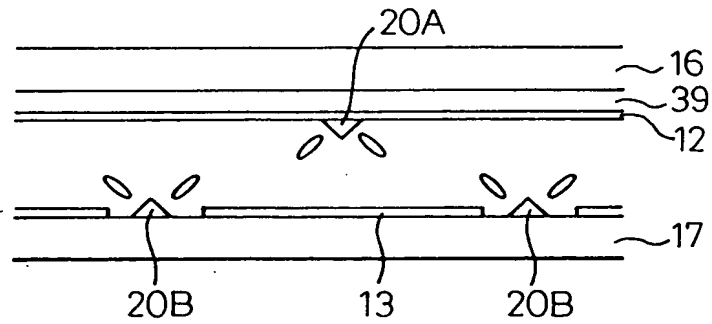


Fig. 254 B



246/246

Fig. 255

